Appendix C

SWM Facility Rating Curves

Lower Morrison Creek West SWM Faciltiy Rating Curve for Flood Control		
Stage	Storage (m^3)	Discharge (m^3/s)
Permanent Pool	0	0
25-year	6176	15.9
100-year	7411	21.2
Overflow	7782	100

Lower Morrison Creek East SWM Faciltiy Rating Curve for Flood Control		
Stage	Storage (m^3)	Discharge (m^3/s)
Permanent Pool	0	0
25-year	9894	12.4
100-year	12222	15.9
Overflow	12833	100

Wedgewood Creek West SWM Faciltiy Rating Curve for Flood Control		
Stage	Storage (m^3)	Discharge (m^3/s)
Permanent Pool	0	0
25-year	6310	4.2
100-year	6993	5.7
Overflow	7343	100

Wedgewood Creek East SWM Faciltiy Rating Curve for Flood Control		
Stage	Storage (m^3)	Discharge (m^3/s)
Permanent Pool	0	0
25-year	21518	20.2
100-year	24746	26.7
Overflow	25983	100

Lower Morrison Creek West SWM Faciltiy Rating Curve for Erosion Control		
Stage	Storage (m^3)	Discharge (m^3/s)
Permanent Pool	0	0
Extended Detention	6587	1.027

Lower Morrison Creek East SWM Faciltiy Rating Curve for Erosion Control		
Stage	Storage (m^3)	Discharge (m^3/s)
Permanent Pool	0	0
Extended Detention	9312	0.340

Wedgewood Creek West SWM Faciltiy Rating Curve for Erosion Control		
Stage	Storage (m^3)	Discharge (m^3/s)
Permanent Pool	0	0
Extended Detention	5458	0.211

Wedgewood Creek East SWM Faciltiy Rating Curve for Erosion Control		
Stage	Storage (m^3)	Discharge (m^3/s)
Permanent Pool	0	0
Extended Detention	17214	0.884

Appendix D

Revised Subcatchment Imperviousness Estimation Methodology and Subcatchment Parameterization

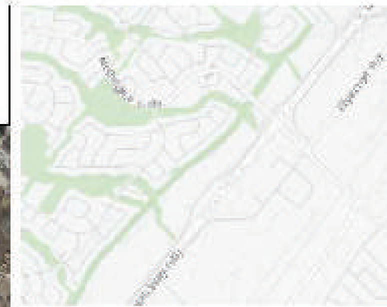
Table 2 Impervious Coverages for Residential Zones and Municipal Rights-of-Way (%)		
Zone Classification	**Type**	**Imperviousness**
Residential Low (RL1)	ROW	60.1
	Lot	44.5
Residential Low (RL1-0)	ROW	64.0
	Lot	34.0
Residential Low (RL2)	ROW	NA[1]
	Lot	55.0
Residential Low (RL2-0)	ROW	64.1
	Lot	39.1
Residential Low (RL3)	ROW	70.8
	Lot	47.4
Residential Low (RL3-0)	ROW	58.8
	Lot	43.2
Residential Low (RL4)	ROW	NA[2]
	Lot	NA[2]
Residential Low (RL4-0)	ROW	58.4
	Lot	40.4
Residential Low (RL5)	ROW	70.8
	Lot	58.3
Residential Low (RL5-0)	ROW	70.5
	Lot	49.1
Residential Low (RL6)	ROW	63.6
	Lot	62.9
Residential Low (RL7)	ROW	65.1
	Lot	62.5
Residential Low (RL7-0)	ROW	59.0
	Lot	58.3
Residential Low (RL8)	ROW	76.1
	Lot	58.9
Residential Low (RL8-0)	ROW	73.4
	Lot	49.4
Residential Low (RL9)	ROW	76.4
	Lot	61.5
Residential Low (RL10)	ROW	NA[1]
	Lot	46.7
Residential Low (RL10-0)	ROW	NA[1]
	Lot	47.0
Residential Low (RL11)	ROW	79.0
	Lot	51.4
Residential Medium (RM1)	ROW	80.5
	Lot	61.5
Residential Medium (RM2)	ROW	NA[2]
	Lot	NA[2]
Residential Medium (RM3)	ROW	NA[2]
	Lot	NA[2]
Residential Medium (RM4)	ROW	63.9
	Lot	80.4
Residential High	ROW	60.4
	Lot	68.3
Residential Uptown Core	ROW	NA[2]
	Lot	NA[2]

Notes: [1] No road right-of-ways are associated with the residential zones based on the zoning information and property parcel data provided by the Town

[2] The residential zone or right-of way is not found within the study area based on the zoning information and property parcel data provided by the Town

Table 3 Impervious Coverages for Non-Residential Zones (%)	
Class	**Imperviousness**
Neighbourhood Commercial	82.9
Community Commercial	85.2
Core Commercial	89.3
Central Business District	100.0
Cemetery	8.7
Community Use	30.1
Office Employment	84.0
Business Employment	93.4
Industrial	77.8
Institutional	75.1
Business Commercial	87.9
Existing Development	62.7
Greenbelt	5.0
Midtown Transitional Commercial	92.2
Midtown Transitional Employment	82.8
Main Street 1	100.0
Main Street 2	95.0
Urban Centre	90.0
Urban Core	95.0
Natural Area	5.0
Park	10.0
Private Open Space	5.0
Parkway Belt Public Use	25.0
Parkway Belt Complementary Use	10.0
Utility	26.6

FIGURE 1: MONITORING LOCATIONS

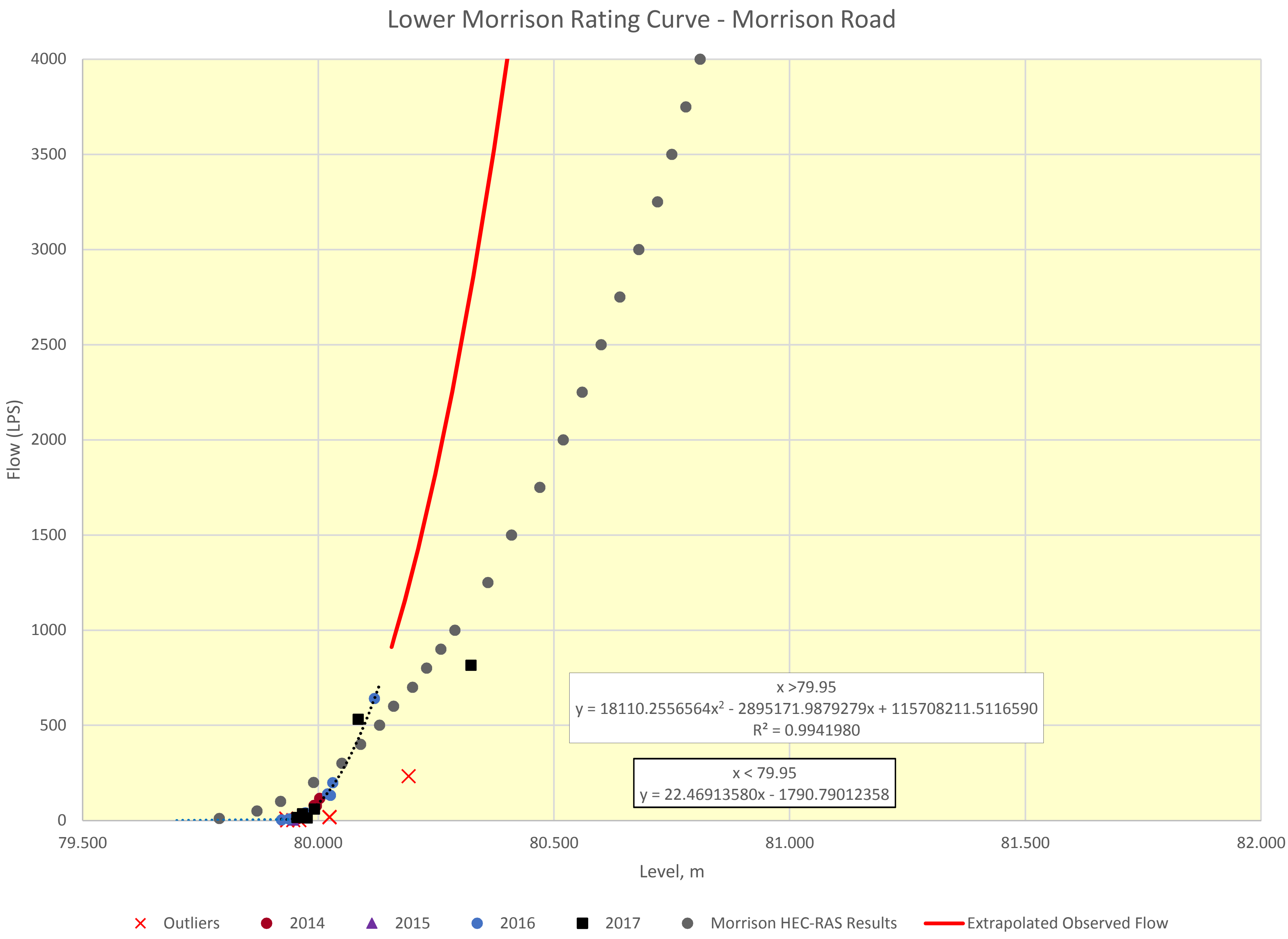


Legend
Cemeteries
Parks
Monitoring Location

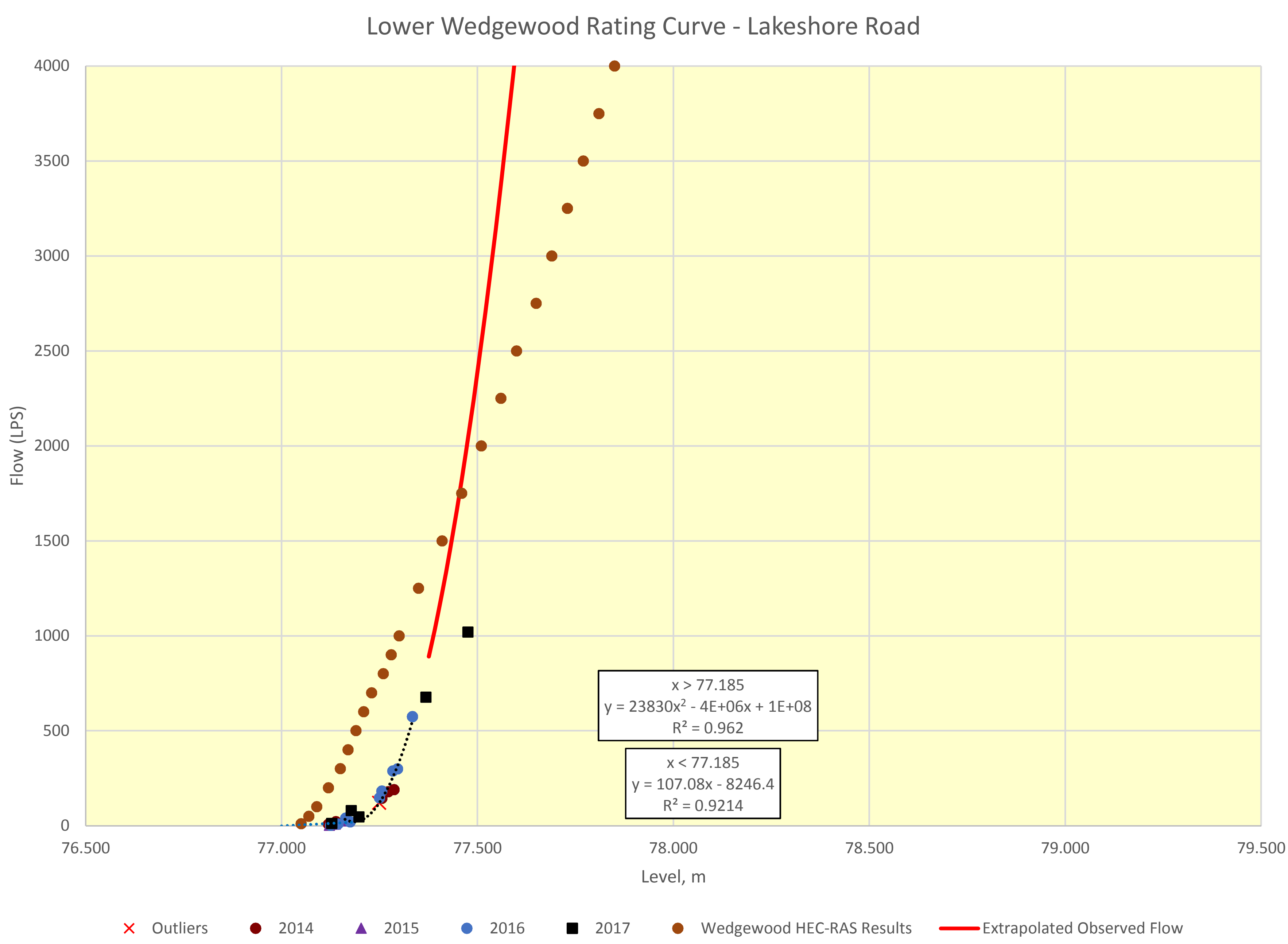
Notes

Disclaimer: THIS IS NOT A LEGAL PLAN OF SURVEY.

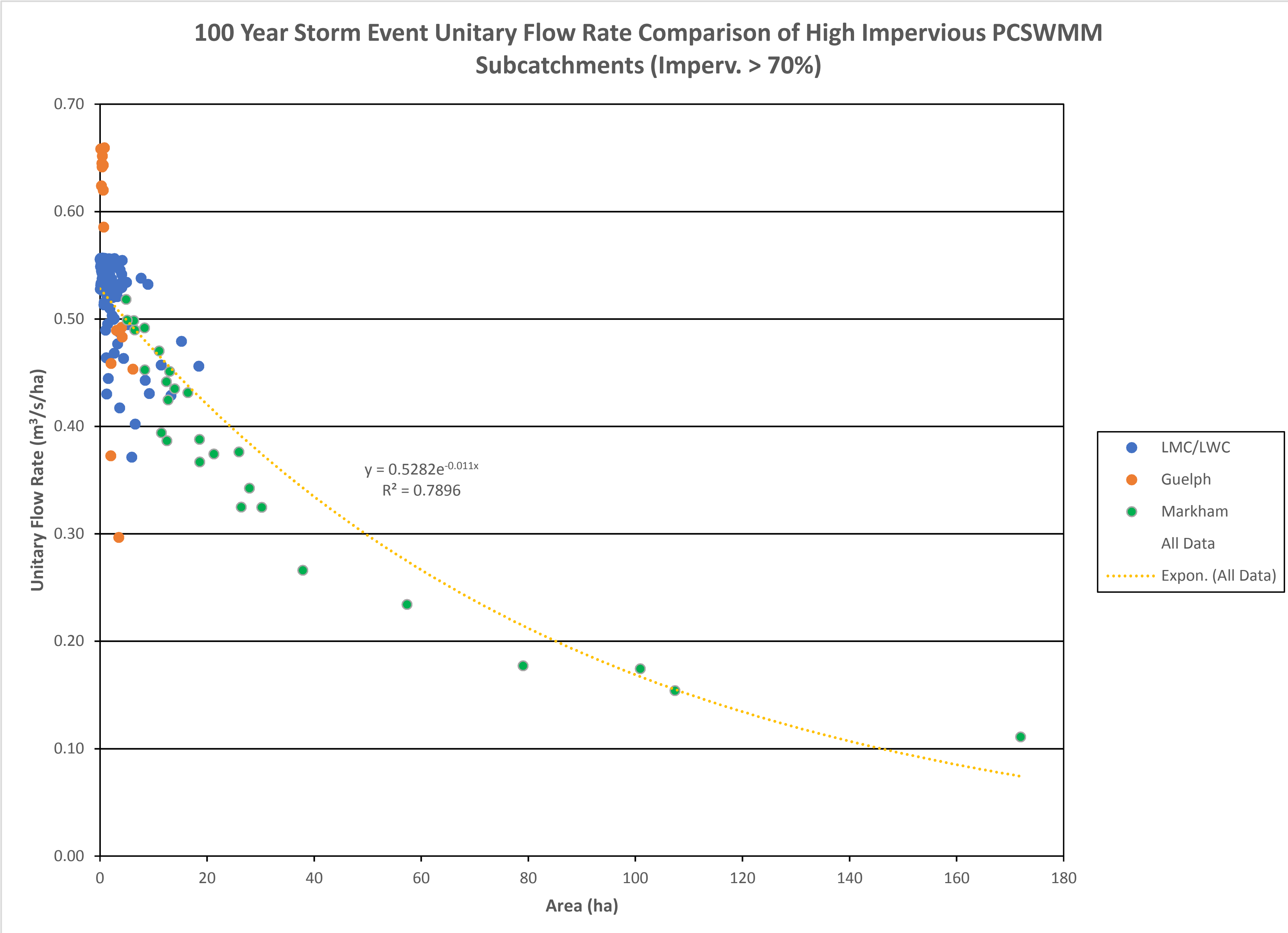
May 22, 2015

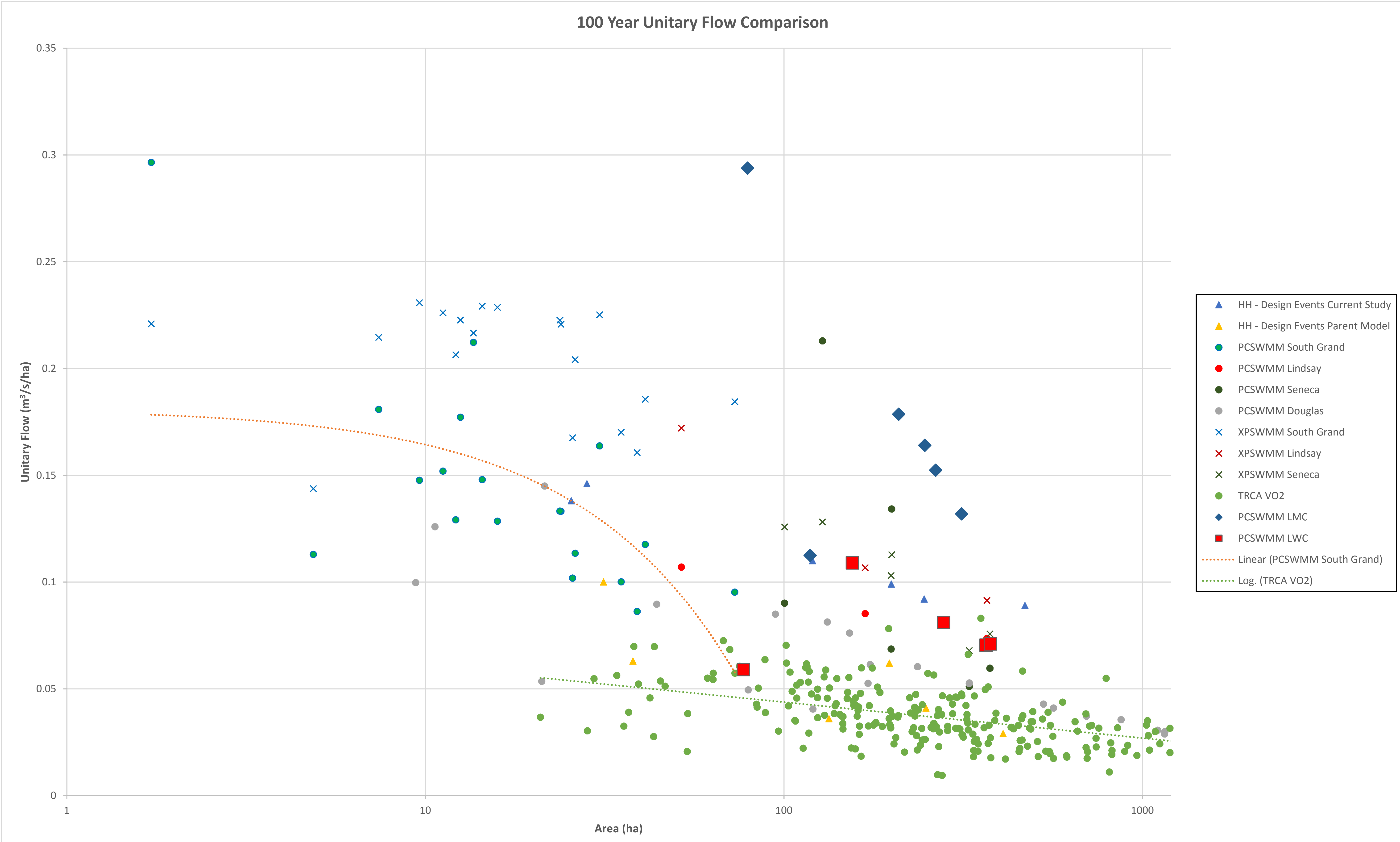


Lower Morrison Rating Curve - Morrison Road
Flow (LPS)
4000
3500
3000
2500
2000
1500
1000
500
0
79.500
80.000
80.500
81.000
81.500
82.000
Level, m
x >79.95
y = 18110.2556564x² - 2895171.9879279x + 115708211.5116590
R² = 0.9941980
x < 79.95
y = 22.46913580x - 1790.79012358
Outliers
2014
2015
2016
2017
Morrison HEC-RAS Results
Extrapolated Observed Flow

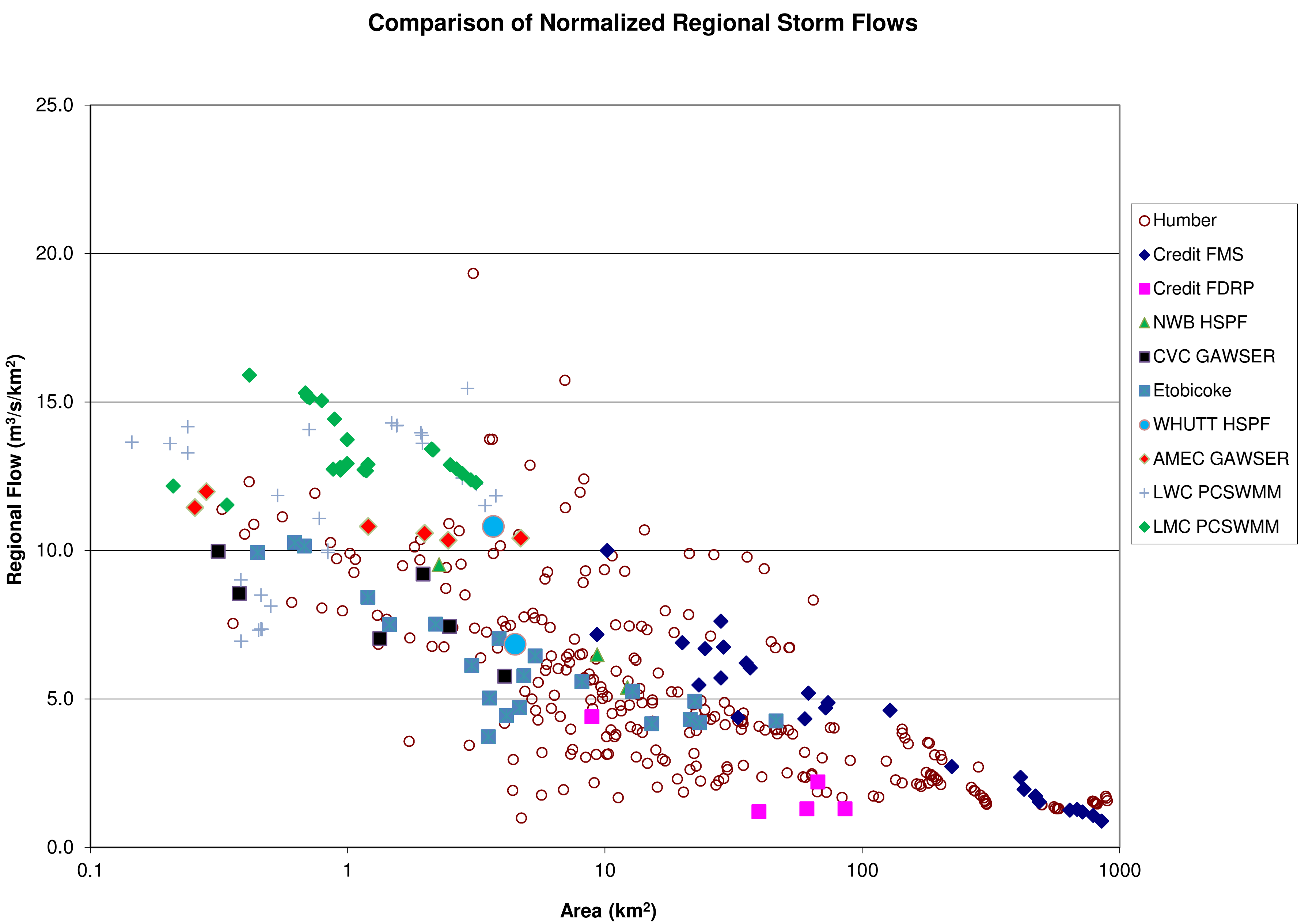


Lower Wedgewood Rating Curve - Lakeshore Road
Flow (LPS)
4000
3500
3000
2500
2000
1500
1000
500
0
76.500
77.000
77.500
78.000
78.500
79.000
79.500
Level, m
x > 77.185
y = 23830x² - 4E+06x + 1E+08
R² = 0.962
x < 77.185
y = 107.08x - 8246.4
R² = 0.9214
Outliers
2014
2015
2016
2017
Wedgewood HEC-RAS Results
Extrapolated Observed Flow


100 Year Storm Event Unitary Flow Rate Comparison of High Impervious PCSWMM Subcatchments (Imperv. > 70%)
Unitary Flow Rate (m³/s/ha)
0.70
0.60
0.50
0.40
0.30
0.20
0.10
0.00
0
20
40
60
80
100
120
140
160
180
Area (ha)
y = 0.5282e^-0.011x
R² = 0.7896
LMC/LWC
Guelph
Markham
All Data
Expon. (All Data)



100 Year Unitary Flow Comparison
Unitary Flow (m3/s/ha)
0.35
0.3
0.25
0.2
0.15
0.1
0.05
0
1
10
100
1000
Area (ha)
HH - Design Events Current Study
HH - Design Events Parent Model
PCSWMM South Grand
PCSWMM Lindsay
PCSWMM Seneca
PCSWMM Douglas
XPSWMM South Grand
XPSWMM Lindsay
XPSWMM Seneca
TRCA VO2
PCSWMM LMC
PCSWMM LWC
Linear (PCSWMM South Grand)
Log. (TRCA VO2)


Comparison of Normalized Regional Storm Flows
25.0
20.0
15.0
10.0
5.0
0.0
Regional Flow (m3/s/km2)
0.1
1
10
100
1000
Area (km2)
Humber
Credit FMS
Credit FDRP
NWB HSPF
CVC GAWSER
Etobicoke
WHUTT HSPF
AMEC GAWSER
LWC PCSWMM
LMC PCSWMM

Appendix E

Hydraulic Structure Inventory

				Potential Channel/Structural Improvements		MTO Criteria									MNRF Criteria							
				Existing	Proposed	Existing					Proposed				Existing				Proposed			
	Reach ID	Road Classification	Location	Existing Structure (Span x Rise)	Potential Upgraded Structure (Span x Rise)	Largest Storm Conveyed (Without Overtopping)	Design Storm (for MTO Criteria)	Clearance (m)	FB (m)	Pass MTO Criteria (Y/N)	Largest Storm Conveyed (Without Overtopping)	Clearance (m)	FB (m)	Pass MTO Criteria (Y/N)	Overtopping Depth (m)	Velocity	Depth x Velocity	Pass MNRF Criteria (Y/N)	Overtopping Depth (m)	Velocity	Depth x Velocity	Pass MNRF Criteria (Y/N)
Morrison Creek	Reach 1 DS	Urban Arterial	Lakeshore	7.9 x 3.2 CONSPAN Arch	14.6 x 3.35 CONSPAN Arch	100	100	0.13	1.51	N	100.00	0.16	1.54	N	N/A	N/A	N/A	Y	N/A	N/A	N/A	Y
	Reach 1 DS	Urban Arterial	Morrison Rd	3.7 x 2.05 Box	N/A	2	50	-1.00	-0.30	N	2.00	N/A	N/A	N	0.36	0.87	0.31	Y	0.35	0.93	0.33	Y
	Reach 1	Urban Arterial	Linbrook Rd	7.3 x 1.5 CONSPAN Arch	N/A	25	100	-0.39	-0.15	N	100.00	0.40	0.64	N	0.15	0.50	0.08	Y	N/A	N/A	N/A	Y
	Reach 1	Urban Arterial	Chartwell Rd	Twin 3 x 2.1 Box	7.32 x 2.13 CONSPAN Arch	100	100	0.13	0.55	N	100.00	0.08	0.50	N	N/A	N/A	N/A	Y	N/A	N/A	N/A	Y
	Reach 1	Urban Arterial	Cornwall Rd	Twin 3.25 x 1.2 Box	N/A	50	100	-1.31	0.02	N	50.00	-1.31	0.02	N	0.02	0.46	0.01	Y	0.02	0.46	0.01	Y
	Reach 1	Urban Arterial	East Longo's Parking Lot	3.5 x 1.3 Box	N/A	10	50	-1.30	-0.06	N	10.00	N/A	N/A	N	0.06	0.41	0.02	Y	0.06	0.57	0.03	Y
	Reach 1	Urban Arterial	Under CNR	1.8 x 1.5 Box	N/A	2	50	-1.20	-0.15	N	2.00	N/A	N/A	N	0.15	0.86	0.13	Y	0.15	0.91	0.14	Y
	Reach 1	Urban Arterial	Hwy 403	5.97 x 1.5 Box	6.4 x 1.8 Box	100	50	0.30	1.52	Y	100.00	N/A	N/A	Y	N/A	N/A	N/A	Y	N/A	N/A	N/A	Y
	Reach 1 US	Urban Arterial	Chartwell Rd	3 x 1.6 Box	6.4 x 1.5 Box	2	50	-0.58	-0.40	N	10.00	-0.42	-0.24	N	0.40	0.44	0.18	Y	0.35	0.81	0.28	Y
	Reach 1 US	Urban Arterial	Maple Ave	3 x 1.2 Box	N/A	2	50	-0.80	-0.01	N	2.00	N/A	N/A	N	0.01	0.54	0.01	Y	0.01	0.58	0.01	Y
	Reach 1 US	Urban Arterial	Cornwall Rd	8 x 1.75 Box	N/A	50	100	-0.58	0.06	N	50.00	N/A	N/A	N	0.06	0.46	0.03	Y	0.06	0.46	0.03	Y
	Reach 1 US	Urban Arterial	DS of CNR Crossing	Twin 1.8 m diameter CSP	N/A	5	50	-2.38	-0.02	N	5.00	N/A	N/A	N	0.02	0.72	0.01	Y	0.02	0.79	0.02	Y
	Reach 1 US	Urban Arterial	CNR Crossing	3.3 x 1.5 Box	N/A	N/A	50	-2.30	-0.02	N	N/A	N/A	N/A	N	0.02	0.44	0.01	Y	0.02	0.55	0.01	Y

				Potential Channel/Structural Improvements		MTO Criteria									MNRF Criteria							
				Existing	Proposed	Existing					Proposed				MNRF Criteria				MNRF Criteria			
	Reach ID	Road Classification	Location	Existing Structure	Largest Structure Possible	Largest Storm Conveyed (Without Overtopping)	Design Storm	Clearance (m)	FB (m)	Pass MTO Criteria (Y/N)	Largest Storm Conveyed (Without Overtopping)	Clearance (m)	FB (m)	Pass MTO Criteria (Y/N)	Overtopping Depth (m)	Velocity	Depth x Velocity	Pass MNRF Criteria (Y/N)	Overtopping Depth (m)	Velocity	Depth x Velocity	Pass MNRF Criteria (Y/N)
Wedgewood Creek	Reach 1 DS	Urban Arterial	Lakeshore	3.8 x 1.9 CONSPAN Arch	14.6 x 3.05 CONSPAN Arch	2	50	-1.58	-0.54	N	25.00	-1.19	-0.15	N	0.54	1.00	0.54	**N**	0.27	1.32	0.36	Y
	Reach 1 DS	Urban Arterial	Warren Dr. Park	4.2 x 1.5 CONSPAN Arch	7.3 x 1.52 CONSPAN Arch	N/A	50	-0.53	-0.44	N	N/A	-0.47	-0.38	N	0.44	0.80	0.35	Y	0.38	0.83	0.32	Y
	Reach 1 DS	Urban Arterial	Wedgewood Dr	5.5 x 1.5 CONSPAN Arch	7.3 x 1.52 CONSPAN Arch	N/A	50	-0.37	-0.49	N	2.00	-0.32	-0.44	N	0.49	0.78	0.38	Y	0.44	0.80	0.35	Y
	Reach 1 DS	Urban Arterial	Devon Rd	Twin 4.3 x 2 CONSPAN Arch	N/A	50	100	-0.71	-0.01	N	100.00	-0.71	-0.01	N	0.01	0.22	0.00	Y	0.01	0.22	0.00	Y
	Reach 4	Urban Arterial	Drummond Rd	1.7 x 1.15 CONSPAN Arch	N/A	N/A	50	-2.07	-0.32	N	N/A	-2.07	-0.32	N	0.32	0.69	0.22	Y	0.32	0.69	0.22	Y
	Reach 2	Urban Arterial	Cumnock Crescent	0.6 m diameter CSP	N/A	N/A	50	-1.76	-0.31	N	N/A	-1.76	-0.31	N	0.31	0.62	0.19	Y	0.31	0.62	0.19	Y
	Reach 2	Urban Arterial	Morrison Rd	1.2 m diameter CSP	N/A	5	50	-0.77	-0.13	N	5.00	-0.77	-0.13	N	0.13	0.41	0.05	Y	0.13	0.41	0.05	Y
	Reach 3	Urban Arterial	Morrison Rd Conc. Bridge	5.7 x 1.5 Box	6.4 x 1.9 Box	100	50	0.06	1.04	N	100.00	0.06	1.04	N	N/A	N/A	N/A	Y	N/A	N/A	N/A	Y
	Reach 3	Urban Arterial	Cornwall Road	5.7 x 1.5 Box	N/A	100	50	0.00	0.45	N	100.00	0.00	0.45	N	N/A	N/A	N/A	Y	N/A	N/A	N/A	Y
	Reach 1 US	Urban Arterial	Duncan Rd	2.45 x 1.8 CONSPAN Arch	N/A	N/A	50	-1.67	-0.57	N	N/A	-1.67	-0.57	N	0.57	0.99	0.56	**N**	0.57	1.02	0.58	N
	Reach 1 US	Urban Arterial	Rd. N of Pond (Cornwall Rd)	Twin 1.75 x 1.2 Box	7.3 x 1.52 CONSPAN Arch	N/A	50	-1.08	-0.58	N	5.00	-0.92	-0.42	N	0.58	0.95	0.55	**N**	0.46	0.98	0.45	N
	Reach 1 US	Urban Arterial	CN Railway	3.1 x 2 Box	N/A	2	50	-2.48	-1.04	N	2.00	-2.48	-1.04	N	1.04	1.17	1.22	**N**	1.04	1.17	1.22	N
	Reach 1 US	Urban Arterial	CN Railway 1993 Culv	3.1 x 2 Box	N/A	2	50	-1.40	-0.43	N	2.00	-1.40	-0.43	N	0.43	1.25	0.54	**N**	0.43	1.25	0.54	N
	Reach 1 US	Urban Arterial	Royal Windsor Dr	1.9 x 1.1 Box	N/A	N/A	50	-1.04	-0.94	N	N/A	-1.04	-0.94	N	0.94	1.25	1.18	**N**	0.94	1.25	1.18	N

Appendix F

Detailed Hydraulic Results

□□□□R□□ □ān□M□rri□□n□□□

Ri□□r	R□a□□	Ri□□r □□a	□r□i□□	□ □□□a□	Min □□ □□	W□□□□□□	□ri□W□□□	□□G□□□□	□□G□□□□□	□□□□□n□	□□w □r□a	□□□Wid□□	□r□□d□ □ □□□
				□□ □□□□	□□ □	□□ □	□□ □	□□ □	□□ □□ □	□□ □□□	□□ □□□	□□ □	
M□rri□□n□a□□	R□a□□□	□□□□□□□□	□□	□□5	□□5□□□	□□□□□□	□□□□□□	□□□□5□	□□□□□□□□	□□□□	□□□□	□□□□	□□□□
M□rri□□n□a□□	R□a□□□	□□□□□□□□	5□	□□□□	□□5□□□	□□□□□□	□□□□□□	□□□□□□	□□□□□□□□	□□□□	□55	5□□□	□□□□
M□rri□□n□a□□	R□a□□□	□□□□□□□□	□□□	□□□□	□□5□□□	□□□□5□	□□□□5□	□□□□□□	□□□□5□□	□□□5	□□□□	5□□□	□□□□
M□rri□□n□a□□	R□a□□□	□□□□□□□□	□5□	□□□□	□□5□□□	□□□□5□	□□□□5□	□□□□□□	□□□5□□□	□□□□	□□□□	□□□□	□□□□
M□rri□□n□a□□	R□a□□□	□□□□□□□□	5□□	5□□□	□□5□□□	□□□□□□	□□□□□□	□□□□□□	□□□5□□□	□□□□	□□□□	□□□□	□□□□
M□rri□□n□a□□	R□a□□□	□□□□□□□□	□□□□	□□□□	□□5□□□	□□□□□□	□□□□□□	□□□□□□	□□□□□□□□	□□□□	□□□□	□□□□	□□□□
M□rri□□n□a□□	R□a□□□	□□□□□□□□	R□gi□na□	□5□	□□5□□□	□□□□□5	□□□□□5	□□□□□□	□□□□□5□	□□□□	□□□□	5□□□	□□□□
M□rri□□n□a□□	R□a□□□	□□□□□□□□	□□	□□□□	□□□□□□	□□5□□□	□□□□□□	□□5□□□	□□□□□□□□	□□□□	□□□□	□□□□	□□□□
M□rri□□n□a□□	R□a□□□	□□□□□□□□	5□	□□□□	□□□□□□	□□5□□□	□□□□□□	□□5□□□	□□□□□□□□	□□□□	□□□□	□□□□	□□□□
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Appendix G

Erosion Threshold Assessment for Midtown Area

Erosion Threshold Analysis DRAFT
Lower Morrison and Lower Wedgewood Creeks
Town of Oakville

Submitted to:

Wood Environment & Infrastructure Solutions Inc.
3450 Harvester Road, Suite 100
Burlington, ON L7N 3W5

January 22, 2019

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Erosion Threshold Analysis
Lower Morrison and Lower Wedgewood Creeks
Town of Oakville

Erosion threshold analysis has been undertaken for Lower Morrison and Lower Wedgewood Creeks as support for midtown Oakville stormwater and flood mitigation studies. The selected locations for threshold analysis are based on existing catchment modelling nodes and were predetermined in discussion between Conservation Halton, Wood Environment & Infrastructure, and Town of Oakville staff. Study site locations are shown in **Figures 1** and **2**.

Figure 1: Lower Morrison Creek study reaches

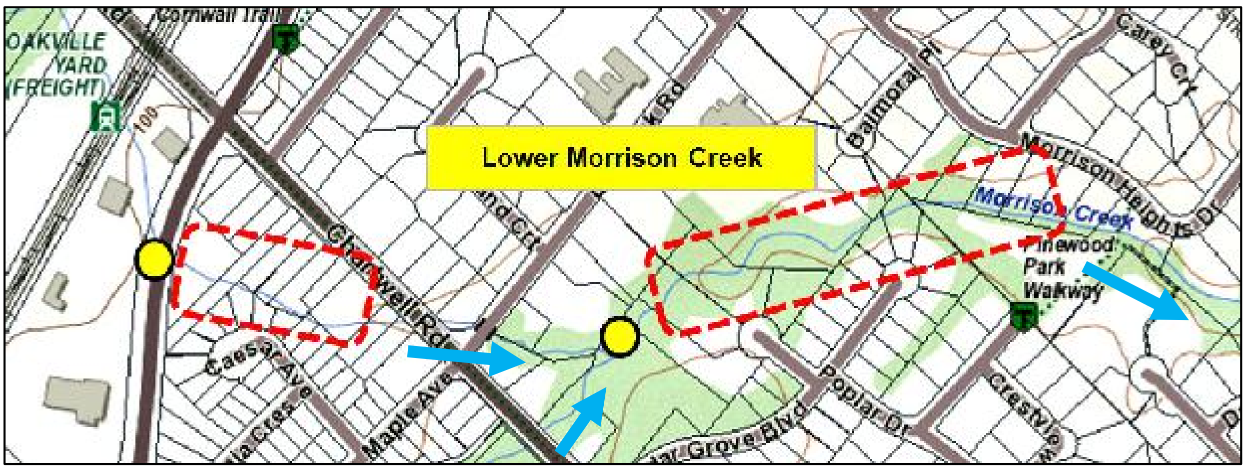
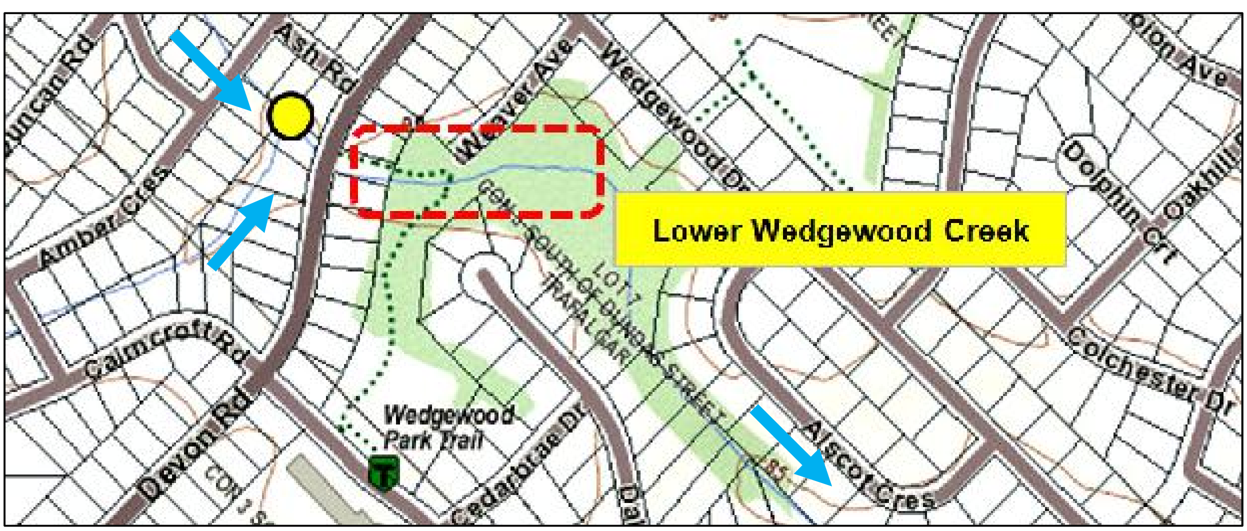


Figure 2: Lower Wedgewood Creek study reach



Analysis has been done based on field review of channel sensitivity and detailed cross-section surveys of the selected locations. Field measurements were used for erosion threshold modelling and results have been summarized for consideration in stormwater management scenarios.

Study Area Summary

The respective drainage area and stream order for each study reach is:

Lower Morrison Creek upstream reach, 70ha, 1st order
Lower Morrison Creek downstream reach, 180ha, 2nd order
Lower Wedgewood Creek, 260ha, 2nd order

The study reaches fall within the Iroquois Plain physiographic region, with each catchment consisting of a diverse mix of urban land uses including low density residential, commercial, industrial, rail corridor, and highway corridor. Each specific study site exists within a mix of residential and linear park land uses. Riparian areas are defined by moderate to high density groundcover and lowland shrub thicket to mature forest canopy. The upstream reach of Lower Morrison Creek flows through a heterogeneous mix of sediment types biased to smaller gravel, sand and cohesive clay-silt. The downstream reach of Lower Morrison Creek and the reach of Lower Wedgewood Creek have made shallow incision contact with underlying sedimentary bedrock and these sites are biased to gravel and cobble mixes of weathered shale and limestone. These reaches have characteristically wider and shallower bankfull channel definition than the lower width to depth ratio of the upper reach of Lower Morrison Creek. The wide shallow conditions and bed pavement result in relatively good channel stability in the downstream reach of Lower Morrison and in Lower Wedgewood Creek. By comparison the upstream reach of Lower Morrison Creek is experiencing combined incision and widening through the finer sediments and displays lower stability under existing conditions.

Erosion Threshold Analysis

Erosion threshold analysis proceeded as a detailed confirmation exercise of the observed channel stability conditions. Modelling analysis was undertaken using the five representative cross-section surveys made over approximately 50m of channel length per location. Backwater influences caused by organic debris were avoided. Channel forming flow lines, fallen and matted vegetation lines where visible, and well defined sediment stain lines were used as field indicators to identify cross-section width under a variety of conditions. Channel geometry was measured laterally at each cross-section and the longitudinal profile was shot and subsequently compared to topographic mapping. Channel bed substrates were measured through random-step Wolman pebble counts and recorded using the Wentworth sediment distribution scale. Geomorphic open channel flow models were created for each cross-section location. Each model required input of channel bed substrate data, cross-section dimensions, gradient, and bank geometry. Model calculation was done for a range of hydraulic geometry, flow condition, and sediment transport parameters. Erosion indicators and thresholds were reviewed from each model. **Table 1** presents the threshold criteria used for this analysis based on small watercourse channel typology which displays some influence of vegetation control.

Table 1: Critical stability threshold criteria

	low flow morphology		
	riffle	run	pool / glide
semi-alluvial firm to dense till channels	D_{84} pavement	D_{84} pavement or vegetation control*	D_{100} pavement or vegetation control*
alluvial cohesionless channels	D_{50} pavement	D_{50} pavement or vegetation control*	D_{84} pavement or vegetation control*

*vegetation control criteria varies depending on vegetation type and density
note: step-pool and cascade-step-pool channels require case by case study

The second row criteria are applied conservatively for this study case, based on soil and sediment conditions, and channel type. Conservative vegetation control criteria are identified as 40N m^{-2} for shear stress and 1.2m s^{-1} for channel velocity. Higher thresholds for vegetation control are common, approximately 80N m^{-2} and 1.8m s^{-1}, and viable under very high levels of vegetative encroachment. Channel run and pool sections that have partial vegetation control but are not judged to be fully protected are deemed to have thresholds of approximately 0.4-0.7m s^{-1} for velocities acting on pure sand to graded sediments, with shear stress values approximately 10-15N m^{-1} being acceptable when large volumes of sub coarse sand sized sediment forms both the channel pavement and subpavement (individual sand particle size values would be too low to be practical). More cohesive gradations of silt-clay or gradations that include some gravel with sand are deemed to have thresholds of approximately 30N m^{-2} and 0.8m s^{-1} respectively for shear stress and velocity (ranges summarized in Fischenich 2001). Several references vary on specific erosion threshold levels for sediment sizing, mixes of sizes, vegetative influence, entrenchment risk, and duration of flow effects, but notwithstanding the multiplicity of methods, the noted targets have proven practical over several similar studies and modelling efforts.

Subsequent checks were done to determine if a critical stability threshold discharge is reached under lower flow rates and stages than the channel forming or bankfull flow. Typically, the bankfull or active channel flow might not be dynamically stable, but a sub-bankfull rate is stable based on an integration of the testing criteria described above. The threshold is a target discharge representing a reach based average point at which channel instability is deemed to begin with rising flow stage and rising discharge, and conversely when instability stops with falling flow stage and falling discharge. This discharge then becomes the comparative flow regime target for detailed analysis of SWM hydrology.

The specific iterations in cross-section models were made to achieve velocity and tractive force levels below or improved towards the conservative range for vegetation control of channel banks, at velocity levels for D50 bed stability with at least a 1.0 ratio of critical velocity to boundary velocity, and at stable tractive force levels for D50 bed material within 5mm +/-. Stream power values were reviewed to confirm stable ranges under 400 watts m^{-1} (Sear et. al. 2003).

Detailed results of stable conditions modelling are appended after the existing conditions bankfull flow modelling. A summary model of the erosion threshold results is included after the stability test cross-section models. This model shows key variables between the respective bankfull and stability conditions. The summary model includes the breakdown of three conditions of dynamic stability, cautionary dynamic stability, and potential instability. The adjustments necessary to achieve stability reflect bump ups from cautionary dynamic stability to full dynamic stability and from unstable to cautionary dynamic stability or full dynamic stability, with an averaged final condition judged to be a realistic stable regime in the watercourse.

The modelling exercise confirmed that the downstream reach of Lower Morrison Creek is deemed stable under existing bankfull flows while each of the upstream reach of Lower Morrison and the reach of Lower Wedgewood required adjustment to achieve stability. **Table 2** shows the determined bankfull or channel forming flow and the dynamic stability flow adjustment, specifically for Lower Morrison downstream and Lower Wedgewood.

Table 2: Cross-section results summary

	bankfull Q cms	stability Q cms
Lower Morrison Creek upstream	0.89	0.24
Lower Morrison Creek downstream	1.41	1.41
Lower Wedgewood Creek	1.70	1.47

The upstream reach of Lower Morrison required stage adjustments of 12 to 16cm to enhance particle size based stability. Specifically, the dynamic stability target of velocity equal to 0.8m s^{-1}, as described above for cohesive clay-silt dominant gradations that include some larger particles, was used as the primary check. Given the relative small size of the channel, the reductions in stage result in a significant percent change in flow rate with the stability flow being 27% of bankfull.

The stage adjustments made for two sections on Lower Wedgewood Creek were 6cm and 7cm. These changes improved the particle based stability at section 4 and the vegetation control stability at section 5. The adjusted stability flow rate is 86% of the bankfull rate, representing only a moderate difference.

Conclusions

Erosion threshold analysis has been undertaken for Lower Morrison and Lower Wedgewood Creeks as support for parallel studies of stormwater and flood mitigation in the midtown Oakville area. Field measurements used for erosion threshold modelling have produced results for consideration in stormwater management scenarios.

The methods and results presented in this report do not address future potential erosion caused by unforeseen circumstances (e.g. SWM pond failure, culvert failures, major debris jam scour, beaver dam construction/breaching, or combinations thereof, etc.). The results presented here are also contingent on long term preservation and maintenance of natural vegetation conditions within the respective corridors. The results are also contingent on maintenance of upstream drainage characteristics that do not adversely modify future flow regime.

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Lower Morrison Creek
Upstream Reach

Bankfull Conditions

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GEO-X v.5.1 Geomorphic Cross-section Analysis Model

Project: Erosion Threshold Analysis
Midtown Oakville
Lower Morrison Creek - upstream Section 1 - existing bankfull flow

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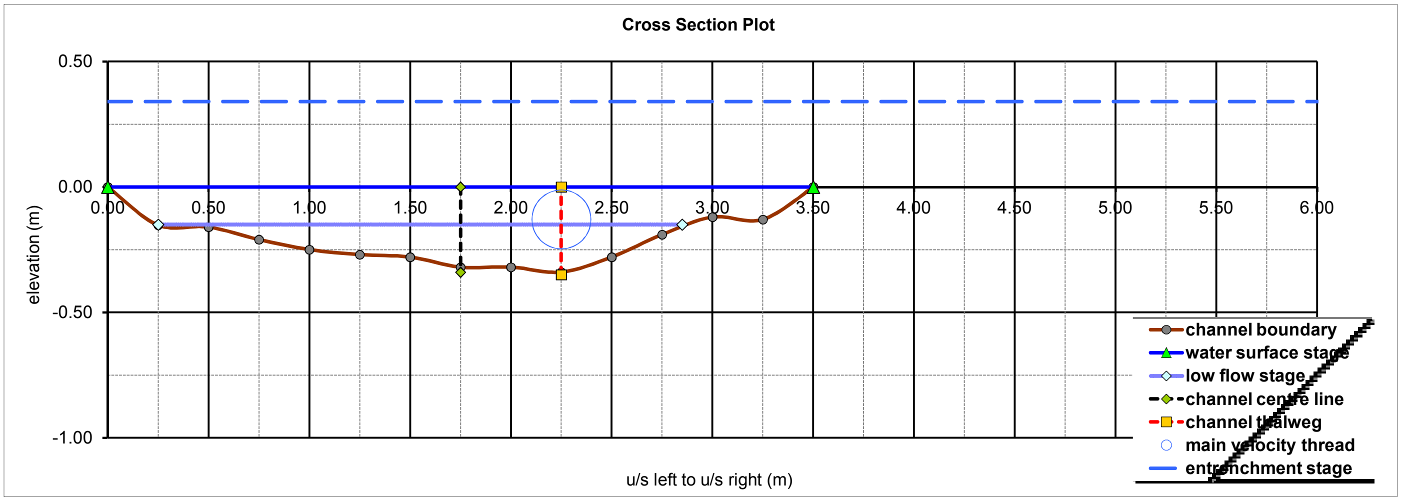

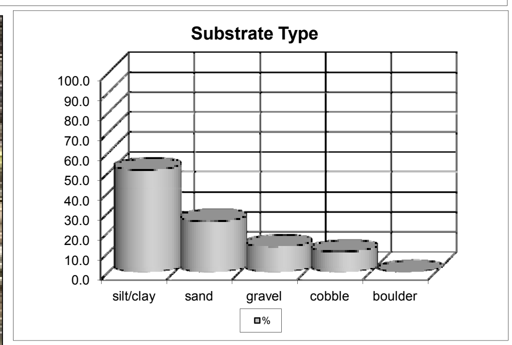

Morphology Type	
cascade	
step	
riffle	
run	
glide	
pool	●
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	0.76
R (m)	0.21
TW (m)	3.50
WP (m)	3.62
max d (m)	0.34
mean d (m)	0.22
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	8.35
ff V mean/V*	7.69
ff D_{84}	8.17
ff mean	7.93
ROUGH BED	

Hydraulic Ratios	
ER max d	4.29
r_c / TW	
TW / Lf_w	1.35
TW/max d	10.3
TW/mean d	16.2

Sediment Transport Mode

			w_s (m s^{-1})	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.001	0.04	YES	YES	YES	YES
V_* (m s^{-1})	0.076	D_{50}	0.003	0.09	YES	YES	YES	YES
		D_{84}	0.733	23.38	NO	NO	NO	NO

Section Data

ER_e (m)	0.34	ER stations L / R	-5.00	10.00	TW ck
WS_e (m)	0.000	WS stations L / R	0.00	3.50	3.50
Lf_e (m)	-0.150	Lf stations L / R	0.25	2.85	
W_{fp} (m)	15.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.35	2.25	
E_g (m m^{-1})	0.0140				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})		D_{30}	D_{50}	D_{84}
			T_*	737.9	492.0	1.2
B3	0.0018	0.0019	saltation	YES	YES	NO
C3	0.0002	0.0003	rolling	YES	YES	YES
C4	0.0062	0.0067	Ø	NO	NO	NO

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.02	0.04	0.06	25.00	160.00
Stability Design Targets (mm)					
τ_{cr} (N m^{-2})				24.25	155.20
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} (kg m^{-2})	2.92		
τ_{calc} (N m^{-2})	28.63		
τ D_{crit} (gr-co) (mm)	29.52		
D_{50} V_c (vcs +) (m s^{-1})	0.04	0.05	
D_{84} V_c (vcs +) (m s^{-1})	0.78	0.94	

Substrate Type (%)

silt/clay	sand	gravel	cobble	boulder
51.3	25.6	12.8	10.3	0.0

Bank Data	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

Flow Regime Strickler method		Flow Regime Limerinos method	
Q (cms)	0.894	Q (cms)	
V (m s^{-1})	1.18	V (m s^{-1})	
n	0.035	n	
Fr	0.81	*Fr*	
D_c rectangular (m)	0.19	D_c rectangular (m)	
D_c trapezoidal (m)	0.31	D_c trapezoidal (m)	
D_c triangular (m)	0.45	D_c triangular (m)	
D_c parabolic (m)	0.30	D_c parabolic (m)	
D_c mean (m)	0.31	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	122.64	Ω (watts m^{-1})	
ω_a (watts m^{-2})	33.88	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	9.68	ω_a/TW (watts m^{-1})	
*Re**	0.1	*Re**	
Re	216599	*Re*	
turbulence	LOW	turbulence	

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

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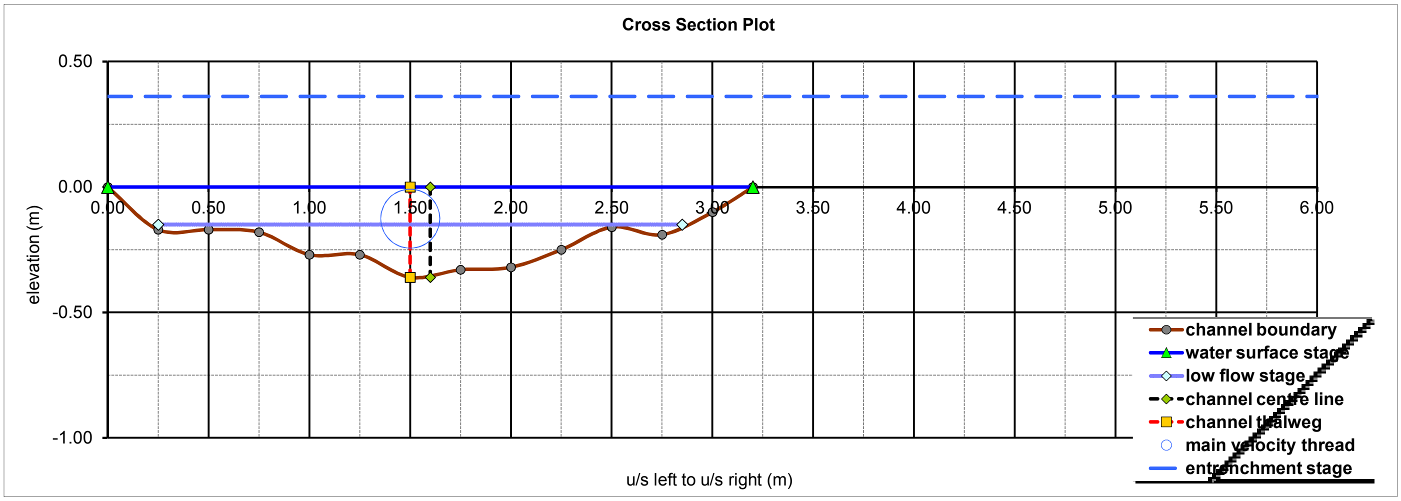
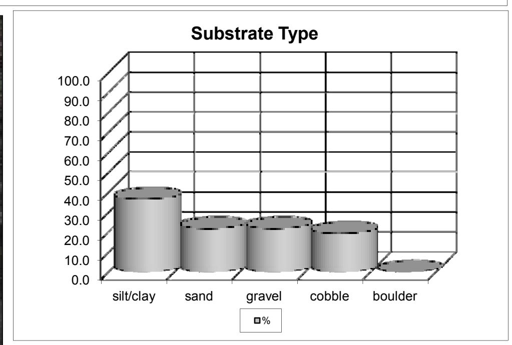
Project: Erosion Threshold Analysis
Block 60 East MESP
Lower Morrison Creek - upstream Section 2 - - existing bankfull flow





Morphology Type	
cascade	
step	
riffle	
run	●
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	0.69
R (m)	0.21
TW (m)	3.20
WP (m)	3.35
max d (m)	0.36
mean d (m)	0.22
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	2.42
ff V mean/V*	6.20
ff D_{84}	5.13
ff mean	5.67
ROUGH BED	

Hydraulic Ratios	
ER max d	4.69
r_c / TW	
TW / Lf_w	1.23
TW/max d	8.9
TW/mean d	14.8

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.003	0.09	YES	YES	YES	YES
V_* ($m\ s^{-1}$)	0.084	D_{50}	0.071	2.07	NO	NO	YES	YES
		D_{84}	1.353	39.44	NO	NO	NO	NO

Section Data

ER_e (m)	0.36	ER stations L / R	-5.00	10.00	TW ck
WS_e (m)	0.000	WS stations L / R	0.00	3.20	3.20
Lf_e (m)	-0.150	Lf stations L / R	0.25	2.85	
W_{fp} (m)	15.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.36	1.50	
E_g ($m\ m^{-1}$)	0.0170				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} ($kg\ sec^{-1}$)	Limerinos Q Q_{sb} ($kg\ sec^{-1}$)		D_{30}	D_{50}	D_{84}
			T_*	589.2	70.7	0.4
B3	0.0018	0.0017	saltation	YES	YES	NO
C3	0.0002	0.0001	rolling	YES	YES	NO
C4	0.0062	0.0055	Ø	NO	NO	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.03	0.06	0.50	85.00	190.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)				82.45	184.30
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime

Strickler method		Limerinos method	
Q (cms)	0.891	Q (cms)	
V ($m\ s^{-1}$)	1.29	V ($m\ s^{-1}$)	
n	0.035	n	
Fr	0.89	*Fr*	
D_c rectangular (m)	0.20	D_c rectangular (m)	
D_c trapezoidal (m)	0.32	D_c trapezoidal (m)	
D_c triangular (m)	0.45	D_c triangular (m)	
D_c parabolic (m)	0.30	D_c parabolic (m)	
D_c mean (m)	0.32	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	148.50	Ω (watts m^{-1})	
ω_a (watts m^{-2})	44.30	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	13.84	ω_a/TW (watts m^{-1})	
*Re**	0.7	*Re**	
Re	233235	*Re*	
turbulence	LOW	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} ($kg\ m^{-2}$)	3.50		
τ_{calc} ($N\ m^{-2}$)	34.29		
$\tau\ D_{crit}$ (gr-co) (mm)	35.35		
$D_{50}\ V_c$ (vcs +) ($m\ s^{-1}$)	0.11	0.12	
$D_{84}\ V_c$ (vcs +) ($m\ s^{-1}$)	1.43	1.58	

Substrate Type (%)

silt/clay	sand	gravel	cobble	boulder
36.6	22.0	22.0	19.5	0.0

Bank Data	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

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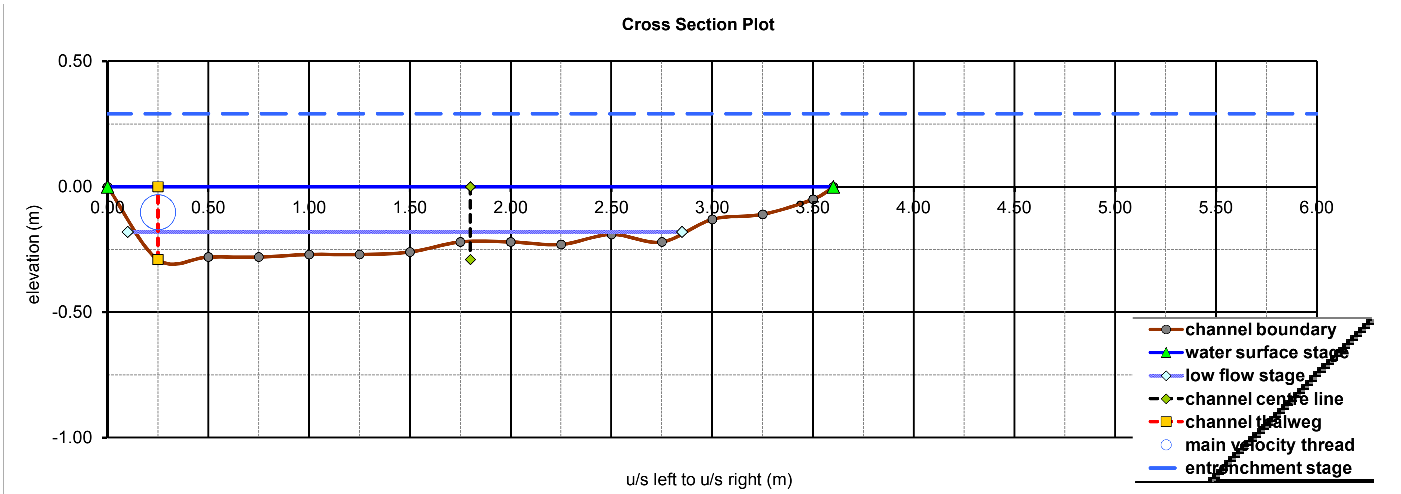
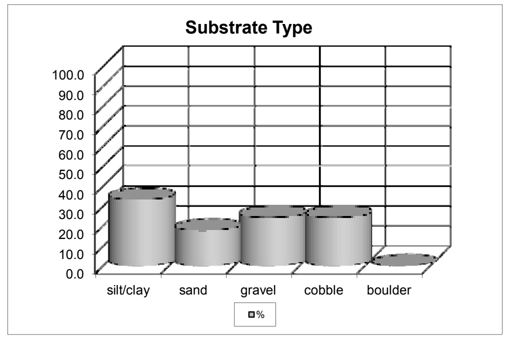
Project: Erosion Threshold Analysis
Midtown Oakville
Lower Morrison Creek - upstream Section 3 - existing bankfull flow





Morphology Type	
cascade	
step	
riffle	
run	●
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	0.75
R (m)	0.20
TW (m)	3.60
WP (m)	3.78
max d (m)	0.29
mean d (m)	0.21
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	1.59
ff V mean/V*	5.68
ff D_{84}	4.10
ff mean	4.89
ROUGH BED	

Hydraulic Ratios	
ER max d	4.17
r_c / TW	
TW / Lf_w	1.31
TW/max d	12.4
TW/mean d	17.3

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.003	0.09	YES	YES	YES	YES
V_* ($m\ s^{-1}$)	0.077	D_{50}	0.126	3.98	NO	NO	NO	YES
		D_{84}	1.641	51.80	NO	NO	NO	NO

Section Data

ER_e (m)	0.29	ER stations L / R	-5.00	10.00	TW ck
WS_e (m)	0.000	WS stations L / R	0.00	3.60	3.60
Lf_e (m)	-0.180	Lf stations L / R	0.10	2.85	
W_{fp} (m)	15.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.29	0.25	
E_g ($m\ m^{-1}$)	0.0150				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} ($kg\ sec^{-1}$)	Limerinos Q Q_{sb} ($kg\ sec^{-1}$)		D_{30}	D_{50}	D_{84}
			T_*	502.3	30.1	0.2
B3	0.0018	0.0016	saltation	YES	YES	NO
C3	0.0002	0.0001	rolling	YES	YES	NO
C4	0.0062	0.0050	Ø	NO	NO	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.03	0.06	1.00	125.00	170.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)				121.25	164.90
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} ($kg\ m^{-2}$)	2.98		
τ_{calc} ($N\ m^{-2}$)	29.24		
$\tau\ D_{crit}$ (gr-co) (mm)	30.14		
$D_{50}\ V_c$ (vcs +) ($m\ s^{-1}$)	0.16	0.19	
$D_{84}\ V_c$ (vcs +) ($m\ s^{-1}$)	1.73	2.09	

Substrate Type (%)

silt/clay	sand	gravel	cobble	boulder
33.3	17.8	24.4	24.4	0.0

Bank Data

	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

Flow Regime

Strickler method		Limerinos method	
Q (cms)	0.891	Q (cms)	
V ($m\ s^{-1}$)	1.19	V ($m\ s^{-1}$)	
n	0.035	n	
Fr	0.83	*Fr*	
D_c rectangular (m)	0.19	D_c rectangular (m)	
D_c trapezoidal (m)	0.31	D_c trapezoidal (m)	
D_c triangular (m)	0.45	D_c triangular (m)	
D_c parabolic (m)	0.30	D_c parabolic (m)	
D_c mean (m)	0.31	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω ($watts\ m^{-1}$)	130.96	Ω ($watts\ m^{-1}$)	
ω_a ($watts\ m^{-2}$)	34.67	ω_a ($watts\ m^{-2}$)	
ω_a/TW ($watts\ m^{-1}$)	9.63	ω_a/TW ($watts\ m^{-1}$)	
*Re**	1.5	*Re**	
Re	206895	*Re*	
turbulence	LOW	turbulence	

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

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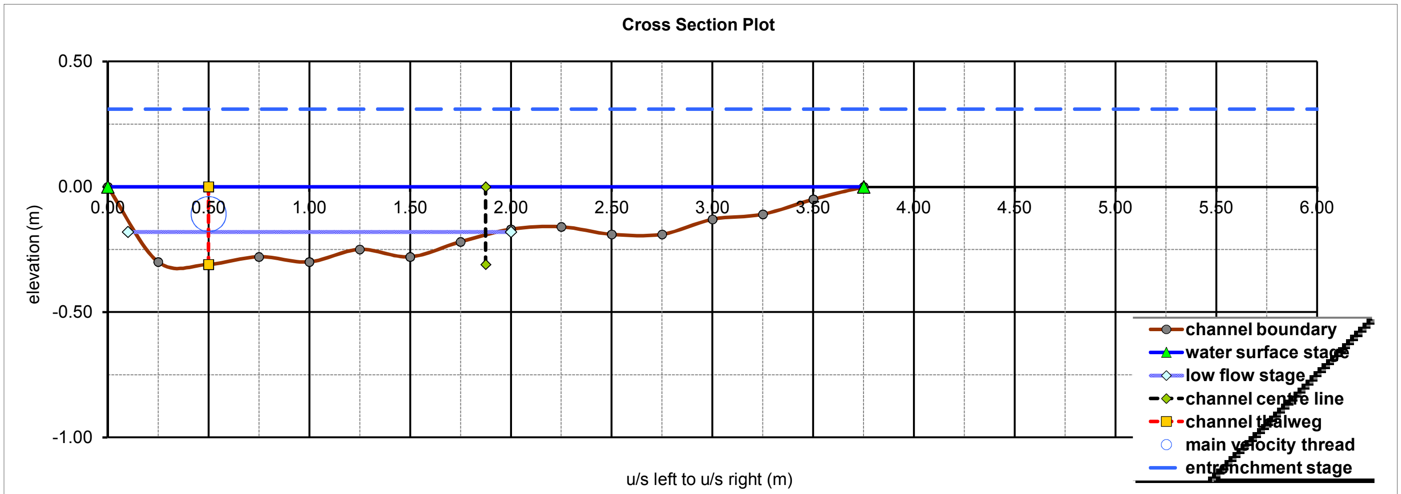
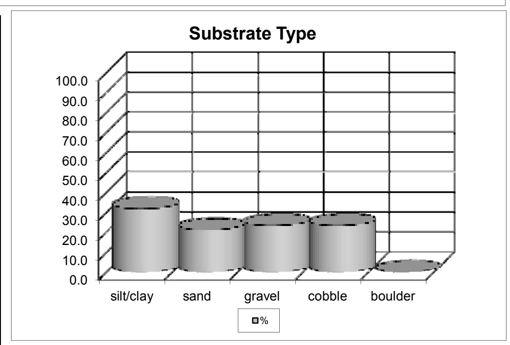
Project: Erosion Threshold Analysis
Midtown Oakville
Lower Morrison Creek - upstream Section 4 - existing bankfull flow





Morphology Type	
cascade	
step	
riffle	
run	●
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	0.74
R (m)	0.19
TW (m)	3.75
WP (m)	3.93
max d (m)	0.31
mean d (m)	0.20
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	1.97
ff V mean/V*	5.90
ff D_{84}	4.62
ff mean	5.26
ROUGH BED	

Hydraulic Ratios	
ER max d	4.00
r_c / TW	
TW / Lf_w	1.97
TW/max d	12.1
TW/mean d	19.1

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.003	0.09	YES	YES	YES	YES
V_* ($m\ s^{-1}$)	0.080	D_{50}	0.196	6.00	NO	NO	NO	YES
		D_{84}	1.431	43.77	NO	NO	NO	NO

Section Data

ER_e (m)	0.31	ER stations L / R	-5.00	10.00	TW ck
WS_e (m)	0.000	WS stations L / R	0.00	3.75	3.75
Lf_e (m)	-0.180	Lf stations L / R	0.10	2.00	
W_{fp} (m)	15.00	E_s sta. (Limerinos) L / R			
r_c (m)		E_s sta. (Strickler) L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.31	0.50	
E_g ($m\ m^{-1}$)	0.0170				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})		D_{30}	D_{50}	D_{84}
			T_*	534.8	16.0	0.3
B3	0.0018	0.0017	saltation	YES	YES	NO
C3	0.0002	0.0001	rolling	YES	YES	NO
C4	0.0062	0.0053	Ø	NO	NO	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.03	0.06	2.00	95.00	160.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)				92.15	155.20
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime

Strickler method		Limerinos method	
Q (cms)	0.890	Q (cms)	
V ($m\ s^{-1}$)	1.21	V ($m\ s^{-1}$)	
n	0.035	n	
Fr	0.87	*Fr*	
D_c rectangular (m)	0.18	D_c rectangular (m)	
D_c trapezoidal (m)	0.31	D_c trapezoidal (m)	
D_c triangular (m)	0.45	D_c triangular (m)	
D_c parabolic (m)	0.30	D_c parabolic (m)	
D_c mean (m)	0.31	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	148.25	Ω (watts m^{-1})	
ω_a (watts m^{-2})	37.68	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	10.05	ω_a/TW (watts m^{-1})	
*Re**	3.0	*Re**	
Re	198413	*Re*	
turbulence	LOW	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} (kg m^{-2})	3.18		
τ_{calc} (N m^{-2})	31.13		
τ D_{crit} (gr-co) (mm)	32.09		
D_{50} V_c (vcs +) ($m\ s^{-1}$)	0.22	0.26	
D_{84} V_c (vcs +) ($m\ s^{-1}$)	1.51	1.78	

Bank Data

	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

Substrate Type (%)

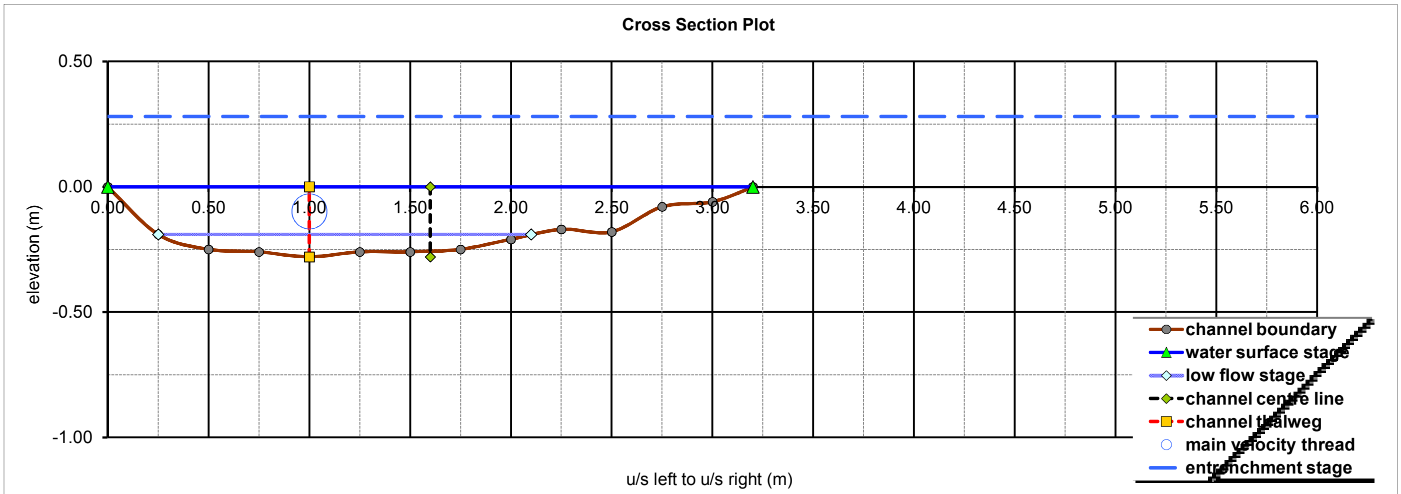
silt/clay	sand	gravel	cobble	boulder
31.9	21.3	23.4	23.4	0.0

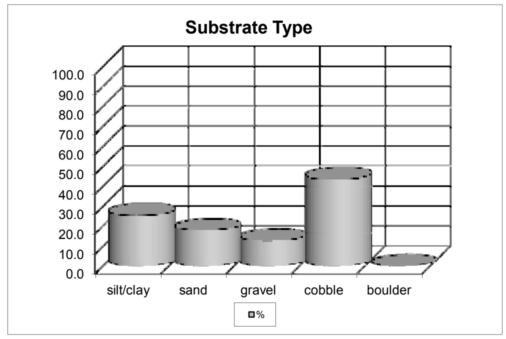
GEO-X v.5.1 Geomorphic Cross-section Analysis Model

AquaLogic

Project: Erosion Threshold Analysis
Midtown Oakville
Lower Morrison Creek - upstream Section 5 - existing bankfull flow

B. de Geus 05.11





Morphology Type		Hydraulic Geometry	
cascade		A (m^2)	0.61
step		*R* (m)	0.18
riffle	●	TW (m)	3.20
run		WP (m)	3.31
glide		max d (m)	0.28
pool		mean d (m)	0.19
thalweg out of phase	●	$E_{s\ (Limerinos)}$ (m) [+]	
		$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness		Hydraulic Ratios	
rr R/D_{84}	1.48	ER max d	4.69
ff V mean/V*	5.53	r_c / TW	
ff D_{84}	3.88	TW / Lf_w	1.73
ff mean	4.71	TW/max d	11.4
ROUGH BED		TW/mean d	16.8

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.032	0.81	NO	YES	YES	YES
V_* ($m\ s^{-1}$)	0.096	D_{50}	0.803	20.38	NO	NO	NO	NO
		D_{84}	1.641	41.64	NO	NO	NO	NO

Section Data

ER_e (m)	0.28	ER stations L / R	-5.00	10.00	TW ck
WS_e (m)	0.000	WS stations L / R	0.00	3.20	3.20
Lf_e (m)	-0.190	Lf stations L / R	0.25	2.10	
W_{fp} (m)	15.00	E_s sta. (Limerinos) L / R			
r_c (m)		E_s sta. (Strickler) L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.28	1.00	
E_g ($m\ m^{-1}$)	0.0250				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})		D_{30}	D_{50}	D_{84}
			T_*	186.6	1.6	0.4
B3	0.0018	0.0016	saltation	YES	NO	NO
C3	0.0002	0.0001	rolling	YES	YES	NO
C4	0.0062	0.0049	Ø	NO	NO	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.05	0.25	30.00	125.00	190.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)			29.10	121.25	184.30
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime Strickler method		Flow Regime Limerinos method	
Q (cms)	0.890	Q (cms)	
V ($m\ s^{-1}$)	1.46	V ($m\ s^{-1}$)	
n	0.035	n	
Fr	1.06	*Fr*	
D_c rectangular (m)	0.20	D_c rectangular (m)	
D_c trapezoidal (m)	0.32	D_c trapezoidal (m)	
D_c triangular (m)	0.45	D_c triangular (m)	
D_c parabolic (m)	0.30	D_c parabolic (m)	
D_c mean (m)	0.32	D_c mean (m)	
flow type	SUPERCRITICAL	flow type	
Ω (watts m^{-1})	218.07	Ω (watts m^{-1})	
ω_a (watts m^{-2})	65.91	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	20.60	ω_a/TW (watts m^{-1})	
*Re**	44.5	*Re**	
Re	235991	*Re*	
turbulence	HIGH	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} ($kg\ m^{-2}$)	4.62		
τ_{calc} ($N\ m^{-2}$)	45.25		
$\tau\ D_{crit}$ (gr-co) (mm)	46.64		
D_{50} V_c (vcs +) ($m\ s^{-1}$)	0.85	0.83	
D_{84} V_c (vcs +) ($m\ s^{-1}$)	1.73	1.70	

Bank Data

	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

Substrate Type (%)

silt/clay	sand	gravel	cobble	boulder
25.6	17.9	12.8	43.6	0.0

Lower Morrison Creek
Downstream Reach

Bankfull Conditions

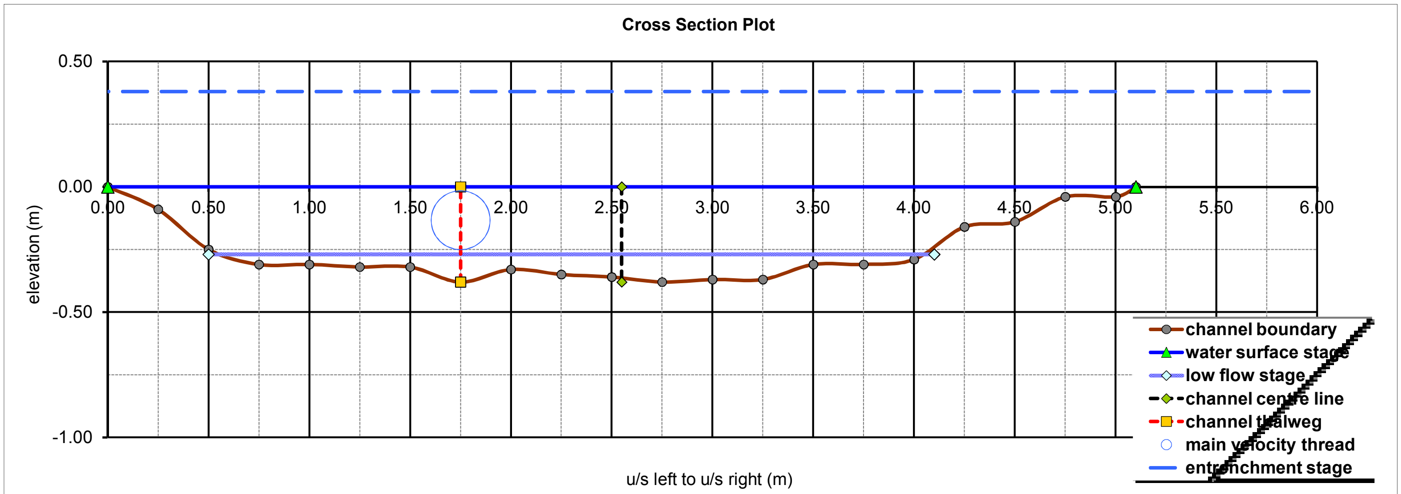
AquaLogic

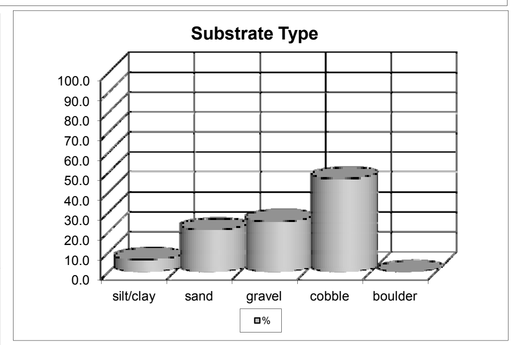
GEO-X v.5.1 Geomorphic Cross-section Analysis Model

AquaLogic

Project: Erosion Threshold Analysis
Midtown Oakville
Lower Morrison Creek - downstream Section 1 - existing bankfull flow

B. de Geus 05.11





Morphology Type	
cascade	
step	
riffle	
run	●
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	1.35
R (m)	0.26
TW (m)	5.10
WP (m)	5.25
max d (m)	0.38
mean d (m)	0.27
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	2.06
ff V mean/V*	6.14
ff D_{84}	4.70
ff mean	5.42
ROUGH BED	

Hydraulic Ratios	
ER max d	2.55
r_c / TW	
TW / Lf_w	1.42
TW/max d	13.4
TW/mean d	19.2

Sediment Transport Mode

			w_s (m s^{-1})	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.385	14.43	NO	NO	NO	NO
V_* (m s^{-1})	0.065	D_{50}	1.089	40.80	NO	NO	NO	NO
		D_{84}	1.641	61.52	NO	NO	NO	NO

Section Data

			L	R	TW ck
ER_e (m)	0.38	ER stations L / R	-3.00	10.00	
WS_e (m)	0.000	WS stations L / R	0.00	5.10	5.10
Lf_e (m)	-0.270	Lf stations L / R	0.50	4.10	
W_{fp} (m)	13.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.38	1.75	
E_g (m m^{-1})	0.0082				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})	T_*	D_{30}	D_{50}	D_{84}
				3.1	0.4	0.2
B3	0.0021	0.0019	saltation	YES	NO	NO
C3	0.0006	0.0003	rolling	YES	NO	NO
C4	0.0077	0.0064	Ø	NO	YES	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.20	7.00	55.00	125.00	170.00
Stability Design Targets (mm)					
τ_{cr} (N m^{-2})			53.35	121.25	164.90
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime

Strickler method		Limerinos method	
Q (cms)	1.414	Q (cms)	
V (m s^{-1})	1.04	V (m s^{-1})	
n	0.035	n	
Fr	0.65	*Fr*	
D_c rectangular (m)	0.20	D_c rectangular (m)	
D_c trapezoidal (m)	0.36	D_c trapezoidal (m)	
D_c triangular (m)	0.54	D_c triangular (m)	
D_c parabolic (m)	0.35	D_c parabolic (m)	
D_c mean (m)	0.36	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	113.60	Ω (watts m^{-1})	
ω_a (watts m^{-2})	21.63	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	4.24	ω_a/TW (watts m^{-1})	
*Re**	77.0	*Re**	
Re	236134	*Re*	
turbulence	HIGH	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} (kg m^{-2})	2.12		
τ_{calc} (N m^{-2})	20.73		
τ D_{crit} (gr-co) (mm)	21.37		
D_{50} V_c (vcs +) (m s^{-1})	1.15	1.57	
D_{84} V_c (vcs +) (m s^{-1})	1.73	2.37	

Bank Data

	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

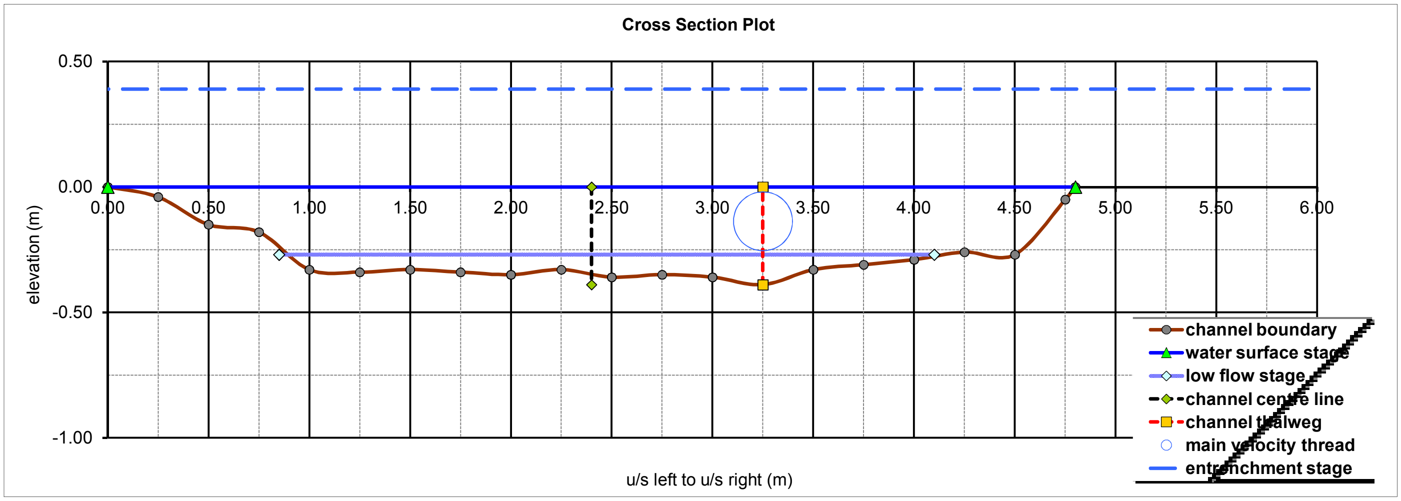
Substrate Type (%)

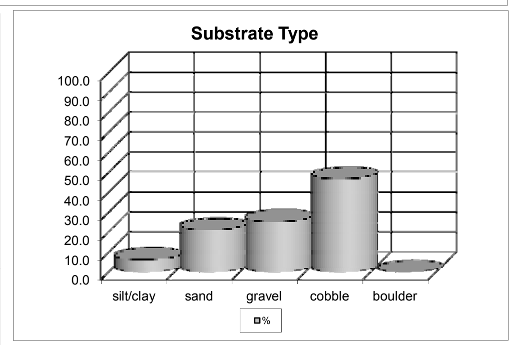
silt/clay	sand	gravel	cobble	boulder
6.4	21.3	25.5	46.8	0.0

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

Project: **Erosion Threshold Analysis**
Midtown Oakville
Lower Morrison Creek - downstream Section 2 - existing bankfull flow

B. de Geus 05.11





Morphology Type	
cascade	
step	
riffle	
run	●
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	1.34
R (m)	0.27
TW (m)	4.80
WP (m)	4.99
max d (m)	0.39
mean d (m)	0.28
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	2.14
ff V mean/V*	6.22
ff D_{84}	4.81
ff mean	5.51
ROUGH BED	

Hydraulic Ratios	
ER max d	2.71
r_c / TW	
TW / Lf_w	1.48
TW/max d	12.3
TW/mean d	17.3

Sediment Transport Mode						high	low	
			w_s (m s^{-1})	P	wash load	sus. load	sus. load	bedload
k	0.41	D_{30}	0.385	14.35	NO	NO	NO	NO
V_* (m s^{-1})	0.065	D_{50}	1.089	40.56	NO	NO	NO	NO
		D_{84}	1.641	61.16	NO	NO	NO	NO

Section Data					
ER_e (m)	0.39	ER stations L / R	-3.00	10.00	TW ck
WS_e (m)	0.000	WS stations L / R	0.00	4.80	4.80
Lf_e (m)	-0.270	Lf stations L / R	0.85	4.10	
W_{fp} (m)	13.00	E_s sta. (Limerinos) L / R			
r_c (m)		E_s sta. (Strickler) L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.39	3.25	
E_g (m m^{-1})	0.0080				

Bedload Transport Data							
	Strickler Q	Limerinos Q					
Rosgen	Q_{sb}	Q_{sb}			D_{30}	D_{50}	D_{84}
type	(kg sec^{-1})	(kg sec^{-1})		T_*	3.1	0.4	0.2
B3	0.0021	0.0019		saltation	YES	NO	NO
C3	0.0006	0.0003		rolling	YES	NO	NO
C4	0.0076	0.0065		Ø	NO	YES	YES

Substrate Gradation	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.20	7.00	55.00	125.00	170.00
Stability Design Targets (mm)					
τ_{cr} (N m^{-2})			53.35	121.25	164.90
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Erosion Thresholds		V_c / V_b Strickler	V_c / V_b Limerinos
τ_{calc} (kg m^{-2})	2.14		
τ_{calc} (N m^{-2})	20.98		
τ D_{crit} (gr-co) (mm)	21.62		
D_{50} V_c (vcs +) (m s^{-1})	1.15	1.55	
D_{84} V_c (vcs +) (m s^{-1})	1.73	2.34	

Substrate Type (%)				
silt/clay	sand	gravel	cobble	boulder
6.4	21.3	25.5	46.8	0.0

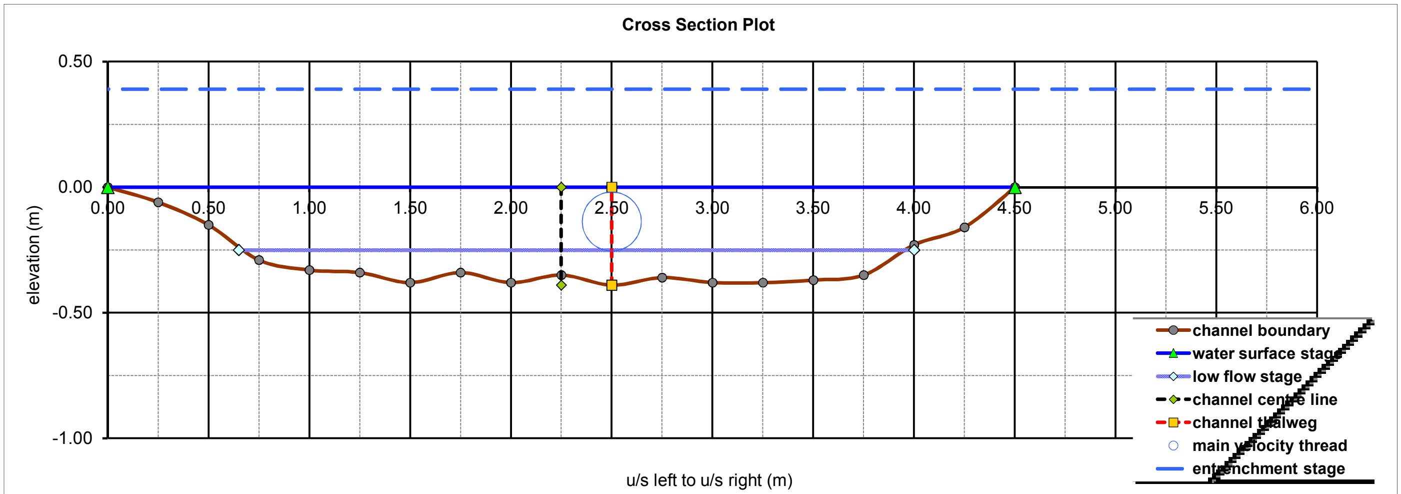
Bank Data	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

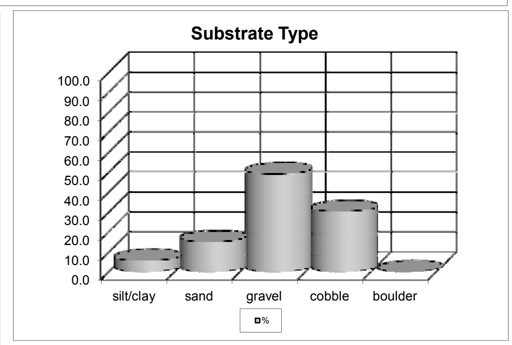
Flow Regime Strickler method		Flow Regime Limerinos method	
Q (cms)	1.410	Q (cms)	
V (m s^{-1})	1.06	V (m s^{-1})	
n	0.035	n	
Fr	0.64	*Fr*	
D_c rectangular (m)	0.21	D_c rectangular (m)	
D_c trapezoidal (m)	0.37	D_c trapezoidal (m)	
D_c triangular (m)	0.54	D_c triangular (m)	
D_c parabolic (m)	0.35	D_c parabolic (m)	
D_c mean (m)	0.37	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	110.57	Ω (watts m^{-1})	
ω_a (watts m^{-2})	22.16	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	4.62	ω_a/TW (watts m^{-1})	
*Re**	76.8	*Re**	
Re	247941	*Re*	
turbulence	HIGH	turbulence	

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

AquaLogic
B. de Geus 05.11

Project: Erosion Threshold Analysis
Midtown Oakvillr
Lower Morrison Creek - downstream Section 3 - existing bankfull flow





Morphology Type	
cascade	
step	
riffle	
run	●
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	1.31
R (m)	0.28
TW (m)	4.50
WP (m)	4.66
max d (m)	0.39
mean d (m)	0.29
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	2.16
ff V mean/V*	6.26
ff D_{84}	4.83
ff mean	5.54
ROUGH BED	

Hydraulic Ratios	
ER max d	2.89
r_c / TW	
TW / Lf_w	1.34
TW/max d	11.5
TW/mean d	15.5

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.356	13.10	NO	NO	NO	NO
V_* ($m\ s^{-1}$)	0.066	D_{50}	0.803	29.59	NO	NO	NO	NO
		D_{84}	1.674	61.65	NO	NO	NO	NO

Section Data

ER_e (m)	0.39	ER stations L / R	-3.00	10.00	TW ck
WS_e (m)	0.000	WS stations L / R	0.00	4.50	4.50
Lf_e (m)	-0.250	Lf stations L / R	0.65	4.00	
W_{fp} (m)	13.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.39	2.50	
E_g ($m\ m^{-1}$)	0.0078				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} ($kg\ sec^{-1}$)	Limerinos Q Q_{sb} ($kg\ sec^{-1}$)		D_{30}	D_{50}	D_{84}
			T_*	3.7	0.7	0.2
B3	0.0021	0.0019	saltation	YES	NO	NO
C3	0.0006	0.0003	rolling	YES	NO	NO
C4	0.0076	0.0065	Ø	NO	YES	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.50	6.00	30.00	130.00	170.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)			29.10	126.10	164.90
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime

Strickler method		Limerinos method	
Q (cms)	1.412	Q (cms)	
V ($m\ s^{-1}$)	1.08	V ($m\ s^{-1}$)	
n	0.035	n	
Fr	0.64	*Fr*	
D_c rectangular (m)	0.22	D_c rectangular (m)	
D_c trapezoidal (m)	0.37	D_c trapezoidal (m)	
D_c triangular (m)	0.54	D_c triangular (m)	
D_c parabolic (m)	0.35	D_c parabolic (m)	
D_c mean (m)	0.37	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω ($watts\ m^{-1}$)	107.90	Ω ($watts\ m^{-1}$)	
ω_a ($watts\ m^{-2}$)	23.13	ω_a ($watts\ m^{-2}$)	
ω_a/TW ($watts\ m^{-1}$)	5.14	ω_a/TW ($watts\ m^{-1}$)	
*Re**	41.5	*Re**	
Re	265463	*Re*	
turbulence	HIGH	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} ($kg\ m^{-2}$)	2.19		
τ_{calc} ($N\ m^{-2}$)	21.47		
τ D_{crit} (gr-co) (mm)	22.13		
D_{50} V_c (vcs +) ($m\ s^{-1}$)	0.85	1.13	
D_{84} V_c (vcs +) ($m\ s^{-1}$)	1.77	2.34	

Substrate Type (%)

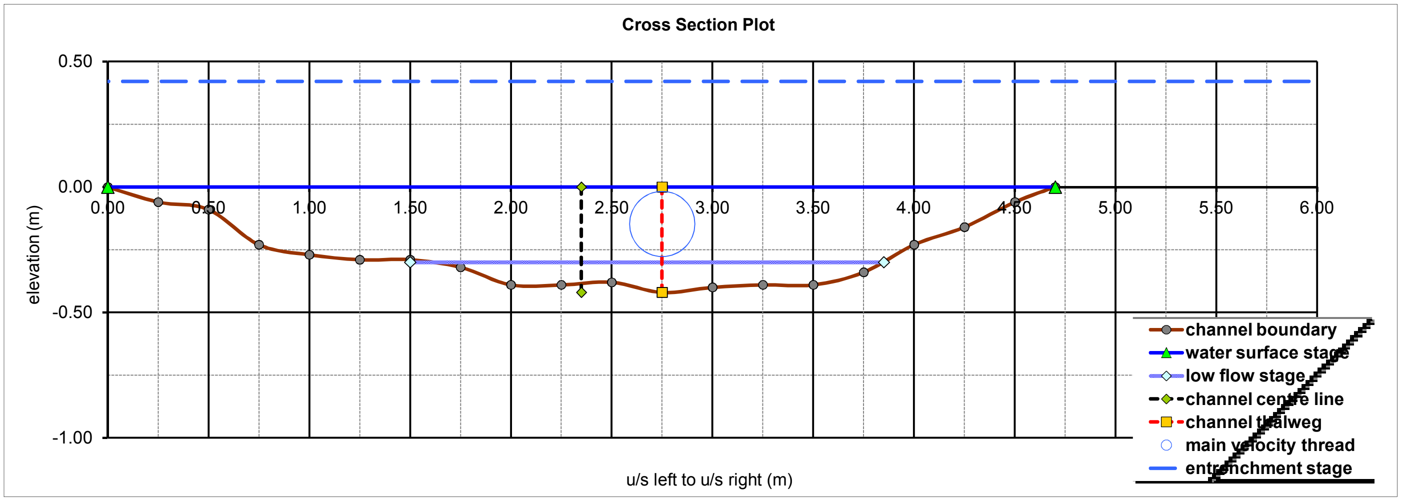
silt/clay	sand	gravel	cobble	boulder
5.7	15.1	49.1	30.2	0.0

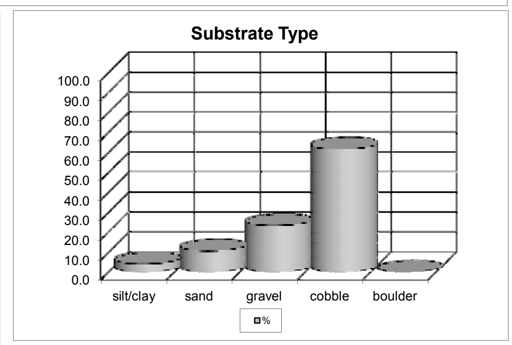
Bank Data	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

B. de Geus 05.11

Project: **Erosion Threshold Analysis**
Midtown Oakville
Lower Morrison Creek - downstream Section 4 - existing bankfull flow





Morphology Type	
cascade	
step	
riffle	●
run	
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	1.27
R (m)	0.26
TW (m)	4.70
WP (m)	4.83
max d (m)	0.42
mean d (m)	0.27
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	1.42
ff V mean/V*	5.71
ff D_{84}	3.77
ff mean	4.74
ROUGH BED	

Hydraulic Ratios	
ER max d	2.77
r_c / TW	
TW / Lf_w	2.00
TW/max d	11.2
TW/mean d	17.3

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.733	25.95	NO	NO	NO	NO
V_* ($m\ s^{-1}$)	0.069	D_{50}	1.353	47.90	NO	NO	NO	NO
		D_{84}	1.997	70.67	NO	NO	NO	NO

Section Data

ER_e (m)	0.42	ER stations L / R	-3.00	10.00	TW ck
WS_e (m)	0.000	WS stations L / R	0.00	4.70	4.70
Lf_e (m)	-0.300	Lf stations L / R	1.50	3.85	
W_{fp} (m)	13.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.42	2.75	
E_g ($m\ m^{-1}$)	0.0090				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} ($kg\ sec^{-1}$)	Limerinos Q Q_{sb} ($kg\ sec^{-1}$)		D_{30}	D_{50}	D_{84}
			T_*	1.0	0.3	0.1
B3	0.0021	0.0018	saltation	NO	NO	NO
C3	0.0006	0.0002	rolling	NO	NO	NO
C4	0.0077	0.0059	Ø	YES	YES	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	2.00	25.00	85.00	185.00	210.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)			82.45	179.45	203.70
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime Strickler method		Flow Regime Limerinos method	
Q (cms)	1.413	Q (cms)	
V ($m\ s^{-1}$)	1.11	V ($m\ s^{-1}$)	
n	0.035	n	
Fr	0.68	*Fr*	
D_c rectangular (m)	0.21	D_c rectangular (m)	
D_c trapezoidal (m)	0.37	D_c trapezoidal (m)	
D_c triangular (m)	0.54	D_c triangular (m)	
D_c parabolic (m)	0.35	D_c parabolic (m)	
D_c mean (m)	0.37	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	124.61	Ω (watts m^{-1})	
ω_a (watts m^{-2})	25.80	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	5.49	ω_a/TW (watts m^{-1})	
*Re**	118.4	*Re**	
Re	256544	*Re*	
turbulence	HIGH	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} ($kg\ m^{-2}$)	2.37		
τ_{calc} ($N\ m^{-2}$)	23.25		
$\tau\ D_{crit}$ (gr-co) (mm)	23.97		
D_{50} V_c (vcs +) ($m\ s^{-1}$)	1.43	1.84	
D_{84} V_c (vcs +) ($m\ s^{-1}$)	2.11	2.71	

Substrate Type (%)

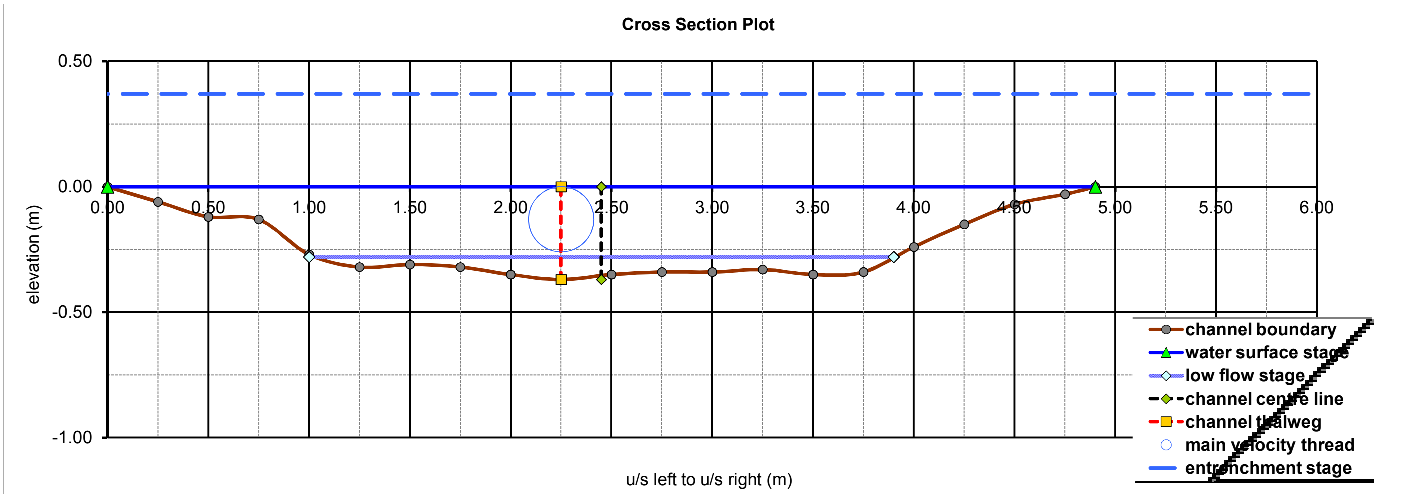
silt/clay	sand	gravel	cobble	boulder
4.3	10.6	23.4	61.7	0.0

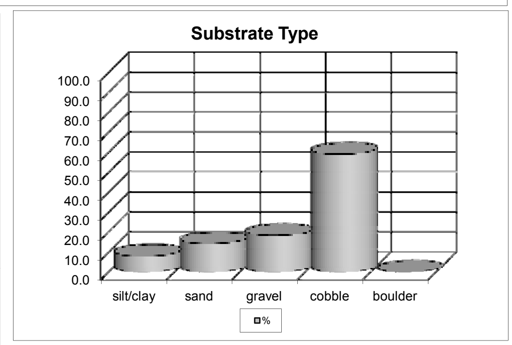
Bank Data	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

Project: Erosion Threshold Analysis
Midtown Oakville
Lower Morrison Creek - downstream Section 5 - existing bankfull flow

B. de Geus 05.11





Morphology Type	
cascade	
step	
riffle	●
run	
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	1.20
R (m)	0.24
TW (m)	4.90
WP (m)	5.01
max d (m)	0.37
mean d (m)	0.24
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	1.33
ff V mean/V*	5.36
ff D_{84}	3.58
ff mean	4.47
ROUGH BED	

Hydraulic Ratios	
ER max d	2.65
r_c / TW	
TW / Lf_w	1.69
TW/max d	13.2
TW/mean d	20.1

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.655	20.29	NO	NO	NO	NO
V_* ($m\ s^{-1}$)	0.079	D_{50}	1.353	41.90	NO	NO	NO	NO
		D_{84}	1.970	60.98	NO	NO	NO	NO

Section Data

					TW ck
ER_e (m)	0.37	ER stations L / R	-3.00	10.00	
WS_e (m)	0.000	WS stations L / R	0.00	4.90	4.90
Lf_e (m)	-0.280	Lf stations L / R	1.00	3.90	
W_{fp} (m)	13.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.37	2.25	
E_g ($m\ m^{-1}$)	0.0130				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})	T_*	D_{30}	D_{50}	D_{84}
				1.6	0.4	0.2
B3	0.0021	0.0018	saltation	NO	NO	NO
C3	0.0006	0.0002	rolling	YES	NO	NO
C4	0.0076	0.0059	Ø	NO	YES	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.20	20.00	85.00	180.00	230.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)		19.40	82.45	174.60	223.10
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} ($kg\ m^{-2}$)	3.10		
τ_{calc} ($N\ m^{-2}$)	30.38		
$\tau\ D_{crit}$ (gr-co) (mm)	31.32		
D_{50} V_c (vcs +) ($m\ s^{-1}$)	1.43	1.73	2.52
D_{84} V_c (vcs +) ($m\ s^{-1}$)	2.08	2.52	

Substrate Type (%)

silt/clay	sand	gravel	cobble	boulder
8.2	14.3	18.4	59.2	0.0

Bank Data	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

Flow Regime Strickler method		Flow Regime Limerinos method	
Q (cms)	1.411	Q (cms)	
V ($m\ s^{-1}$)	1.18	V ($m\ s^{-1}$)	
n	0.037	n	
Fr	0.76	*Fr*	
D_c rectangular (m)	0.21	D_c rectangular (m)	
D_c trapezoidal (m)	0.37	D_c trapezoidal (m)	
D_c triangular (m)	0.54	D_c triangular (m)	
D_c parabolic (m)	0.36	D_c parabolic (m)	
D_c mean (m)	0.37	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	179.72	Ω (watts m^{-1})	
ω_a (watts m^{-2})	35.84	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	7.31	ω_a/TW (watts m^{-1})	
*Re**	127.0	*Re**	
Re	246758	*Re*	
turbulence	HIGH	turbulence	

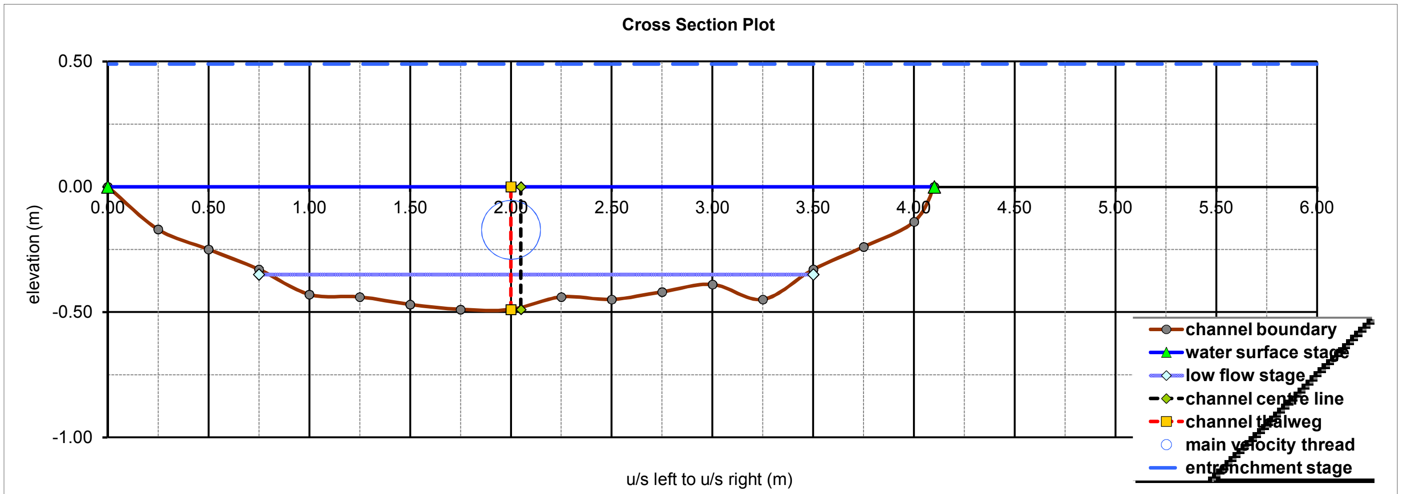
Lower Wedgewood Creek

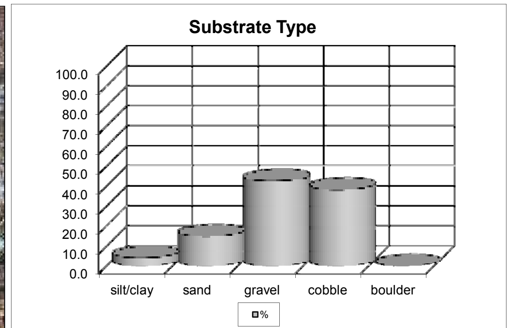
Bankfull Conditions

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

B. de Geus 05.11

Project: Erosion Threshold Analysis
Midtown Oakville
Lower Wedgewood Creek - Section 1 - existing bankfull flow





Morphology Type		Hydraulic Geometry	
cascade		A (m^2)	1.47
step		*R* (m)	0.34
riffle		TW (m)	4.10
run		WP (m)	4.35
glide		max d (m)	0.49
pool	●	mean d (m)	0.36
thalweg out of phase		$E_{s\ (Limerinos)}$ (m) [+]	
		$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness		Hydraulic Ratios	
rr *R*/D_{84}	2.82	ER max d	2.44
ff V mean/V*	6.72	r_c / TW	
ff D_{84}	5.54	TW / Lf_w	1.49
ff mean	6.13	TW/max d	8.4
ROUGH BED		TW/mean d	11.4

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.438	15.51	NO	NO	NO	NO
V_* ($m\ s^{-1}$)	0.069	D_{50}	0.984	34.87	NO	NO	NO	NO
		D_{84}	1.608	56.96	NO	NO	NO	NO

Section Data

					TW ck
ER_e (m)	0.49	ER stations L / R	-2.00	8.00	
WS_e (m)	0.000	WS stations L / R	0.00	4.10	4.10
Lf_e (m)	-0.350	Lf stations L / R	0.75	3.50	
W_{fp} (m)	10.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.49	2.00	
E_g ($m\ m^{-1}$)	0.0070				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} ($kg\ sec^{-1}$)	Limerinos Q Q_{sb} ($kg\ sec^{-1}$)	T_*	D_{30}	D_{50}	D_{84}
				2.7	0.5	0.2
B3	0.0022	0.0021	saltation	YES	NO	NO
C3	0.0008	0.0005	rolling	YES	NO	NO
C4	0.0084	0.0074	Ø	NO	YES	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.50	9.00	45.00	120.00	140.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)			43.65	116.40	135.80
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime

Strickler method		Limerinos method	
Q (cms)	1.703	Q (cms)	
V ($m\ s^{-1}$)	1.16	V ($m\ s^{-1}$)	
n	0.035	n	
Fr	0.62	*Fr*	
D_c rectangular (m)	0.26	D_c rectangular (m)	
D_c trapezoidal (m)	0.40	D_c trapezoidal (m)	
D_c triangular (m)	0.58	D_c triangular (m)	
D_c parabolic (m)	0.36	D_c parabolic (m)	
D_c mean (m)	0.40	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω ($watts\ m^{-1}$)	116.80	Ω ($watts\ m^{-1}$)	
ω_a ($watts\ m^{-2}$)	26.85	ω_a ($watts\ m^{-2}$)	
ω_a/TW ($watts\ m^{-1}$)	6.55	ω_a/TW ($watts\ m^{-1}$)	
*Re**	61.0	*Re**	
Re	343390	*Re*	
turbulence	HIGH	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	V_c / V_b Limerinos
τ_{calc} ($kg\ m^{-2}$)	2.37		
τ_{calc} ($N\ m^{-2}$)	23.22		
τ D_{crit} (gr-co) (mm)	23.93		
D_{50} V_c (vcs +) ($m\ s^{-1}$)	1.04	1.28	
D_{84} V_c (vcs +) ($m\ s^{-1}$)	1.70	2.10	

Bank Data

	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

Substrate Type (%)

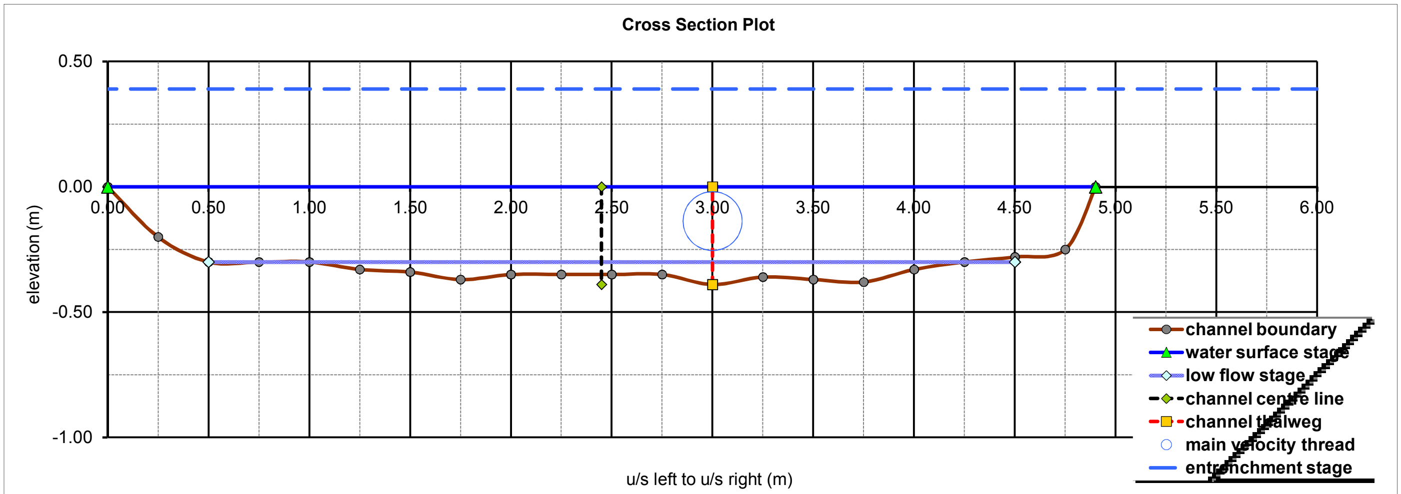
silt/clay	sand	gravel	cobble	boulder
4.3	14.9	42.6	38.3	0.0

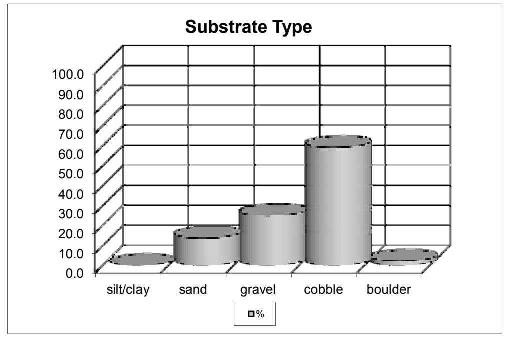
GEO-X v.5.1 Geomorphic Cross-section Analysis Model

AquaLogic

B. de Geus 05.11

Project: Erosion Threshold Analysis
Midtown Oakville
Lower Wedgewood Creek - Section 2 - existing bankfull flow





Morphology Type	
cascade	
step	
riffle	●
run	
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	1.54
R (m)	0.30
TW (m)	4.90
WP (m)	5.15
max d (m)	0.39
mean d (m)	0.31
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	1.49
ff V mean/V*	5.66
ff D_{84}	3.94
ff mean	4.80
ROUGH BED	

Hydraulic Ratios	
ER max d	4.49
r_c / TW	
TW / Lf_w	1.23
TW/max d	12.6
TW/mean d	15.6

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.803	27.49	NO	NO	NO	NO
V_* ($m\ s^{-1}$)	0.071	D_{50}	1.468	50.24	NO	NO	NO	NO
		D_{84}	2.076	71.06	NO	NO	NO	NO

Section Data

ER_e (m)	0.39	ER stations L / R	-2.00	20.00	TW ck
WS_e (m)	0.000	WS stations L / R	0.00	4.90	4.90
Lf_e (m)	-0.300	Lf stations L / R	0.50	4.50	
W_{fp} (m)	22.00	E_s sta. (Limerinos) L / R			
r_c (m)		E_s sta. (Strickler) L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.39	3.00	
E_g ($m\ m^{-1}$)	0.0085				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})		D_{30}	D_{50}	D_{84}
			T_*	0.9	0.3	0.1
B3	0.0022	0.0019	saltation	NO	NO	NO
C3	0.0008	0.0003	rolling	NO	NO	NO
C4	0.0084	0.0066	Ø	YES	YES	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	6.00	30.00	100.00	200.00	270.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)		29.10	97.00	194.00	261.90
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime

Strickler method		Limerinos method	
Q (cms)	1.704	Q (cms)	
V ($m\ s^{-1}$)	1.11	V ($m\ s^{-1}$)	
n	0.037	n	
Fr	0.63	*Fr*	
D_c rectangular (m)	0.23	D_c rectangular (m)	
D_c trapezoidal (m)	0.40	D_c trapezoidal (m)	
D_c triangular (m)	0.58	D_c triangular (m)	
D_c parabolic (m)	0.37	D_c parabolic (m)	
D_c mean (m)	0.40	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	141.97	Ω (watts m^{-1})	
ω_a (watts m^{-2})	27.57	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	5.63	ω_a/TW (watts m^{-1})	
*Re**	145.8	*Re**	
Re	290288	*Re*	
turbulence	HIGH	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} (kg m^{-2})	2.54		
τ_{calc} ($N\ m^{-2}$)	24.87		
τ D_{crit} (gr-co) (mm)	25.64		
D_{50} V_c (vcs +) ($m\ s^{-1}$)	1.55	2.00	
D_{84} V_c (vcs +) ($m\ s^{-1}$)	2.19	2.82	

Bank Data

	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

Substrate Type (%)

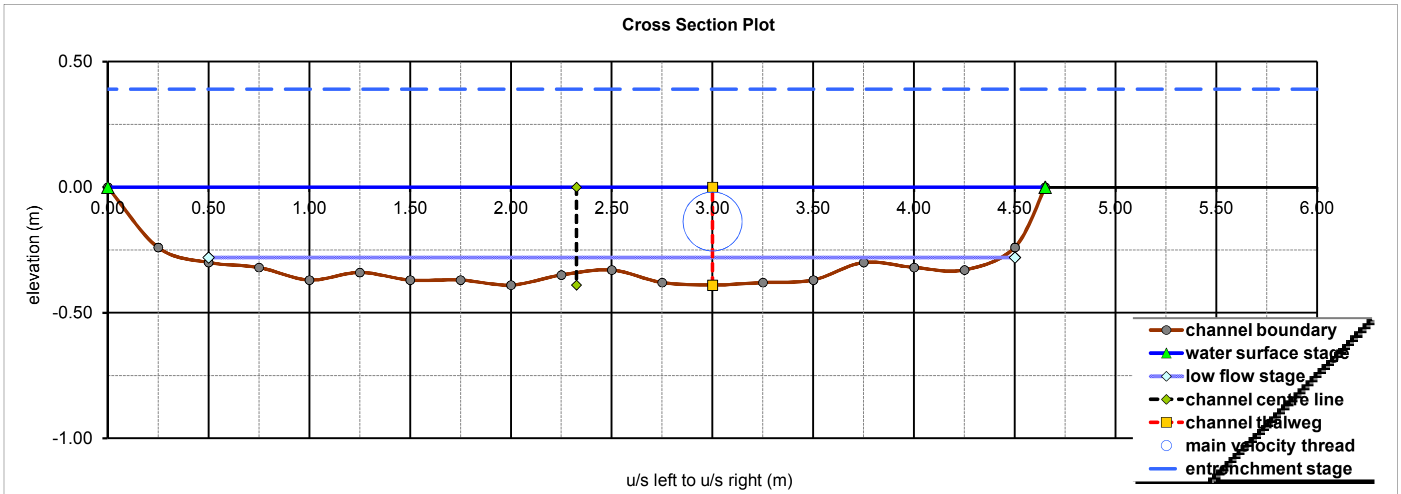
silt/clay	sand	gravel	cobble	boulder
0.0	13.6	25.0	59.1	2.3

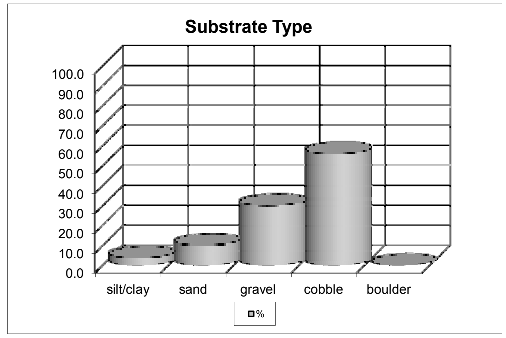
GEO-X v.5.1 Geomorphic Cross-section Analysis Model

AquaLogic

B. de Geus 05.11

Project: Erosion Threshold Analysis
Midtown Oakville
Lower Wedgewood Creek - Section 3 - existing bankfull flow





Morphology Type	
cascade	
step	
riffle	
run	●
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	1.51
R (m)	0.31
TW (m)	4.65
WP (m)	4.93
max d (m)	0.39
mean d (m)	0.32
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr *R*/D_{84}	2.04
ff V mean/V*	6.06
ff D_{84}	4.74
ff mean	5.40
ROUGH BED	

Hydraulic Ratios	
ER max d	4.73
r_c / TW	
TW / Lf_w	1.16
TW/max d	11.9
TW/mean d	14.3

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.655	22.15	NO	NO	NO	NO
V_* ($m\ s^{-1}$)	0.072	D_{50}	1.228	41.50	NO	NO	NO	NO
		D_{84}	1.798	60.76	NO	NO	NO	NO

Section Data

ER_e (m)	0.39	ER stations L / R	-2.00	20.00	TW ck
WS_e (m)	0.000	WS stations L / R	0.00	4.65	4.65
Lf_e (m)	-0.280	Lf stations L / R	0.50	4.50	
W_{fp} (m)	22.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.39	3.00	
E_g ($m\ m^{-1}$)	0.0085				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})	T_*	D_{30}	D_{50}	D_{84}
				1.3	0.4	0.2
B3	0.0022	0.0020	saltation	NO	NO	NO
C3	0.0008	0.0004	rolling	YES	NO	NO
C4	0.0084	0.0071	Ø	NO	YES	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	3.00	20.00	70.00	150.00	200.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)		19.40	67.90	145.50	194.00
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime Strickler method		Flow Regime Limerinos method	
Q (cms)	1.703	Q (cms)	
V ($m\ s^{-1}$)	1.13	V ($m\ s^{-1}$)	
n	0.037	n	
Fr	0.63	*Fr*	
D_c rectangular (m)	0.24	D_c rectangular (m)	
D_c trapezoidal (m)	0.40	D_c trapezoidal (m)	
D_c triangular (m)	0.58	D_c triangular (m)	
D_c parabolic (m)	0.37	D_c parabolic (m)	
D_c mean (m)	0.40	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	141.88	Ω (watts m^{-1})	
ω_a (watts m^{-2})	28.76	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	6.19	ω_a/TW (watts m^{-1})	
*Re**	102.1	*Re**	
Re	302893	*Re*	
turbulence	HIGH	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} (kg m^{-2})	2.60		
τ_{calc} (N m^{-2})	25.51		
τ D_{crit} (gr-co) (mm)	26.30		
D_{50} V_c (vcs +) ($m\ s^{-1}$)	1.30	1.64	
D_{84} V_c (vcs +) ($m\ s^{-1}$)	1.90	2.41	

Substrate Type (%)

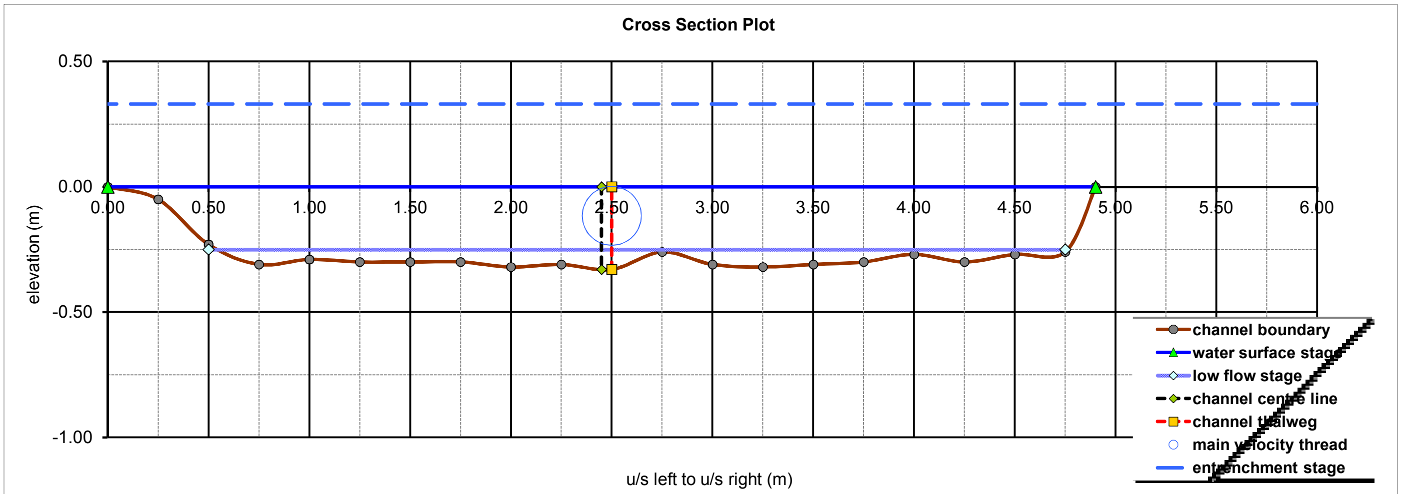
silt/clay	sand	gravel	cobble	boulder
4.0	10.0	30.0	56.0	0.0

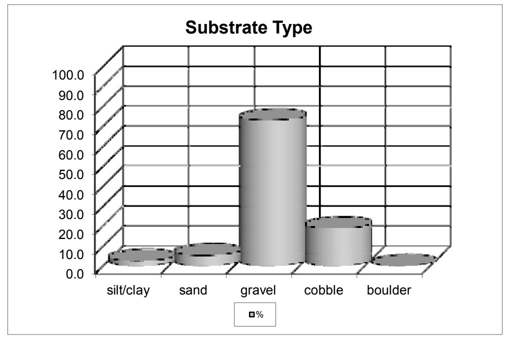
Bank Data	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

Project: Erosion Threshold Analysis
Midtown Oakville
Lower Wedgewood Creek - Section 4 - existing bankfull flow

AquaLogic
B. de Geus 05.11





Morphology Type		Hydraulic Geometry	
cascade		A (m²)	1.32
step		R (m)	0.26
riffle	●	TW (m)	4.90
run		WP (m)	5.15
glide		max d (m)	0.33
pool		mean d (m)	0.27
thalweg out of phase		$E_{s\ (Limerinos)}$ (m) [+]	
Hydraulic Roughness		$E_{s\ (Strickler)}$ (m) [+]	
rr R/D_{84}	3.67	**Hydraulic Ratios**	
ff V mean/V*	6.65	ER max d	2.45
ff D_{84}	6.17	r_c / TW	
ff mean	6.41	TW / Lf_w	1.15
ROUGH BED		TW/max d	14.8
		TW/mean d	18.2

Sediment Transport Mode

			w_s (m s^{-1})	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.604	17.37	NO	NO	NO	NO
V_* (m s^{-1})	0.085	D_{50}	0.733	21.08	NO	NO	NO	NO
		D_{84}	1.228	35.31	NO	NO	NO	NO

Section Data

ER_e (m)	0.33	ER stations L / R	-2.00	10.00	TW ck
WS_e (m)	0.000	WS stations L / R	0.00	4.90	4.90
Lf_e (m)	-0.250	Lf stations L / R	0.50	4.75	
W_{fp} (m)	12.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.33	2.50	
E_g (m m^{-1})	0.0140				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})	T_*	D_{30}	D_{50}	D_{84}
				2.1	1.5	0.5
B3	0.0022	0.0022	saltation	YES	NO	NO
C3	0.0008	0.0007	rolling	YES	YES	NO
C4	0.0084	0.0081	Ø	NO	NO	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	8.00	17.00	25.00	70.00	160.00
Stability Design Targets (mm)					
τ_{cr} (N m^{-2})		16.49	24.25	67.90	155.20
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime

Strickler method		Limerinos method	
Q (cms)	1.700	Q (cms)	
V (m s^{-1})	1.29	V (m s^{-1})	
n	0.037	n	
Fr	0.79	*Fr*	
D_c rectangular (m)	0.23	D_c rectangular (m)	
D_c trapezoidal (m)	0.40	D_c trapezoidal (m)	
D_c triangular (m)	0.58	D_c triangular (m)	
D_c parabolic (m)	0.39	D_c parabolic (m)	
D_c mean (m)	0.40	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	233.24	Ω (watts m^{-1})	
ω_a (watts m^{-2})	45.30	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	9.24	ω_a/TW (watts m^{-1})	
*Re**	37.4	*Re**	
Re	289606	*Re*	
turbulence	HIGH	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	V_c / V_b Limerinos
τ_{calc} (kg m^{-2})	3.59		
τ_{calc} (N m^{-2})	35.22		
τ D_{crit} (gr-co) (mm)	36.31		
D_{50} V_c (vcs +) (m s^{-1})	0.78	0.86	
D_{84} V_c (vcs +) (m s^{-1})	1.30	1.44	

Substrate Type (%)

silt/clay	sand	gravel	cobble	boulder
2.7	5.4	73.0	18.9	0.0

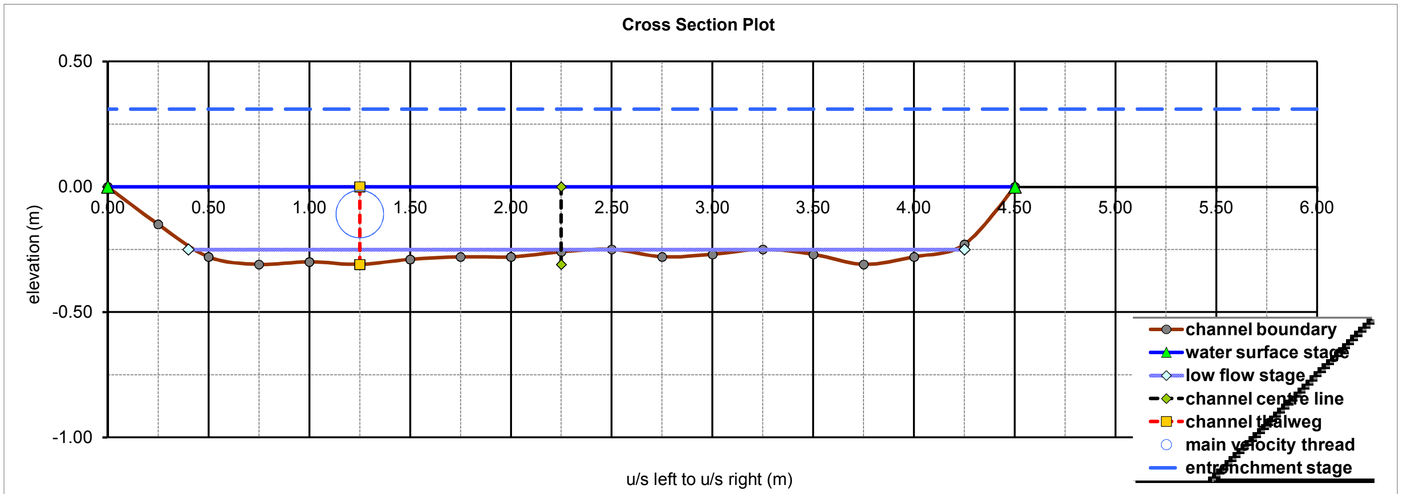
Bank Data

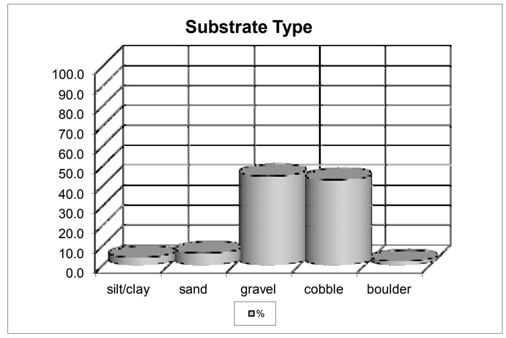
	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

Project: **Erosion Threshold Analysis**
Midtown Oakville
Lower Wedgewood Creek - Section 5 - existing bankfull flow

B. de Geus 05.11





Morphology Type	
cascade	
step	
riffle	●
run	
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	1.15
R (m)	0.25
TW (m)	4.50
WP (m)	4.68
max d (m)	0.31
mean d (m)	0.26
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	2.05
ff V mean/V*	5.66
ff D_{84}	4.70
ff mean	5.18
ROUGH BED	

Hydraulic Ratios	
ER max d	2.67
r_c / TW	
TW / Lf_w	1.17
TW/max d	14.5
TW/mean d	17.6

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.655	15.03	NO	NO	NO	NO
V_* ($m\ s^{-1}$)	0.106	D_{50}	1.089	24.96	NO	NO	NO	NO
		D_{84}	1.608	36.88	NO	NO	NO	NO

Section Data

ER_e (m)	0.31	ER stations L / R	-2.00	10.00	TW ck
WS_e (m)	0.000	WS stations L / R	0.00	4.50	4.50
Lf_e (m)	-0.250	Lf stations L / R	0.40	4.25	
W_{fp} (m)	12.00	E_s sta. (Limerinos) L / R			
r_c (m)		E_s sta. (Strickler) L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.31	1.25	
E_g ($m\ m^{-1}$)	0.0230				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} ($kg\ sec^{-1}$)	Limerinos Q Q_{sb} ($kg\ sec^{-1}$)	T_*	D_{30}	D_{50}	D_{84}
				2.9	1.0	0.5
B3	0.0022	0.0021	saltation	YES	NO	NO
C3	0.0008	0.0005	rolling	YES	YES	NO
C4	0.0084	0.0075	Ø	NO	NO	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	4.00	20.00	55.00	120.00	200.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)		19.40	53.35	116.40	194.00
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Erosion Thresholds

τ_{calc} ($kg\ m^{-2}$)	5.65		
τ_{calc} ($N\ m^{-2}$)	55.38	V_c / V_b	
$\tau\ D_{crit}$ (gr-co) (mm)	57.09	Strickler	Limerinos
$D_{50}\ V_c$ (vcs +) ($m\ s^{-1}$)	1.15	1.11	
$D_{84}\ V_c$ (vcs +) ($m\ s^{-1}$)	1.70	1.64	

Substrate Type (%)

silt/clay	sand	gravel	cobble	boulder
4.1	6.1	44.9	42.9	2.0

Bank Data	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

Flow Regime Strickler method		Flow Regime Limerinos method	
Q (cms)	1.702	Q (cms)	
V ($m\ s^{-1}$)	1.48	V ($m\ s^{-1}$)	
n	0.040	n	
Fr	0.94	*Fr*	
D_c rectangular (m)	0.25	D_c rectangular (m)	
D_c trapezoidal (m)	0.41	D_c trapezoidal (m)	
D_c triangular (m)	0.58	D_c triangular (m)	
D_c parabolic (m)	0.39	D_c parabolic (m)	
D_c mean (m)	0.41	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω ($watts\ m^{-1}$)	383.72	Ω ($watts\ m^{-1}$)	
ω_a ($watts\ m^{-2}$)	81.98	ω_a ($watts\ m^{-2}$)	
ω_a/TW ($watts\ m^{-1}$)	18.22	ω_a/TW ($watts\ m^{-1}$)	
*Re**	89.1	*Re**	
Re	319036	*Re*	
turbulence	HIGH	turbulence	

Lower Morrison Creek
Upstream Reach

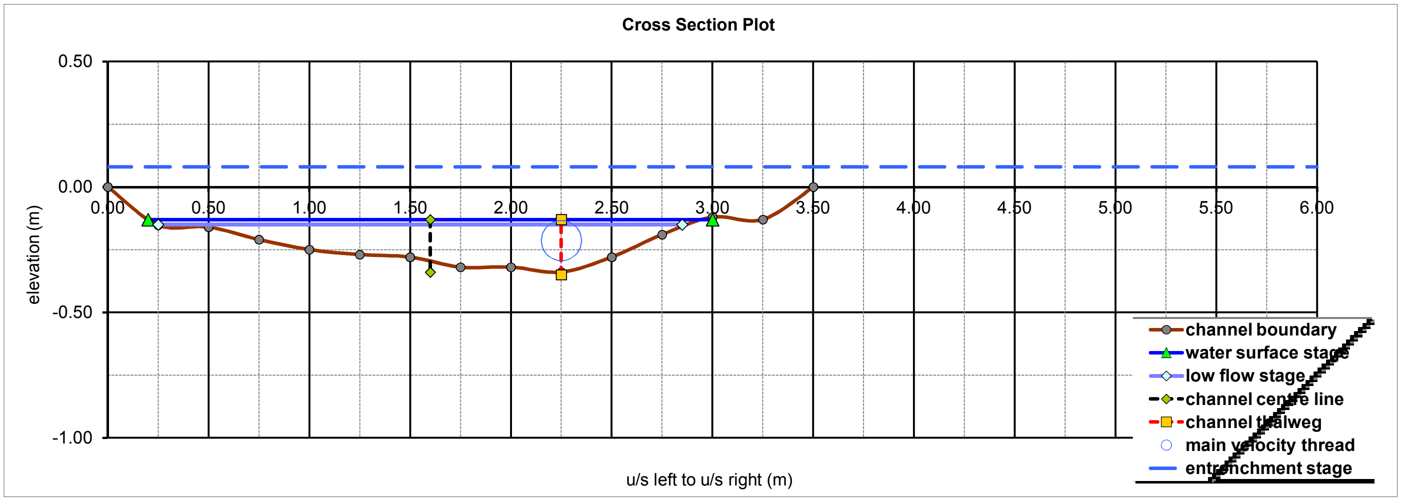
Stability Conditions

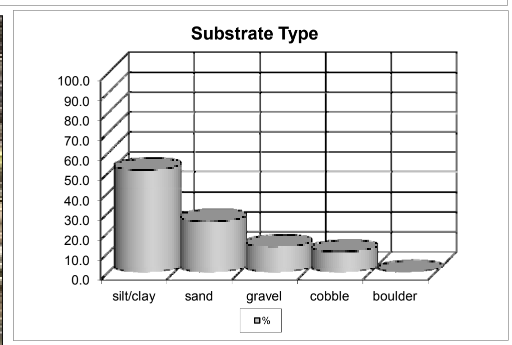
AquaLogic

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

Project: Erosion Threshold Analysis
Midtown Oakville
Lower Morrison Creek - upstream Section 1 - stability test

B. de Geus 05.11





Morphology Type	
cascade	
step	
riffle	
run	
glide	
pool	●
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	0.33
R (m)	0.12
TW (m)	2.75
WP (m)	2.80
max d (m)	0.21
mean d (m)	0.12
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	4.74
ff V mean/V*	6.66
ff D_{84}	6.73
ff mean	6.69
ROUGH BED	

Hydraulic Ratios	
ER max d	5.45
r_c / TW	
TW / Lf_w	1.06
TW/max d	13.1
TW/mean d	22.8

Sediment Transport Mode

			w_s (m s^{-1})	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.001	0.06	YES	YES	YES	YES
V_* (m s^{-1})	0.058	D_{50}	0.003	0.13	YES	YES	YES	YES
		D_{84}	0.733	31.02	NO	NO	NO	NO

Section Data

ER_e (m)	0.08	ER stations L / R	-5.00	10.00	TW ck
WS_e (m)	-0.130	WS stations L / R	0.20	3.00	2.80
Lf_e (m)	-0.150	Lf stations L / R	0.25	2.85	
W_{fp} (m)	15.00	E_s sta. (Limerinos) L / R			
r_c (m)		E_s sta. (Strickler) L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.35	2.25	
E_g (m m^{-1})	0.0140				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})	T_*	D_{30}	D_{50}	D_{84}
				419.2	279.5	0.7
B3	0.0013	0.0013	saltation	YES	YES	NO
C3	0.0000	0.0000	rolling	YES	YES	NO
C4	0.0035	0.0037	Ø	NO	NO	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.02	0.04	0.06	25.00	160.00
Stability Design Targets (mm)					
τ_{cr} (N m^{-2})				24.25	155.20
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime Strickler method		Flow Regime Limerinos method	
Q (cms)	0.269	Q (cms)	
V (m s^{-1})	0.81	V (m s^{-1})	
n	0.035	n	
Fr	0.74	*Fr*	
D_c rectangular (m)	0.10	D_c rectangular (m)	
D_c trapezoidal (m)	0.19	D_c trapezoidal (m)	
D_c triangular (m)	0.28	D_c triangular (m)	
D_c parabolic (m)	0.19	D_c parabolic (m)	
D_c mean (m)	0.19	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	36.91	Ω (watts m^{-1})	
ω_a (watts m^{-2})	13.18	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	4.79	ω_a/TW (watts m^{-1})	
*Re**	0.1	*Re**	
Re	84250	*Re*	
turbulence	LOW	turbulence	

Erosion Thresholds

		Strickler V_c / V_b	Limerinos V_c / V_b
τ_{calc} (kg m^{-2})	1.66		
τ_{calc} (N m^{-2})	16.27		
τ D_{crit} (gr-co) (mm)	16.77		
D_{50} V_c (vcs +) (m s^{-1})	0.04	0.07	
D_{84} V_c (vcs +) (m s^{-1})	0.78	1.37	

Substrate Type (%)

silt/clay	sand	gravel	cobble	boulder
51.3	25.6	12.8	10.3	0.0

Bank Data	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

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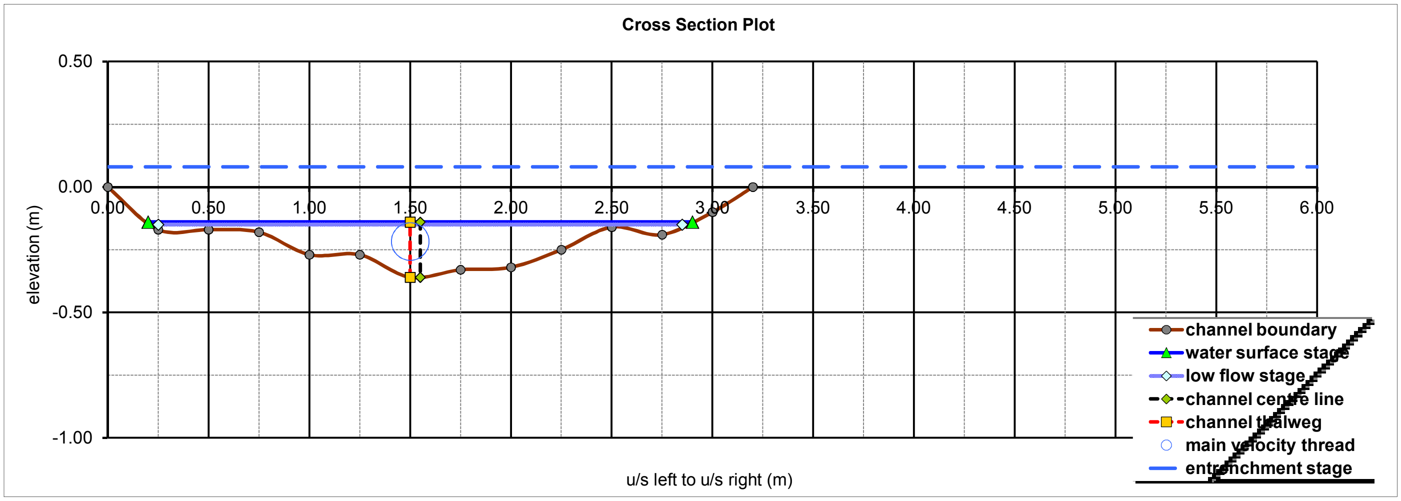
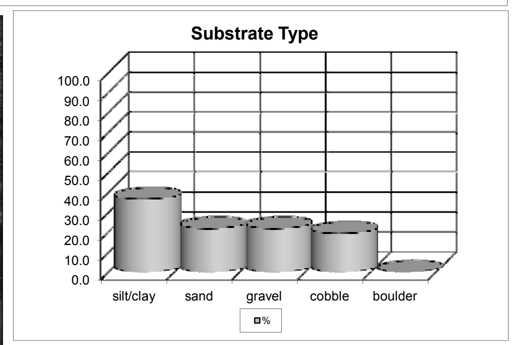
Project: **Erosion Threshold Analysis**
Midtown Oakville
Lower Morrison Creek - upstream Section 2 - stability test





Morphology Type	
cascade	
step	
riffle	
run	●
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	0.28
R (m)	0.10
TW (m)	2.68
WP (m)	2.76
max d (m)	0.22
mean d (m)	0.10
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	1.18
ff V mean/V*	4.91
ff D_{84}	3.31
ff mean	4.11
ROUGH BED	

Hydraulic Ratios	
ER max d	5.59
r_c / TW	
TW / Lf_w	1.03
TW/max d	12.2
TW/mean d	26.0

Sediment Transport Mode

			w_s (m s^{-1})	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.003	0.12	YES	YES	YES	YES
V_* (m s^{-1})	0.058	D_{50}	0.071	2.97	NO	NO	NO	YES
		D_{84}	1.353	56.54	NO	NO	NO	NO

Section Data

ER_e (m)	0.08	ER stations L / R	-5.00	10.00	TW ck
WS_e (m)	-0.140	WS stations L / R	0.20	2.90	2.70
Lf_e (m)	-0.150	Lf stations L / R	0.25	2.85	
W_{fp} (m)	15.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.36	1.50	
E_g (m m^{-1})	0.0170				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})		D_{30}	D_{50}	D_{84}
			T_*	286.7	34.4	0.2
B3	0.0012	0.0010	saltation	YES	YES	NO
C3	0.0000	0.0000	rolling	YES	YES	NO
C4	0.0032	0.0025	Ø	NO	NO	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.03	0.06	0.50	85.00	190.00
Stability Design Targets (mm)					
τ_{cr} (N m^{-2})				82.45	184.30
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime

Strickler method		Limerinos method	
Q (cms)	0.221	Q (cms)	
V (m s^{-1})	0.80	V (m s^{-1})	
n	0.035	n	
Fr	0.79	*Fr*	
D_c rectangular (m)	0.09	D_c rectangular (m)	
D_c trapezoidal (m)	0.17	D_c trapezoidal (m)	
D_c triangular (m)	0.26	D_c triangular (m)	
D_c parabolic (m)	0.18	D_c parabolic (m)	
D_c mean (m)	0.17	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	36.75	Ω (watts m^{-1})	
ω_a (watts m^{-2})	13.31	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	4.96	ω_a/TW (watts m^{-1})	
*Re**	0.8	*Re**	
Re	70060	*Re*	
turbulence	LOW	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} (kg m^{-2})	1.70		
τ_{calc} (N m^{-2})	16.69		
τ D_{crit} (gr-co) (mm)	17.20		
D_{50} V_c (vcs +) (m s^{-1})	0.11	0.20	
D_{84} V_c (vcs +) (m s^{-1})	1.43	2.56	

Bank Data

	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

Substrate Type (%)

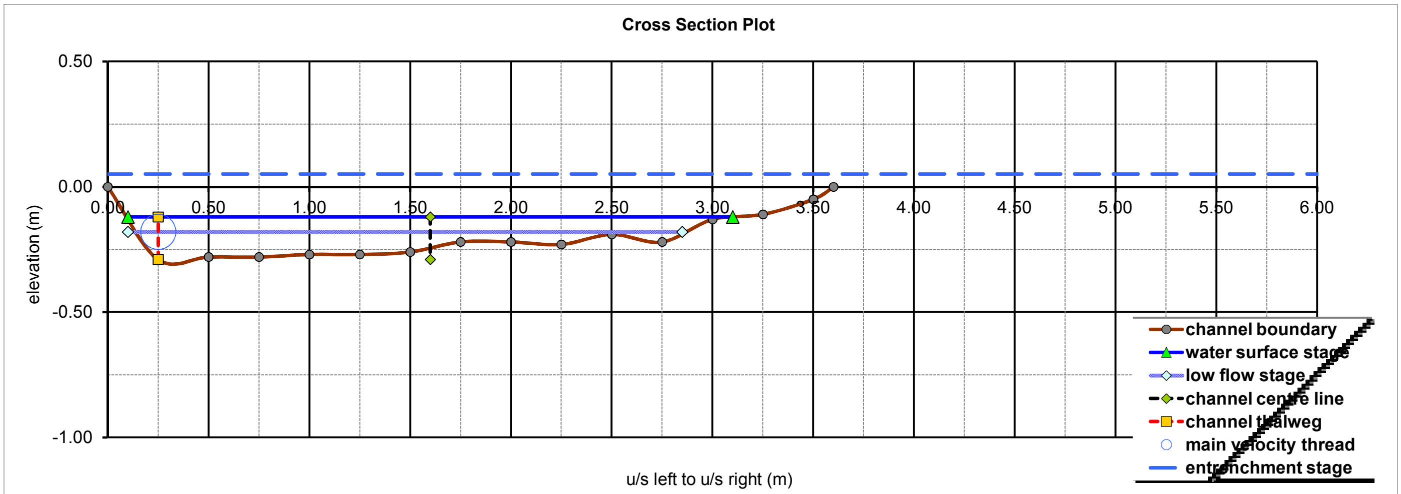
silt/clay	sand	gravel	cobble	boulder
36.6	22.0	22.0	19.5	0.0

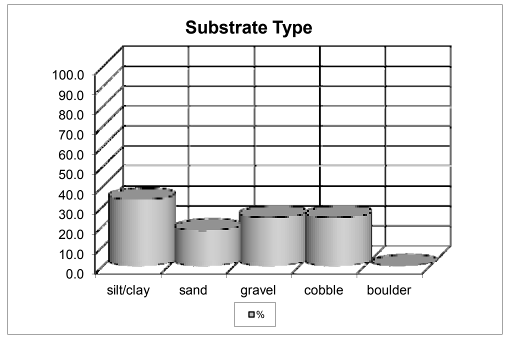
GEO-X v.5.1 Geomorphic Cross-section Analysis Model

AquaLogic

B. de Geus 05.11

Project: Erosion Threshold Analysis
Midtown Oakville
Lower Morrison Creek - upstream Section 3 - stability test





Morphology Type	
cascade	
step	
riffle	
run	●
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	0.35
R (m)	0.11
TW (m)	3.02
WP (m)	3.12
max d (m)	0.17
mean d (m)	0.11
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	0.88
ff V mean/V*	4.63
ff D_{84}	2.61
ff mean	3.62
ROUGH BED	

Hydraulic Ratios	
ER max d	4.96
r_c / TW	
TW / Lf_w	1.10
TW/max d	17.8
TW/mean d	26.4

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.003	0.13	YES	YES	YES	YES
V_* ($m\ s^{-1}$)	0.058	D_{50}	0.126	5.34	NO	NO	NO	YES
		D_{84}	1.641	69.47	NO	NO	NO	NO

Section Data

ER_e (m)	0.05	ER stations L / R	-5.00	10.00	TW ck
WS_e (m)	-0.120	WS stations L / R	0.10	3.10	3.00
Lf_e (m)	-0.180	Lf stations L / R	0.10	2.85	
W_{fp} (m)	15.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.29	0.25	
E_g ($m\ m^{-1}$)	0.0150				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})	T_*	D_{30}	D_{50}	D_{84}
				279.4	16.8	0.1
B3	0.0013	0.0011	saltation	YES	YES	NO
C3	0.0000	0.0000	rolling	YES	YES	NO
C4	0.0035	0.0025	Ø	NO	NO	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.03	0.06	1.00	125.00	170.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)				121.25	164.90
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} (kg m^{-2})	1.66		
τ_{calc} ($N\ m^{-2}$)	16.26		
$\tau\ D_{crit}$ (gr-co) (mm)	16.76		
$D_{50}\ V_c$ (vcs +) ($m\ s^{-1}$)	0.16	0.28	
$D_{84}\ V_c$ (vcs +) ($m\ s^{-1}$)	1.73	3.09	

Substrate Type (%)

silt/clay	sand	gravel	cobble	boulder
33.3	17.8	24.4	24.4	0.0

Bank Data

	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

Flow Regime

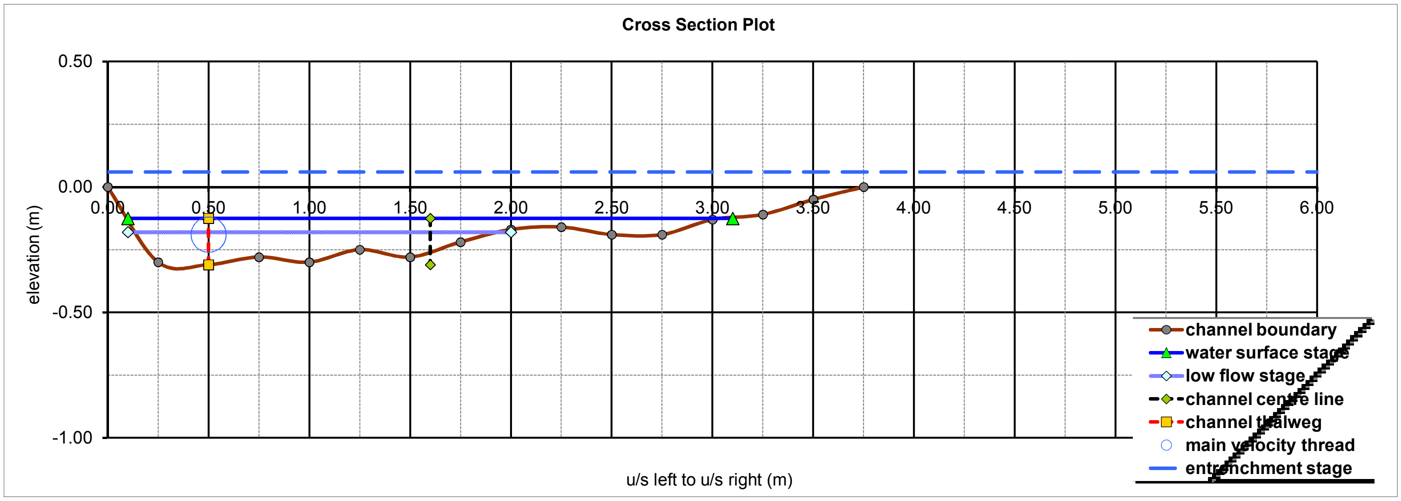
Strickler method		Limerinos method	
Q (cms)	0.277	Q (cms)	
V ($m\ s^{-1}$)	0.80	V ($m\ s^{-1}$)	
n	0.035	n	
Fr	0.76	*Fr*	
D_c rectangular (m)	0.10	D_c rectangular (m)	
D_c trapezoidal (m)	0.19	D_c trapezoidal (m)	
D_c triangular (m)	0.28	D_c triangular (m)	
D_c parabolic (m)	0.19	D_c parabolic (m)	
D_c mean (m)	0.19	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	40.66	Ω (watts m^{-1})	
ω_a (watts m^{-2})	13.01	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	4.31	ω_a/TW (watts m^{-1})	
*Re**	1.6	*Re**	
Re	77655	*Re*	
turbulence	LOW	turbulence	

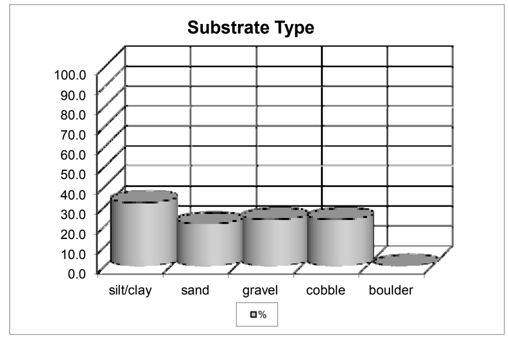
GEO-X v.5.1 Geomorphic Cross-section Analysis Model

AquaLogic

B. de Geus 05.11

Project: **Erosion Threshold Analysis**
Midtown Oakville
Lower Morrison Creek - upstream Section 4 - stability test





Morphology Type	
cascade	
step	
riffle	
run	●
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	0.31
R (m)	0.10
TW (m)	2.96
WP (m)	3.07
max d (m)	0.19
mean d (m)	0.10
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	1.06
ff V mean/V*	4.80
ff D_{84}	3.08
ff mean	3.94
ROUGH BED	

Hydraulic Ratios	
ER max d	5.07
r_c / TW	
TW / Lf_w	1.56
TW/max d	16.0
TW/mean d	28.2

Sediment Transport Mode

			w_s (m s^{-1})	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.003	0.12	YES	YES	YES	YES
V_* (m s^{-1})	0.059	D_{50}	0.196	8.16	NO	NO	NO	NO
		D_{84}	1.431	59.50	NO	NO	NO	NO

Section Data

ER_e (m)	0.06	ER stations L / R	-5.00	10.00	TW ck
WS_e (m)	-0.125	WS stations L / R	0.10	3.10	3.00
Lf_e (m)	-0.180	Lf stations L / R	0.10	2.00	
W_{fp} (m)	15.00	E_s sta. (Limerinos) L / R			
r_c (m)		E_s sta. (Strickler) L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.31	0.50	
E_g (m m^{-1})	0.0170				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})			D_{30}	D_{50}	D_{84}
				T_*	289.3	8.7	0.2
B3	0.0013	0.0011	saltation		YES	YES	NO
C3	0.0000	0.0000	rolling		YES	YES	NO
C4	0.0034	0.0025		Ø	NO	NO	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.03	0.06	2.00	95.00	160.00
Stability Design Targets (mm)					
τ_{cr} (N m^{-2})				92.15	155.20
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime Strickler method		Flow Regime Limerinos method	
Q (cms)	0.249	Q (cms)	
V (m s^{-1})	0.80	V (m s^{-1})	
n	0.035	n	
Fr	0.79	*Fr*	
D_c rectangular (m)	0.09	D_c rectangular (m)	
D_c trapezoidal (m)	0.18	D_c trapezoidal (m)	
D_c triangular (m)	0.27	D_c triangular (m)	
D_c parabolic (m)	0.19	D_c parabolic (m)	
D_c mean (m)	0.18	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	41.48	Ω (watts m^{-1})	
ω_a (watts m^{-2})	13.51	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	4.57	ω_a/TW (watts m^{-1})	
*Re**	3.3	*Re**	
Re	71121	*Re*	
turbulence	LOW	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} (kg m^{-2})	1.72		
τ_{calc} (N m^{-2})	16.84		
τ D_{crit} (gr-co) (mm)	17.36		
D_{50} V_c (vcs +) (m s^{-1})	0.22	0.39	
D_{84} V_c (vcs +) (m s^{-1})	1.51	2.69	

Substrate Type (%)

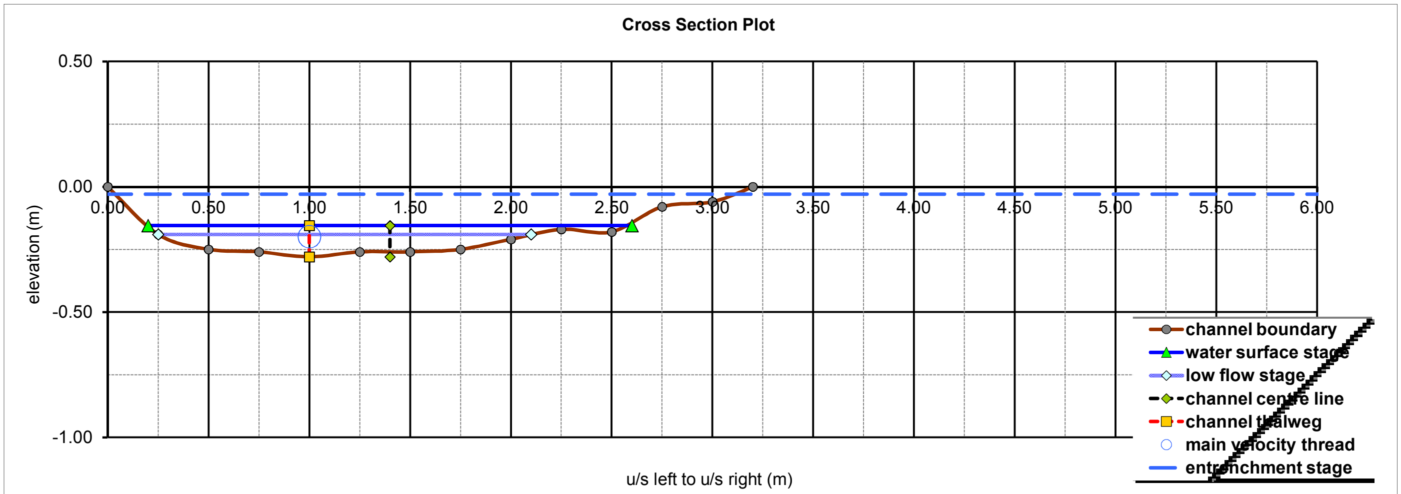
silt/clay	sand	gravel	cobble	boulder
31.9	21.3	23.4	23.4	0.0

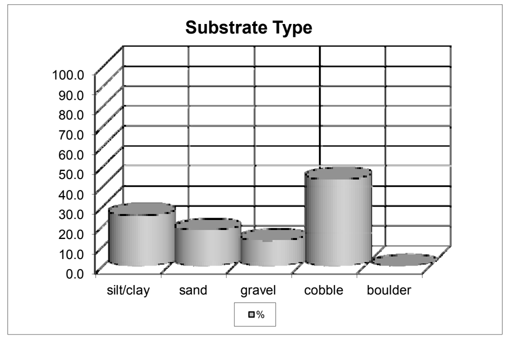
Bank Data u/s L	u/s R
H_b (m)	
Bf_d (m)	
RDp (m)	
H_b/Bf_d	
RDp/H_b	
RDn (%)	
BA (°)	
BFP (%)	

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

Project: **Erosion Threshold Analysis**
Midtown Oakville
Lower Morrison Creek - upstream Section 5 - stability test

B. de Geus 05.11





Morphology Type		Hydraulic Geometry	
cascade		A (m^2)	0.18
step		R (m)	0.08
riffle	●	TW (m)	2.36
run		WP (m)	2.39
glide		max d (m)	0.13
pool		mean d (m)	0.08
thalweg out of phase	●	$E_{s\ (Limerinos)}$ (m) [+]	
		$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness		Hydraulic Ratios	
rr R/D_{84}	0.62	ER max d	6.36
ff V mean/V*	3.98	r_c / TW	
ff D_{84}	1.66	TW / Lf_w	1.27
ff mean	2.82	TW/max d	18.9
ROUGH BED		TW/mean d	30.2

Sediment Transport Mode

			w_s (m s^{-1})	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.032	1.25	NO	NO	YES	YES
V_* (m s^{-1})	0.062	D_{50}	0.803	31.57	NO	NO	NO	NO
		D_{84}	1.641	64.49	NO	NO	NO	NO

Section Data

					TW ck
ER_e (m)	-0.03	ER stations L / R	-5.00	10.00	
WS_e (m)	-0.155	WS stations L / R	0.20	2.60	2.40
Lf_e (m)	-0.190	Lf stations L / R	0.25	2.10	
W_{fp} (m)	15.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.28	1.00	
E_g (m m^{-1})	0.0250				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})	T_*	D_{30}	D_{50}	D_{84}
				77.8	0.6	0.2
B3	0.0011	0.0008	saltation	YES	NO	NO
C3	0.0000	0.0000	rolling	YES	NO	NO
C4	0.0026	0.0016	Ø	NO	YES	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	0.05	0.25	30.00	125.00	190.00
Stability Design Targets (mm)					
τ_{cr} (N m^{-2})			29.10	121.25	184.30
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime

Strickler method		Limerinos method	
Q (cms)	0.149	Q (cms)	
V (m s^{-1})	0.81	V (m s^{-1})	
n	0.035	n	
Fr	0.93	*Fr*	
D_c rectangular (m)	0.08	D_c rectangular (m)	
D_c trapezoidal (m)	0.15	D_c trapezoidal (m)	
D_c triangular (m)	0.22	D_c triangular (m)	
D_c parabolic (m)	0.16	D_c parabolic (m)	
D_c mean (m)	0.15	D_c mean (m)	
flow type	SUPERCRITICAL	flow type	
Ω (watts m^{-1})	36.56	Ω (watts m^{-1})	
ω_a (watts m^{-2})	15.29	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	6.48	ω_a/TW (watts m^{-1})	
*Re**	51.1	*Re**	
Re	54754	*Re*	
turbulence	HIGH	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} (kg m^{-2})	1.92		
τ_{calc} (N m^{-2})	18.86		
τ D_{crit} (gr-co) (mm)	19.45		
D_{50} V_c (vcs +) (m s^{-1})	0.85	1.50	
D_{84} V_c (vcs +) (m s^{-1})	1.73	3.05	

Bank Data

	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

Substrate Type (%)

silt/clay	sand	gravel	cobble	boulder
25.6	17.9	12.8	43.6	0.0

Lower Wedgewood Creek

Stability Conditions

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

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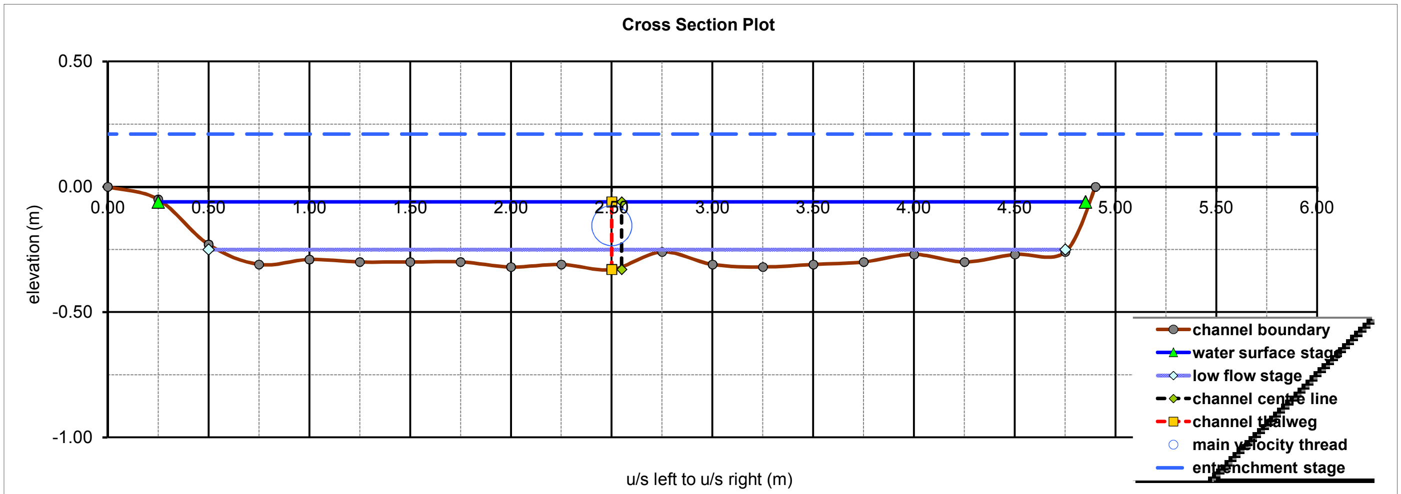
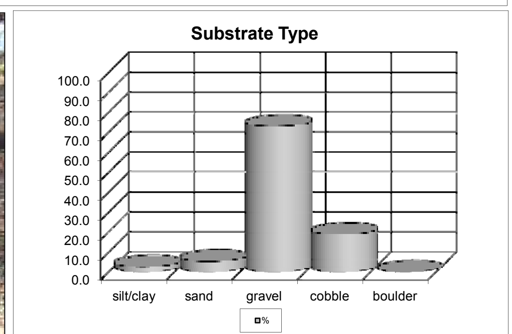
Project: Erosion Threshold Analysis
Midtown Oakville
Lower Wedgewood Creek - Section 4 - stability test





Morphology Type	
cascade	
step	
riffle	●
run	
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	1.04
R (m)	0.22
TW (m)	4.60
WP (m)	4.81
max d (m)	0.27
mean d (m)	0.23
$E_{s\,(Limerinos)}$ (m) [+]	
$E_{s\,(Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	3.08
ff V mean/V*	6.33
ff D_{84}	5.73
ff mean	6.03
ROUGH BED	

Hydraulic Ratios	
ER max d	2.61
r_c / TW	
TW / Lf_w	1.08
TW/max d	17.0
TW/mean d	20.4

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.604	18.94	NO	NO	NO	NO
V_* ($m\ s^{-1}$)	0.078	D_{50}	0.733	22.99	NO	NO	NO	NO
		D_{84}	1.228	38.51	NO	NO	NO	NO

Section Data

ER_e (m)	0.21	ER stations L / R	-2.00	10.00	TW ck
WS_e (m)	-0.060	WS stations L / R	0.25	4.85	4.60
Lf_e (m)	-0.250	Lf stations L / R	0.50	4.75	
W_{fp} (m)	12.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.33	2.50	
E_g ($m\ m^{-1}$)	0.0140				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} ($kg\ sec^{-1}$)	Limerinos Q Q_{sb} ($kg\ sec^{-1}$)	T_*	D_{30}	D_{50}	D_{84}
				1.8	1.2	0.4
B3	0.0020	0.0019	saltation	NO	NO	NO
C3	0.0004	0.0003	rolling	YES	YES	NO
C4	0.0071	0.0067	Ø	NO	NO	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	8.00	17.00	25.00	70.00	160.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)		16.49	24.25	67.90	155.20
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime

Strickler method		Limerinos method	
Q (cms)	1.188	Q (cms)	
V ($m\ s^{-1}$)	1.14	V ($m\ s^{-1}$)	
n	0.037	n	
Fr	0.77	*Fr*	
D_c rectangular (m)	0.19	D_c rectangular (m)	
D_c trapezoidal (m)	0.34	D_c trapezoidal (m)	
D_c triangular (m)	0.50	D_c triangular (m)	
D_c parabolic (m)	0.34	D_c parabolic (m)	
D_c mean (m)	0.34	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	163.03	Ω (watts m^{-1})	
ω_a (watts m^{-2})	33.91	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	7.37	ω_a/TW (watts m^{-1})	
*Re**	38.4	*Re**	
Re	216794	*Re*	
turbulence	HIGH	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} ($kg\ m^{-2}$)	3.02		
τ_{calc} ($N\ m^{-2}$)	29.62		
τ D_{crit} (gr-co) (mm)	30.53		
D_{50} V_c (vcs +) ($m\ s^{-1}$)	0.78	0.97	
D_{84} V_c (vcs +) ($m\ s^{-1}$)	1.30	1.62	

Substrate Type (%)

silt/clay	sand	gravel	cobble	boulder
2.7	5.4	73.0	18.9	0.0

Bank Data	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

GEO-X v.5.1 Geomorphic Cross-section Analysis Model

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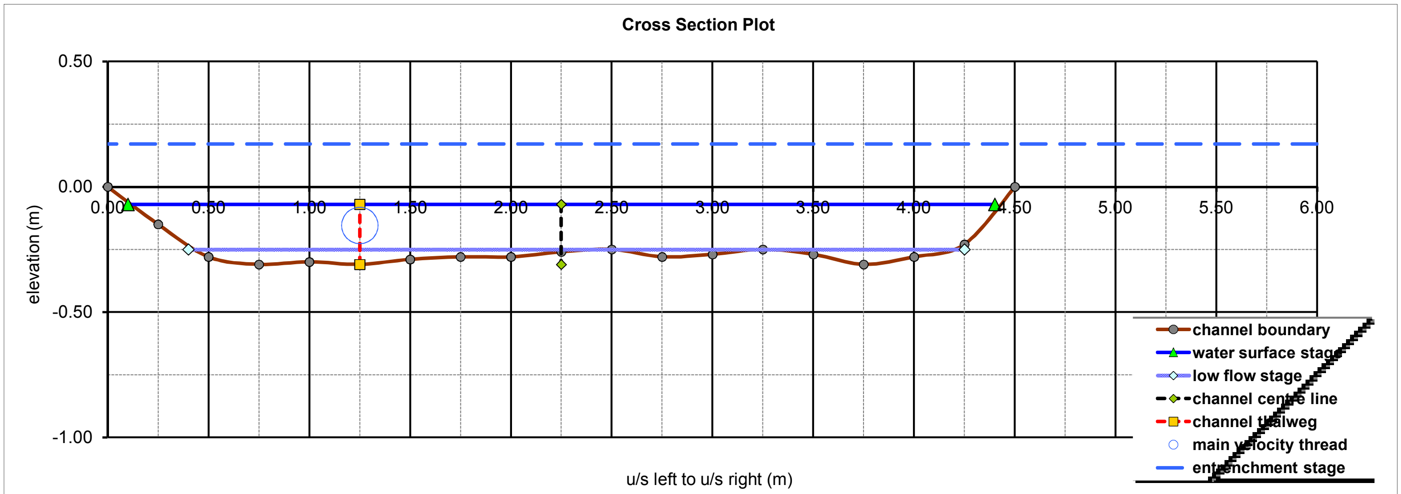
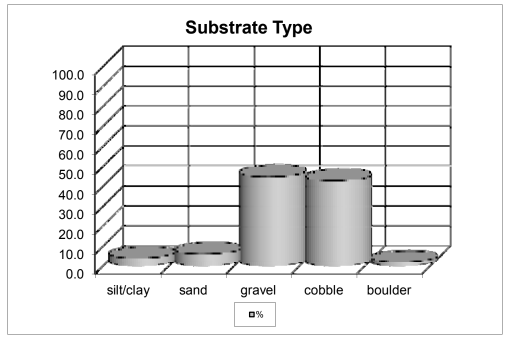
Project: Erosion Threshold Analysis
Midtown Oakville
Lower Wedgewood Creek - Section 5 - stability test





Morphology Type	
cascade	
step	
riffle	●
run	
glide	
pool	
thalweg out of phase	

Hydraulic Geometry	
A (m^2)	0.84
R (m)	0.19
TW (m)	4.31
WP (m)	4.44
max d (m)	0.24
mean d (m)	0.20
$E_{s\ (Limerinos)}$ (m) [+]	
$E_{s\ (Strickler)}$ (m) [+]	

Hydraulic Roughness	
rr R/D_{84}	1.58
ff V mean/V*	5.20
ff D_{84}	4.04
ff mean	4.62
ROUGH BED	

Hydraulic Ratios	
ER max d	2.79
r_c / TW	
TW / Lf_w	1.12
TW/max d	17.9
TW/mean d	22.0

Sediment Transport Mode

			w_s ($m\ s^{-1}$)	P	wash load	high sus. load	low sus. load	bedload
k	0.41	D_{30}	0.655	17.11	NO	NO	NO	NO
V_* ($m\ s^{-1}$)	0.093	D_{50}	1.089	28.42	NO	NO	NO	NO
		D_{84}	1.608	41.99	NO	NO	NO	NO

Section Data

ER_e (m)	0.17	ER stations L / R	-2.00	10.00	TW ck
WS_e (m)	-0.070	WS stations L / R	0.10	4.40	4.30
Lf_e (m)	-0.250	Lf stations L / R	0.40	4.25	
W_{fp} (m)	12.00	E_s sta. $_{(Limerinos)}$ L / R			
r_c (m)		E_s sta. $_{(Strickler)}$ L / R			
z		T_e (m) $T_{o/s}$ (m)	-0.31	1.25	
E_g ($m\ m^{-1}$)	0.0230				

Bedload Transport Data

Rosgen type	Strickler Q Q_{sb} (kg sec^{-1})	Limerinos Q Q_{sb} (kg sec^{-1})		T_*	D_{30}	D_{50}	D_{84}
					2.2	0.8	0.4
B3	0.0019	0.0018	saltation		YES	NO	NO
C3	0.0003	0.0002	rolling		YES	NO	NO
C4	0.0066	0.0057		Ø	NO	YES	YES

Substrate Gradation

	D_{15}	D_{30}	D_{50}	D_{84}	D_{100}
Existing Conditions (mm)	4.00	20.00	55.00	120.00	200.00
Stability Design Targets (mm)					
τ_{cr} ($N\ m^{-2}$)		19.40	53.35	116.40	194.00
high turbulence - angular (mm)					
high turbulence - rounded (mm)					
low turbulence - angular (mm)					
low turbulence - rounded (mm)					

Flow Regime

Strickler method		Limerinos method	
Q (cms)	1.047	Q (cms)	
V ($m\ s^{-1}$)	1.24	V ($m\ s^{-1}$)	
n	0.040	n	
Fr	0.90	*Fr*	
D_c rectangular (m)	0.18	D_c rectangular (m)	
D_c trapezoidal (m)	0.33	D_c trapezoidal (m)	
D_c triangular (m)	0.48	D_c triangular (m)	
D_c parabolic (m)	0.33	D_c parabolic (m)	
D_c mean (m)	0.33	D_c mean (m)	
flow type	SUBCRITICAL	flow type	
Ω (watts m^{-1})	236.04	Ω (watts m^{-1})	
ω_a (watts m^{-2})	53.15	ω_a (watts m^{-2})	
ω_a/TW (watts m^{-1})	12.34	ω_a/TW (watts m^{-1})	
*Re**	92.7	*Re**	
Re	206829	*Re*	
turbulence	HIGH	turbulence	

Erosion Thresholds

		V_c / V_b Strickler	Limerinos
τ_{calc} ($kg\ m^{-2}$)	4.36		
τ_{calc} ($N\ m^{-2}$)	42.72		
$\tau\ D_{crit}$ (gr-co) (mm)	44.04		
$D_{50}\ V_c$ (vcs +) ($m\ s^{-1}$)	1.15	1.32	1.95
$D_{84}\ V_c$ (vcs +) ($m\ s^{-1}$)	1.70	1.95	

Bank Data

	u/s L	u/s R
H_b (m)		
Bf_d (m)		
RDp (m)		
H_b/Bf_d		
RDp/H_b		
RDn (%)		
BA (°)		
BFP (%)		

Substrate Type (%)

silt/clay	sand	gravel	cobble	boulder
4.1	6.1	44.9	42.9	2.0

Erosion Threshold Summary Models

GEO - ESUM v.1.3 Erosion Threshold Summary Model

Project: Erosion Threshold Analysis
Midtown Oakville
Lower Morrison Creek- upstream reach

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Existing

	Q $m^3 s^{-1}$	V $m s^{-1}$	veg control	D_{50} particle	D_{84}-D_{100} particle	τ_{calc} $N m^{-2}$	veg control	D_{50} particle*	D_{84}-D_{100} particle*	Ω watts m^{-1}	Ω threshold
Xsec. 1	0.894	1.18	Y	N	N	29	Y	N	Y	123	Y
Xsec. 2	0.891	1.29	N	N	Y	34	Y	N	Y	149	Y
Xsec. 3	0.891	1.19	Y	N	Y	29	Y	N	Y	131	Y
Xsec. 4	0.890	1.21	N	N	Y	31	Y	N	Y	148	Y
Xsec. 5	0.890	1.46	N	N	Y	45	N	N	Y	218	Y

Dynamic Stability

Xsec. 1	0.289	0.81	Y	D	Y	26	Y	D	Y	37	Y
Xsec. 2	0.221	0.80	Y	D	Y	17	Y	D	Y	37	Y
Xsec. 3	0.277	0.80	Y	D	Y	16	Y	D	Y	41	Y
Xsec. 4	0.249	0.80	Y	D	Y	17	Y	D	Y	41	Y
Xsec. 5	0.149	0.82	Y	Y	Y	19	Y	Y	Y	37	Y

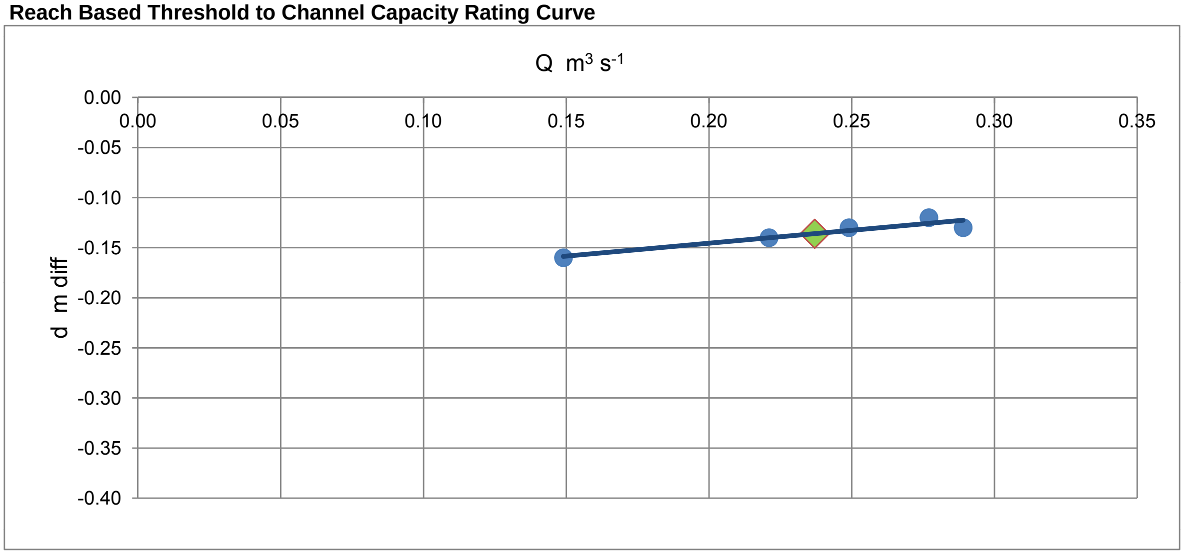
Stability Criteria Met: Y - Yes, N - No, D - Dynamic

* - within 5 mm

Dynamic Stability
Dynamic Stability = Cautionary
Unstable

	Q $m^3 s^{-1}$ existing	Q $m^3 s^{-1}$ stable	Q $m^3 s^{-1}$ diff	d m diff
Xsec. 1	0.89	0.29	0.61	-0.13
Xsec. 2	0.89	0.22	0.67	-0.14
Xsec. 3	0.89	0.28	0.61	-0.12
Xsec. 4	0.89	0.25	0.64	-0.13
Xsec. 5	0.89	0.15	0.74	-0.16
mean	**0.89**	**0.24**	0.65	-0.14

Reach Based Threshold to Channel Capacity Rating Curve



GEO - ESUM v.1.3 Erosion Threshold Summary Model

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Project: Erosion Threshold Analysis
Midtown Oakville
Lower Morrison Creek - downstream reach

Existing

	Q $m^3 s^{-1}$	V $m s^{-1}$	veg control	D_{50} particle	D_{84}-D_{100} particle	τ_{calc} $N m^{-2}$	veg control	D_{50} particle*	D_{84}-D_{100} particle*	Ω watts m^{-1}	Ω threshold
Xsec. 1	1.414	1.04	Y	Y	Y	21	Y	Y	Y	114	Y
Xsec. 2	1.410	1.06	Y	Y	Y	21	Y	Y	Y	111	Y
Xsec. 3	1.412	1.08	Y	Y	Y	21	Y	Y	Y	107	Y
Xsec. 4	1.413	1.11	Y	Y	Y	23	Y	Y	Y	125	Y
Xsec. 5	1.411	1.18	Y	Y	Y	30	Y	Y	Y	180	Y

Dynamic Stability

Xsec. 1											
Xsec. 2											
Xsec. 3											
Xsec. 4											
Xsec. 5											

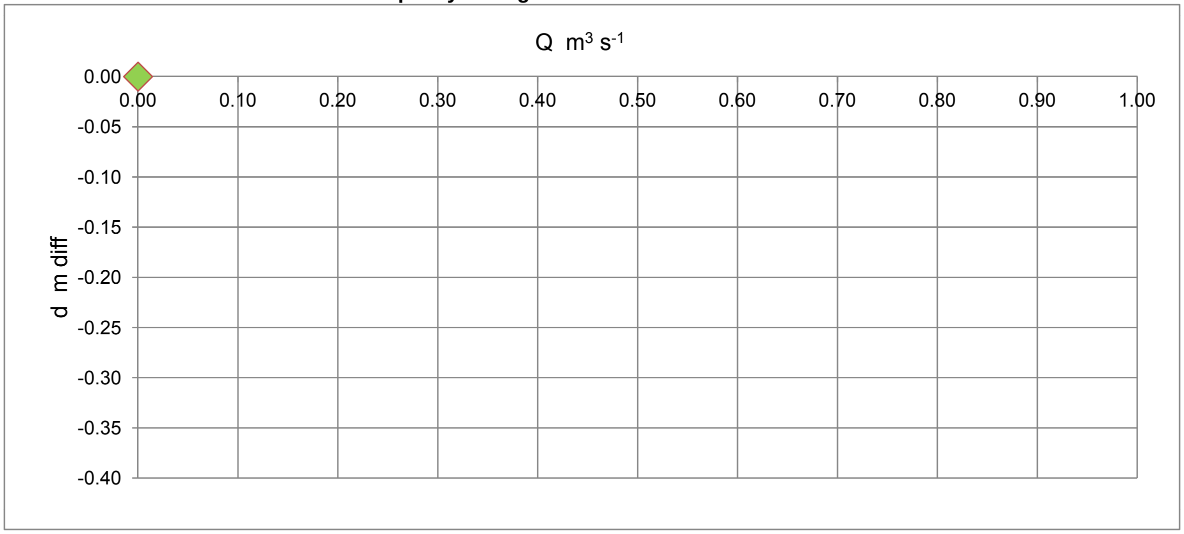
Stability Criteria Met: Y - Yes, N - No, D - Dynamic

* - within 5 mm

Dynamic Stability
Dynamic Stability = Cautionary
Unstable

	Q $m^3 s^{-1}$ existing	Q $m^3 s^{-1}$ stable	Q $m^3 s^{-1}$ diff	d m diff
Xsec. 1	1.41			
Xsec. 2	1.41			
Xsec. 3	1.41			
Xsec. 4	1.41			
Xsec. 5	1.41			
mean	**1.41**			

Reach Based Threshold to Channel Capacity Rating Curve



GEO - ESUM v.1.3 Erosion Threshold Summary Model

AquaLogic

B. de Geus 8.11

Project: Erosion Threshold Analysis
Midtown Oakville
Lower Wedgewood Creek

	Q $m^3 s^{-1}$	V $m s^{-1}$	veg control	D_{50} particle	D_{84}-D_{100} particle	τ_{calc} $N m^{-2}$	veg control	D_{50} particle*	D_{84}-D_{100} particle*	Ω watts m^{-1}	Ω threshold
Existing											
Xsec. 1	1.703	1.16	Y	Y	Y	23	Y	Y	Y	117	Y
Xsec. 2	1.704	1.11	Y	Y	Y	25	Y	Y	Y	142	Y
Xsec. 3	1.703	1.13	Y	Y	Y	26	Y	Y	Y	141	Y
Xsec. 4	1.700	1.29	N	N	Y	35	Y	N	Y	233	Y
Xsec. 5	1.702	1.48	N	Y	Y	55	N	Y	Y	383	Y
Dynamic Stability											
Xsec. 1	1.703	1.16	Y	Y	Y	23	Y	Y	Y	117	Y
Xsec. 2	1.704	1.11	Y	Y	Y	25	Y	Y	Y	142	Y
Xsec. 3	1.703	1.13	Y	Y	Y	26	Y	Y	Y	141	Y
Xsec. 4	1.188	1.14	Y	D	Y	30	Y	D	Y	163	Y
Xsec. 5	1.047	1.24	D	Y	Y	43	D	Y	Y	236	Y

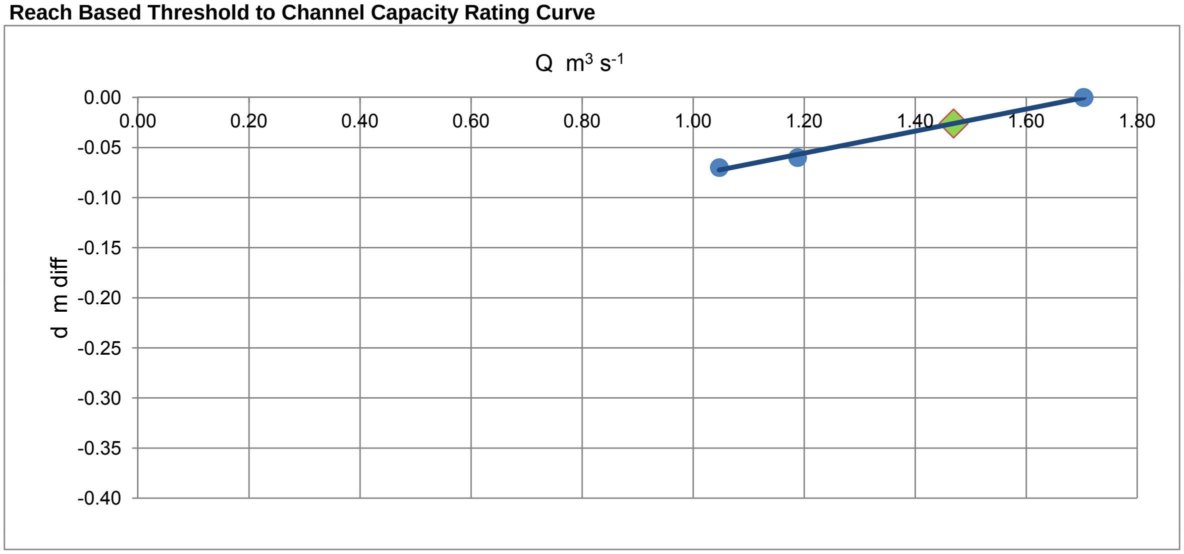
Stability Criteria Met: Y - Yes, N - No, D - Dynamic

* - within 5 mm

- Dynamic Stability
- Dynamic Stability = Cautionary
- Unstable

	Q $m^3 s^{-1}$ existing	Q $m^3 s^{-1}$ stable	Q $m^3 s^{-1}$ diff	d m diff
Xsec. 1	1.70	1.70	0.00	0.00
Xsec. 2	1.70	1.70	0.00	0.00
Xsec. 3	1.70	1.70	0.00	0.00
Xsec. 4	1.70	1.19	0.51	-0.06
Xsec. 5	1.70	1.05	0.66	-0.07
mean	**1.70**	**1.47**	0.23	-0.03

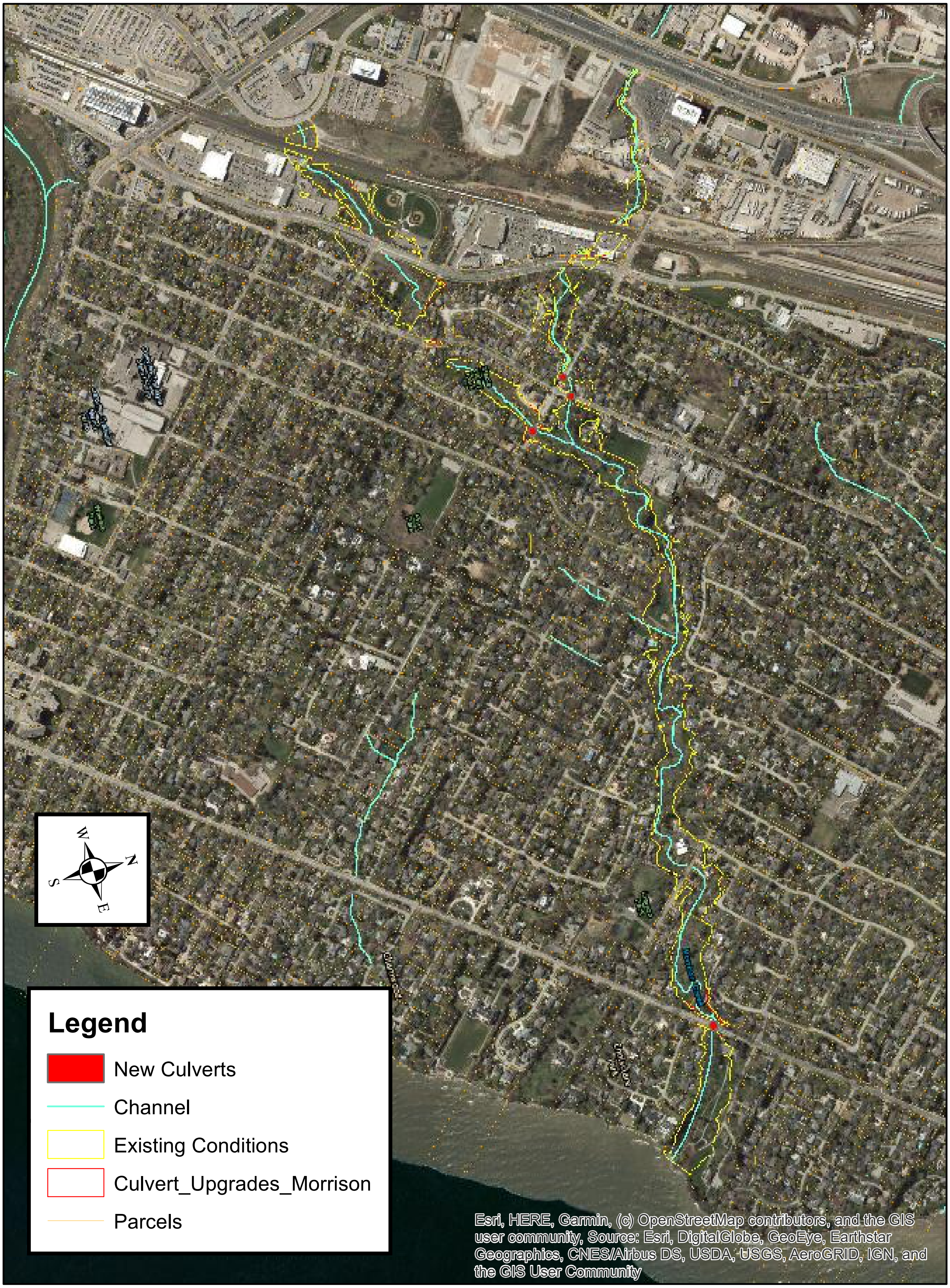
Reach Based Threshold to Channel Capacity Rating Curve



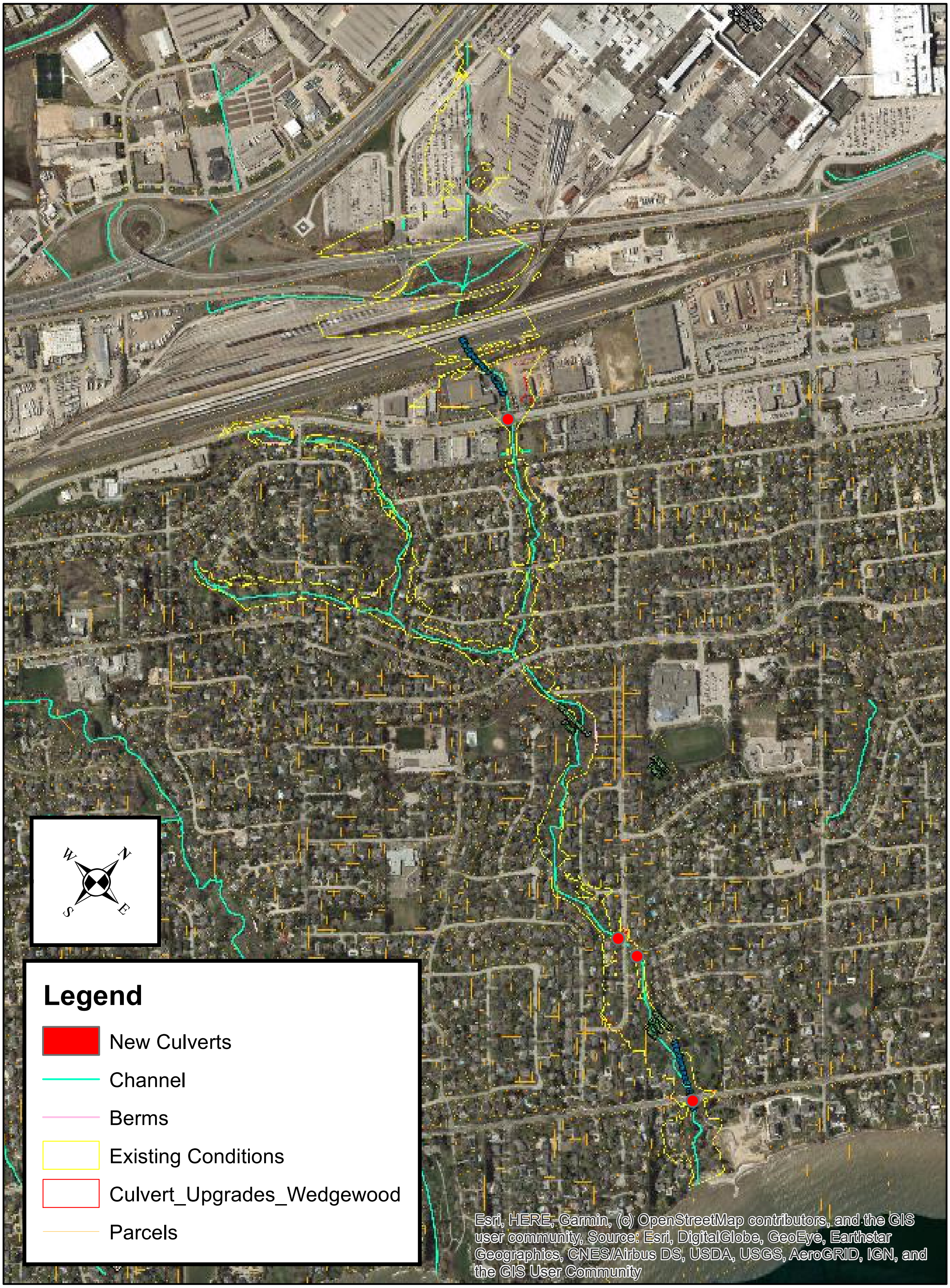
Appendix H

Invicta Drive Figures and Flood Mitigation Alternative Assessment Results

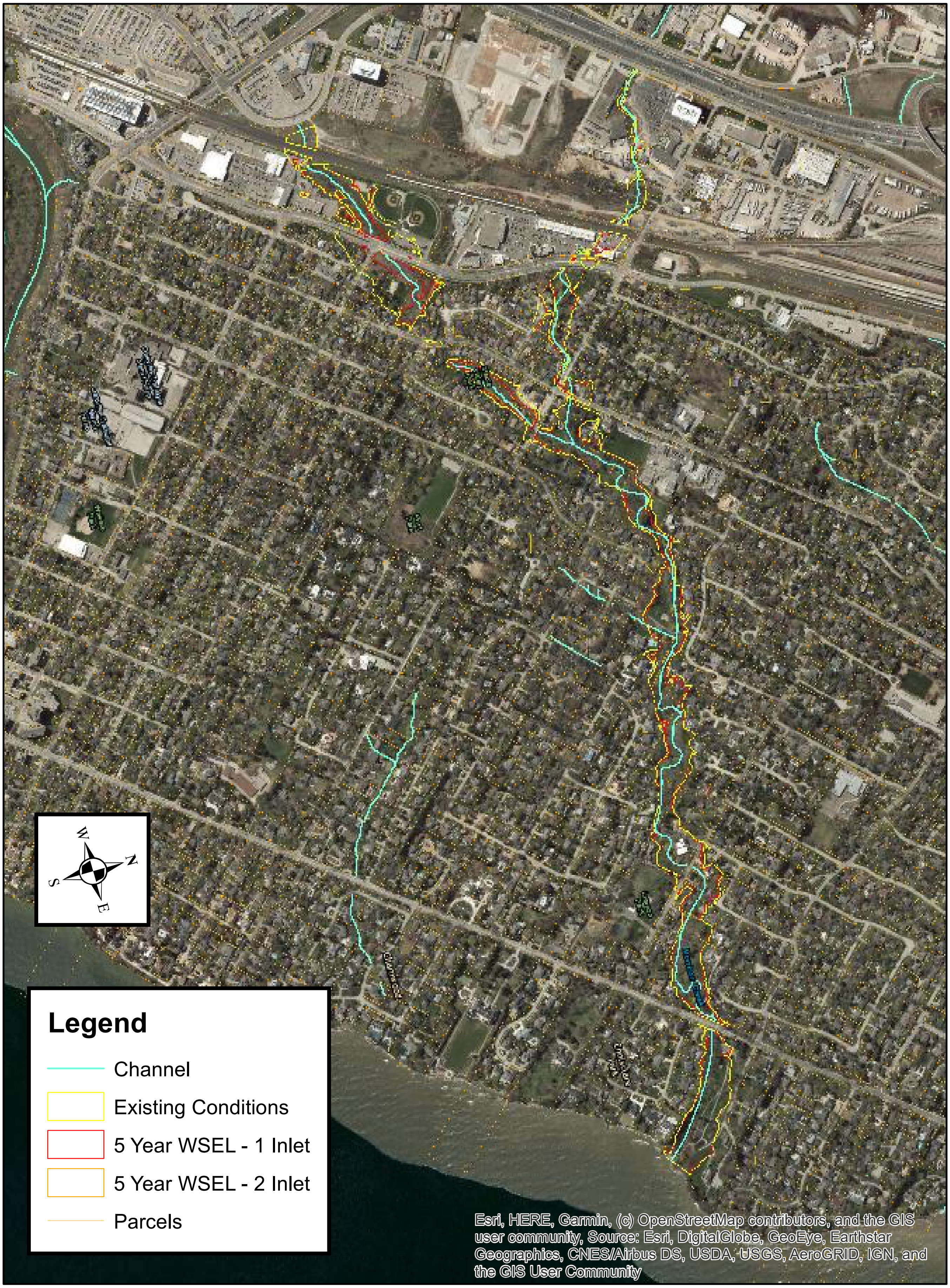
Drawing □ - Morrison Creek (100 Year Floodlines) with Culvert Upgrades



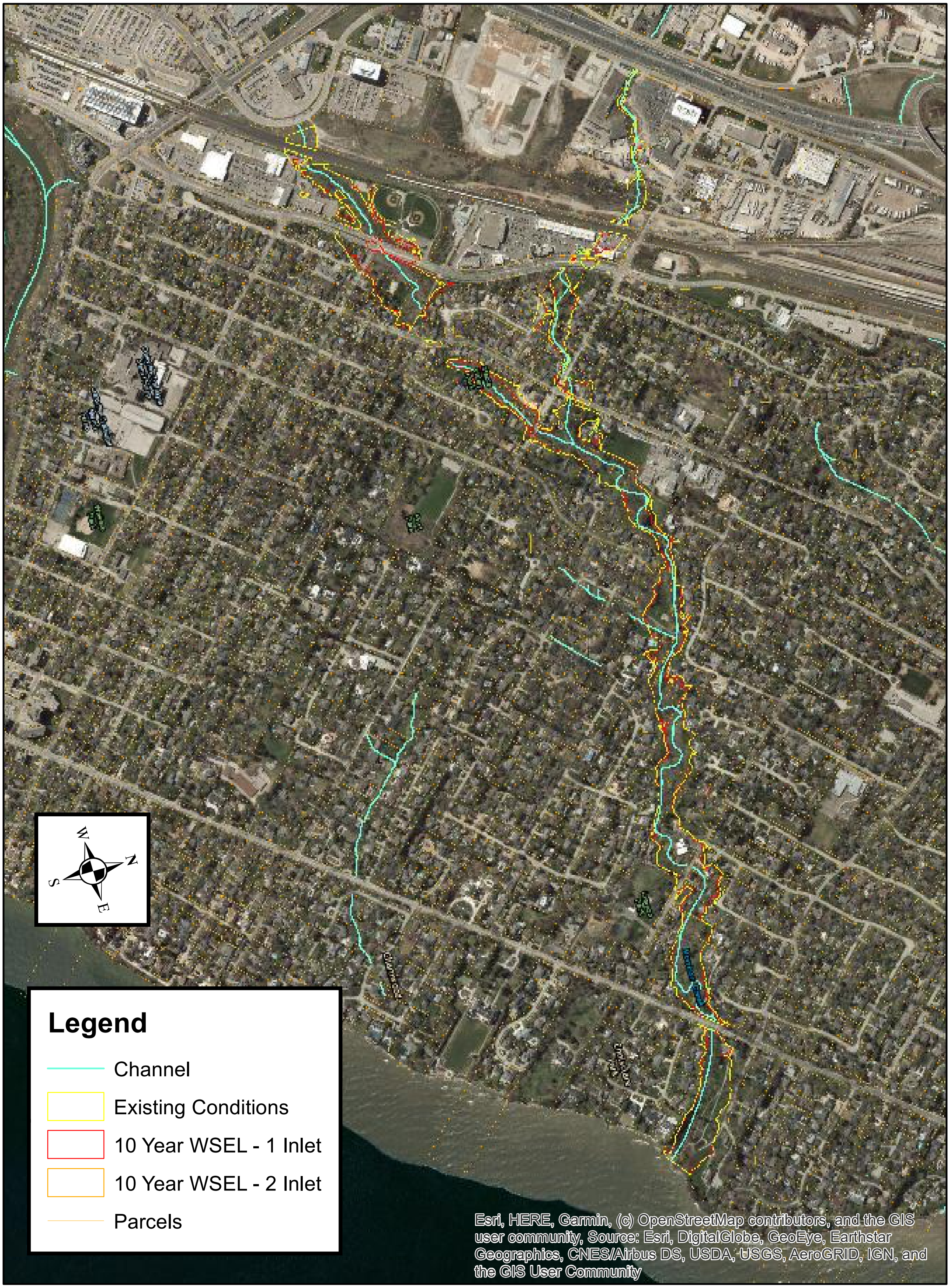
Drawing □ - Wedgewood Creek (100 Year Floodlines) with Culvert Upgrades



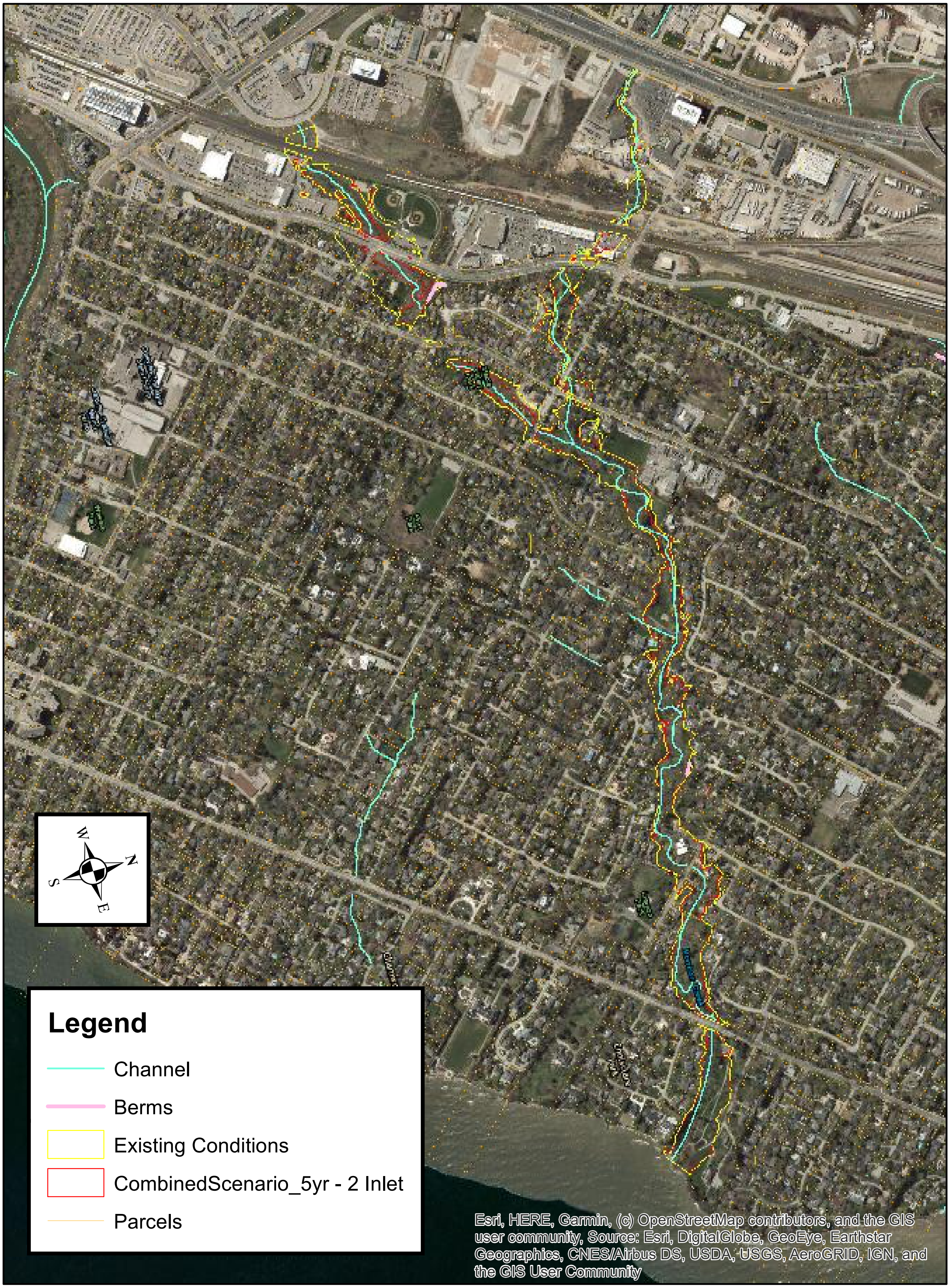
Drawing □ - Morrison Creek (100 Year Floodlines) with 5 Year Inlet WSELs

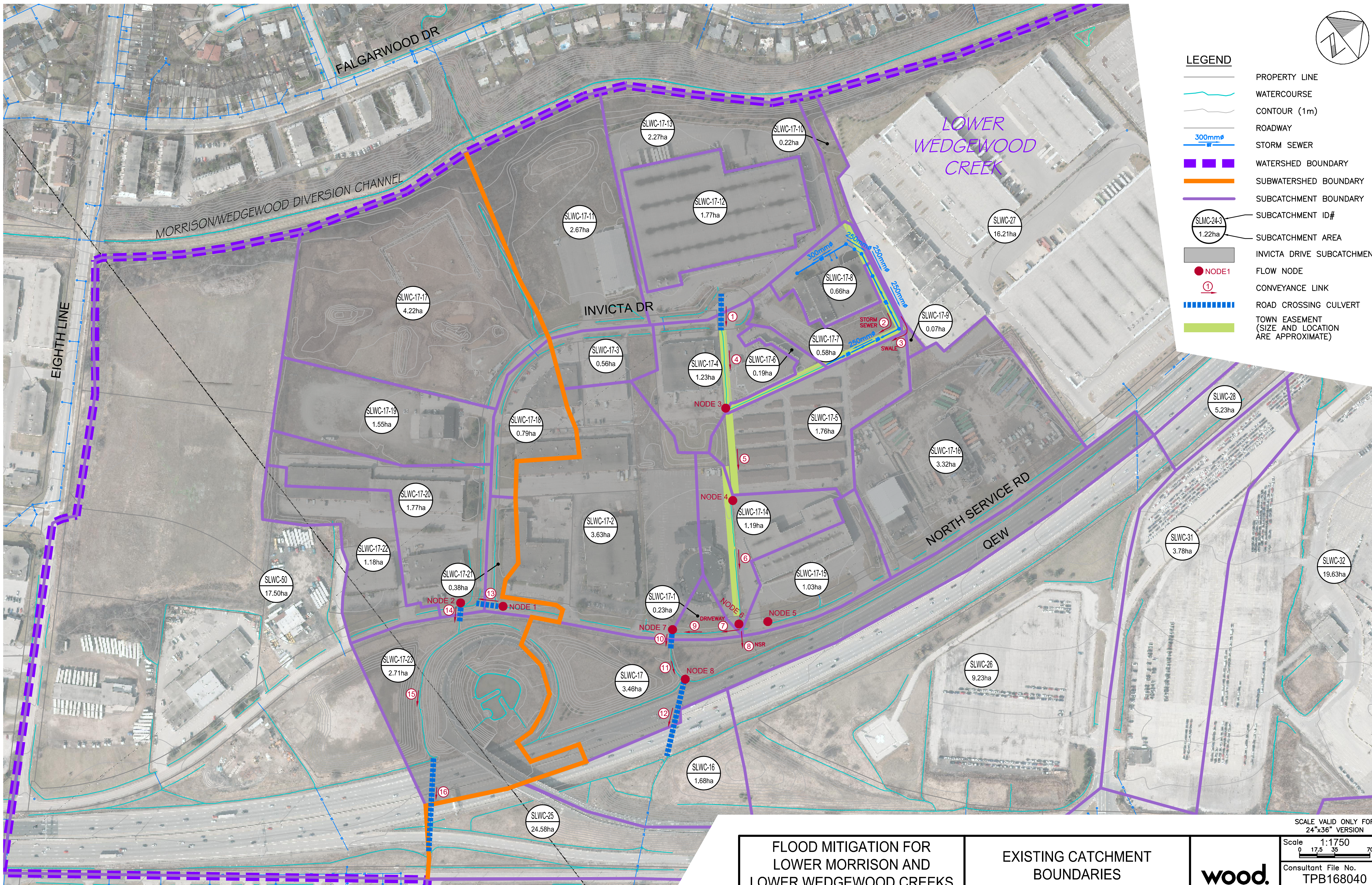


Drawing - Morrison Creek (100 Year Floodlines) with 10 Year Inlet WSELs



Drawing 5 - Morrison Creek (100 Year Floodlines) Combined Scenario with Culverts, 5 Year 2-Inlet WSELs, and Localized Berming



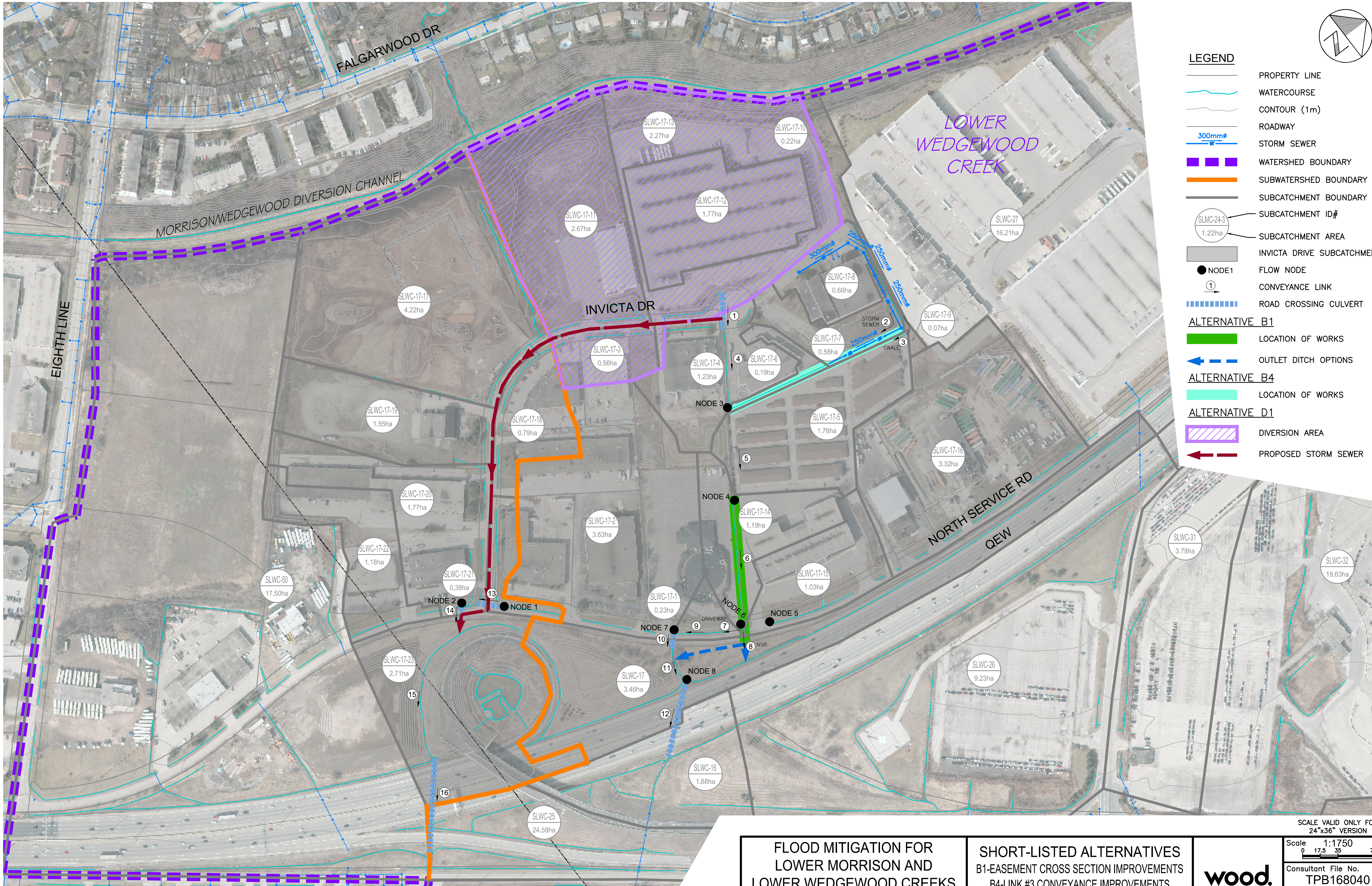


SCALE VALID ONLY FOR 24"x36" VERSION

FLOOD MITIGATION FOR LOWER MORRISON AND LOWER WEDGEWOOD CREEKS TOWN OF OAKVILLE	EXISTING CATCHMENT BOUNDARIES INVICTA DRIVE	wood.	Scale 1:1750 (0 17.5 35 70); Consultant File No. TPB168040; Figure No. 1

Path: I:\TPB168040 – LowerMorrison-Wedgewood\06_DES-ENG\01_CAD\02_DWGS\05_WR\01_PROJ\2021-05 (InvictaUpd)\Fig1 Catchment.dwg

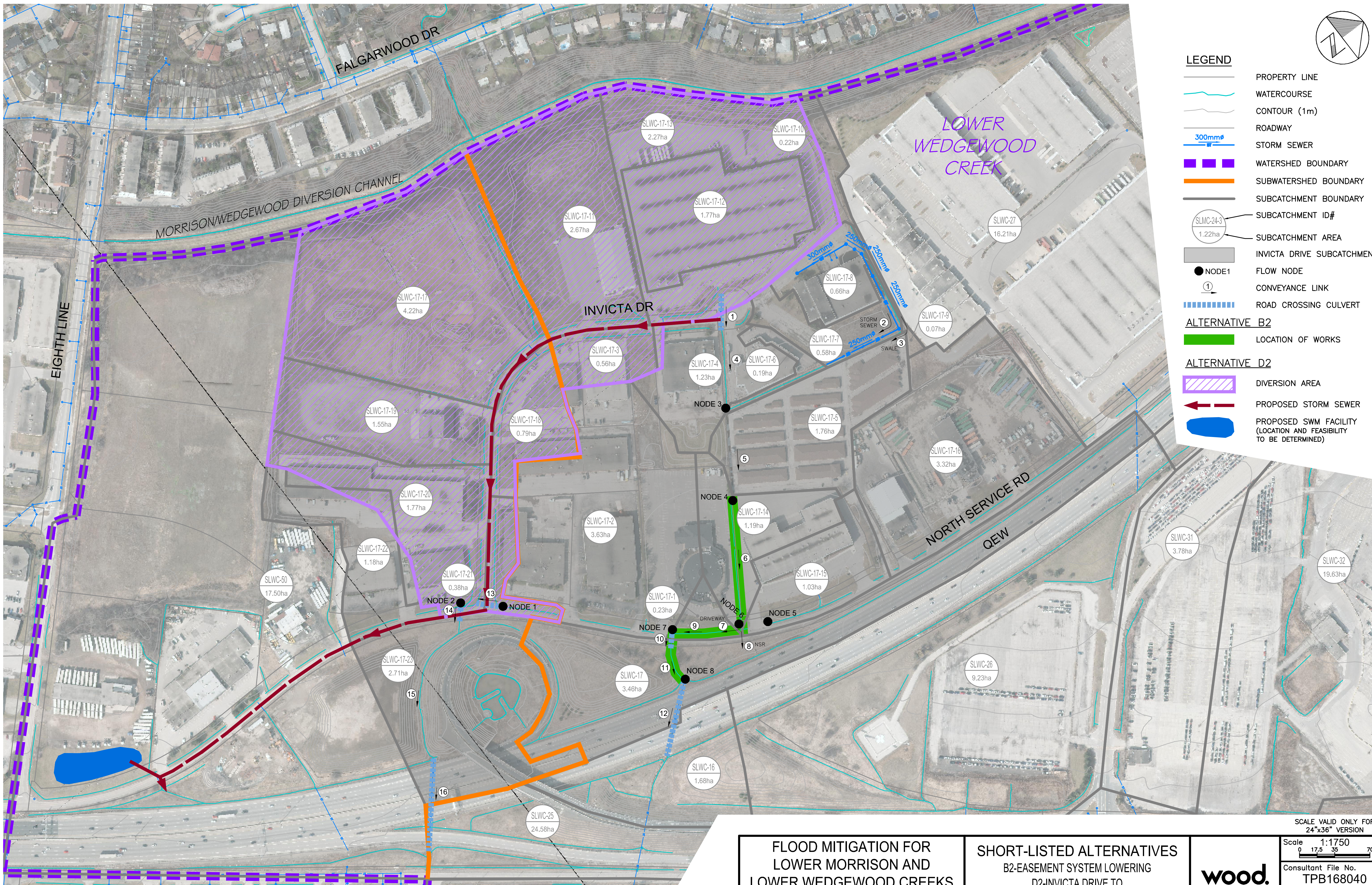
Plotted By: richard.bartolo
Last Saved By: richard.bartolo
Plotted: 2021-05-18
Last Saved: 2021-05-10



Path: I:\TPB168040 – LowerMorrison-Wedgewood\06_DES-ENG\01_CAD\02_DWGS\05_WR\01_PROJ\2021-05 (InvictaUpd)\Fig2-3 AlternativeWorks.dwg

Plotted By: richard.bartolo
Last Saved By: richard.bartolo
Plotted: 2021-05-18
Last Saved: 2021-05-10

FLOOD MITIGATION FOR LOWER MORRISON AND LOWER WEDGEWOOD CREEKS TOWN OF OAKVILLE	SHORT-LISTED ALTERNATIVES B1-EASEMENT CROSS SECTION IMPROVEMENTS B4-LINK #3 CONVEYANCE IMPROVEMENTS D1-NORTH INVICTA DRIVE DIVERSION	wood.	Scale 1:1750 (0 17.5 35 70)	Consultant File No. TPB168040 Figure No. 2



SCALE VALID ONLY FOR 24"x36" VERSION

FLOOD MITIGATION FOR LOWER MORRISON AND LOWER WEDGEWOOD CREEKS TOWN OF OAKVILLE	SHORT-LISTED ALTERNATIVES B2-EASEMENT SYSTEM LOWERING D2-INVICTA DRIVE TO EIGHTH LINE DIVERSION	wood.	Scale 1:1750 0 17.5 35 70	Consultant File No. TPB168040 Figure No. 3

Path: I:\TPB168040 – LowerMorrison-Wedgewood\06_DES-ENG\01_CAD\02_DWGS\05_WR\01_PROJ\2021-05 (InvictaUpd)\Fig2-3 AlternativeWorks.dwg

Plotted By: richard.bartolo
Last Saved By: richard.bartolo
Plotted: 2021-05-18
Last Saved: 2021-05-10

Appendix I

Cost Estimates

West Morrison Creek Flow Diversion to Sixteen Mile Creek					
Item	Unit of Measure	Estimated Quantity	Unit Cost ($)	Total Cost ($)	With Contingency (%15)
Inlet Structure/ Headwall	each	2	$ 34,729	$ 69,458	$ 79,876
3 m x 2.4 m inlet box culvert (twin)	Length (m)	12	$ 43,786	$ 525,432	$ 604,247
Custom MH Structures (Reduce from 3 m * 2.4 m to 1500 mm sewer)	each	2	$ 57,881	$ 115,763	$ 133,127
1500 mm diameter reinforced concrete pipes (Park to Cornwall Road)	Length (m)	10	$ 6,008	$ 60,081	$ 69,093
1500 mm diameter reinforced concrete pipe	Length (m)	800	$ 6,008	$ 4,806,459	$ 5,527,428
1500 mm diameter reinforced concrete outlet pipe	Length (m)	40	$ 6,008	$ 240,323	$ 276,371
Cast in Place Manhole (for 1500 mm diameter pipe)	each	10	$ 17,364	$ 173,644	$ 199,690
Outlet Drop Structure	each	1	$ 231,525	$ 231,525	$ 266,254
Outlet Headwall	each	1	$ 22,050	$ 22,050	$ 25,358
ESC and Dewatering	LS	1	$ 57,881	$ 57,881	$ 66,563
Revegetation	m2	675	$ 174	$ 117,210	$ 134,791
Mobilization and Demobilization	LS	1	$ 11,576	$ 11,576	$ 13,313
Notes: 1 - Costing does not include utilities or removal of municipal infrastructure			Sub Total	$ 6,431,401	$ 7,396,111

Location	LWMC Height (m)	Length (m)	Volume (m^3)
Bohemia Crescent	0.5	63.7	96
Botany Hill	0.5	26.7	40
Wedgewood Drive	0.5	65	98
Cynthia Lane	0.5	66	99
		221	332

Item	Unit of Measure	Estimated Quantity	Unit Cost ($)	Total Cost ($)	With Contingency ($)
Morrison Creek - West of Bohemia Crescent					
Fill	Volume (m_3)	96	$ 46	$ 4,445	$ 5,112.07
Landscaping	Area (m_2)	255	$ 23	$ 5,904	$ 6,789.47
Site Access/Removals/Replacements	Each	1	$ 23,153	$ 23,153	$ 26,625.38
Mobilization and Demobilization	Each	1	$ 11,025	$ 11,025	$ 12,678.75
			Sub Total	$ 44,527	$ 51,206
Morrison Creek - West of Botany Hill					
Fill	Volume (m_3)	40	$ 46	$ 1,852	$ 2,130.03
Landscaping	Area (m_2)	107	$ 23	$ 2,477	$ 2,848.92
Site Access/Removals/Replacements	Each	1	$ 23,153	$ 23,153	$ 26,625.38
Mobilization and Demobilization	Each	1	$ 11,025	$ 11,025	$ 12,678.75
			Sub Total	$ 38,507	$ 44,283
Wedgewood Creek - West of Wedgewood Drive					
Fill	Volume (m_3)	98	$ 46	$ 4,538	$ 5,218.57
Landscaping	Area (m_2)	260	$ 23	$ 6,020	$ 6,922.60
Site Access/Removals/Replacements	Each	2	$ 23,153	$ 46,305	$ 53,250.75
Mobilization and Demobilization	Item	2	$ 11,025	$ 22,050	$ 25,357.50
			Sub Total	$ 78,913	$ 90,749
Wedgewood Creek - South of Cynthia Lane					
Fill	Volume (m_3)	99	$ 46	$ 4,584	$ 5,271.82
Landscaping	Area (m_2)	264	$ 23	$ 6,112	$ 7,029.10
Site Access/Removals/Replacements	Each	1	$ 23,153	$ 23,153	$ 26,625.38
Mobilization and Demobilization	Item	1	$ 11,025	$ 11,025	$ 12,678.75
			Sub Total	$ 44,874	$ 51,605
			Grand Total	$ 206,820	$ 237,843

Total Cost for Morrison	$ 83,033.69	$ 95,489
Total Cost for Wedgewood	$ 123,786.50	$ 142,354

Culvert Upgrades						
Culvert Upgrades (Proposed Sizing)	Item	Unit of Measure	Estimated Quantity	Unit Cost ($)1	Total Cost ($)	With Contingency (%15)
	Morrison - Lakeshore Rd (14.6 x 3.35)	Length (m)	10	$ 67,605	$ 676,053	$ 777,460.95
	Morrison - Chartwell Rd (N. of Linbrook Rd - 6.4 x 2.13)	Length (m)	15	$ 29,635	$ 444,528	$ 511,207.20
	Morrison - Linbrook Rd (7.32 x 2.13)	Length (m)	6.9	$ 42,369	$ 292,347	$ 336,198.61
	Morrison - Chartwell Rd (S. of Linbrook Rd - 6.4 x 1.5)	Length (m)	16.3	$ 29,635	$ 483,054	$ 555,511.82
	Wedgewood - Lakeshore Rd (14.6 x 3.05)	Length (m)	15.1	$ 67,605	$ 1,020,840	$ 1,173,966.03
	Wedgewood - Warren Dr Park (7.3 x 1.52)	Length (m)	29.5	$ 33,803	$ 997,178	$ 1,146,754.90
	Wedgewood - Wedgewood Dr (7.3 x 1.52)	Length (m)	21.2	$ 33,803	$ 716,616	$ 824,108.61
	Wedgewood - Cornwall Rd (N. of SWM Facility - 7.3 x 1.52)	Length (m)	33.6	$ 33,803	$ 1,135,769	$ 1,306,134.40
				Sub-Total	$ 5,766,385	$ 6,631,343
Miscellaneous	Item	Unit of Measure	Estimated Quantity	Unit Cost ($)	Total Cost ($)	With Contingency (%15)
	Dewatering	Unit	8	28940.625	$ 231,525	$ 266,253.75
	Temporary Flow Controls	Unit	8	34728.75	$ 277,830	$ 319,504.50
	Traffic Control	Unit	8	23152.5	$ 185,220	$ 213,003.00
Notes: 1 - Costing does not include utilities or removal of municipal infrastructure				Sub-Total	$ 694,575	$ 798,761
				Grand Total	$ 6,460,960	$ 7,430,104
1. Unit Cost is based on Deck Area of $4000/m^2						

Cornwall Road Park Flood Storage Tank						
PIPES	Item	Unit of Measure	Estimated Quantity	Unit Cost ($)	Total Cost ($)	With Contingency (%15)
	Inlet Structure/ Headwall	each	2	$ 34,729	$ 69,458	$ 79,876.13
	3 m x 2.4 m inlet box culvert (twin)	Length (m)	12	$ 43,786	$ 525,432	$ 604,246.91
	Outlet Headwall	each	1	$ 5,788	$ 5,788	$ 6,656.34
				Sub-Total	$ 600,678	$ 690,779
TANK	Item	Unit of Measure	Estimated Quantity	Unit Cost ($)	Total Cost ($)	With Contingency (%15)
	Tank	Volume (m3)	10800	$ 405	$ 4,375,823	$ 5,032,195.88
	Excavated Soil Treatment	Volume (m3)	18000	$ 58	$ 1,041,863	$ 1,198,141.88
	Pump System	LS	1	$ 115,763	$ 115,763	$ 133,126.88
				Sub-Total	$ 5,533,448	$ 6,363,465
Erosion and Sedimentation	Item	Unit of Measure	Estimated Quantity	Unit Cost ($)	Total Cost ($)	With Contingency (%15)
	ESC and Dewatering	Unit	1	$ 57,881	$ 57,881	$ 66,563.44
				Sub-Total	$ 57,881	$ 66,563
Miscellaneous	Item	Unit of Measure	Estimated Quantity	Unit Cost ($)	Total Cost ($)	With Contingency (%15)
	Mobilization and Demobilization	LS	1	$ 11,576	$ 11,576	$ 13,312.69
	Revegetation	Area (m2)	150	$ 174	$ 26,047	$ 29,953.55
	Topsoil and sod	Area (m2)	4320	$ 6	$ 25,005	$ 28,755.41
Notes: 1 - Costing does not include utilities or removal of municipal infrastructure				Sub-Total	$ 62,628	$ 72,022
				Grand Total	$ 6,254,634	$ 7,192,829
				Cost per m3 of storage		$ 666

Appendix J

Archaeological and Cultural Heritage Assessment

Ontario

Ministry of Tourism, Culture and Sport

Programs & Services Branch
401 Bay Street, Suite 1700
Toronto ON M7A 0A7

Criteria for Evaluating Archaeological Potential

A Checklist for the Non-Specialist

The **purpose of the checklist** is to determine:

- if a property(ies) or project area may contain archaeological resources i.e., have archaeological potential
- it includes all areas that may be impacted by project activities, including – but not limited to:
  - the main project area
  - temporary storage
  - staging and working areas
  - temporary roads and detours

Processes covered under this checklist, such as:

- *Planning Act*
- *Environmental Assessment Act*
- *Aggregates Resources Act*
- *Ontario Heritage Act* – Standards and Guidelines for Conservation of Provincial Heritage Properties

Archaeological assessment

If you are not sure how to answer one or more of the questions on the checklist, you may want to hire a licensed consultant archaeologist (see page 4 for definitions) to undertake an archaeological assessment.

The assessment will help you:

- identify, evaluate and protect archaeological resources on your property or project area
- reduce potential delays and risks to your project

Note: By law, archaeological assessments **must** be done by a licensed consultant archaeologist. Only a licensed archaeologist can assess – or alter – an archaeological site.

What to do if you:

- **find an archaeological resource**

  If you find something you think may be of archaeological value during project work, you must – by law – stop all activities immediately and contact a licensed consultant archaeologist
  The archaeologist will carry out the fieldwork in compliance with the *Ontario Heritage Act* [s.48(1)].
- **unearth a burial site**

  If you find a burial site containing human remains, you must immediately notify the appropriate authorities (i.e., police, coroner's office, and/or Registrar of Cemeteries) and comply with the *Funeral, Burial and Cremation Services Act*.

Other checklists

Please use a separate checklist for your project, if:

- you are seeking a Renewable Energy Approval under Ontario Regulation 359/09 – separate checklist
- your Parent Class EA document has an approved screening criteria (as referenced in Question 1)

Please refer to the Instructions pages when completing this form.

Project or Property Name

Flood Mitigation Opportunities Study Lower Morrison and Lower Wedgewood Creeks

Project or Property Location (upper and lower or single tier municipality)

Cornwall Road Park, 439 Cornwall Road, Oakville. Property location is the west side of the park.

Proponent Name

Town of Oakville

Proponent Contact Information

Diana Michalakos, Diana.Michalakos@oakville.ca

Screening Questions

	Yes	No
1. Is there a pre-approved screening checklist, methodology or process in place?		4

If Yes, please follow the pre-approved screening checklist, methodology or process.

If No, continue to Question 2.

	Yes	No
2. Has an archaeological assessment been prepared for the property (or project area) and been accepted by MTCS?		4

If Yes, do **not** complete the rest of the checklist. You are expected to follow the recommendations in the archaeological assessment report(s).

The proponent, property owner and/or approval authority will:

- summarize the previous assessment
- add this checklist to the project file, with the appropriate documents that demonstrate an archaeological assessment was undertaken e.g., MTCS letter stating acceptance of archaeological assessment report

The summary and appropriate documentation may be:

- submitted as part of a report requirement e.g., environmental assessment document
- maintained by the property owner, proponent or approval authority

If No, continue to Question 3.

	Yes	No
3. Are there known archaeological sites on or within 300 metres of the property (or the project area)?		4
4. Is there Aboriginal or local knowledge of archaeological sites on or within 300 metres of the property (or project area)?		4
5. Is there Aboriginal knowledge or historically documented evidence of past Aboriginal use on or within 300 metres of the property (or project area)?		4
6. Is there a known burial site or cemetery on the property or adjacent to the property (or project area)?		4
7. Has the property (or project area) been recognized for its cultural heritage value?		4

If Yes to any of the above questions (3 to 7), do **not** complete the checklist. Instead, you need to hire a licensed consultant archaeologist to undertake an archaeological assessment of your property or project area.

If No, continue to question 8.

	Yes	No
8. Has the entire property (or project area) been subjected to recent, extensive and intensive disturbance?		4

If Yes to the preceding question, do **not** complete the checklist. Instead, please keep and maintain a summary of documentation that provides evidence of the recent disturbance.

An archaeological assessment is not required.

If No, continue to question 9.

	Yes	No
9. Are there present or past water sources within 300 metres of the property (or project area)?	4	

If Yes, an archaeological assessment is required.

If No, continue to question 10.

	Yes	No
10. Is there evidence of two or more of the following on the property (or project area)?		4

- elevated topography
- pockets of well-drained sandy soil
- distinctive land formations
- resource extraction areas
- early historic settlement
- early historic transportation routes

If Yes, an archaeological assessment is required.

If No, there is low potential for archaeological resources at the property (or project area).

The proponent, property owner and/or approval authority will:

- summarize the conclusion
- add this checklist with the appropriate documentation to the project file

The summary and appropriate documentation may be:

- submitted as part of a report requirement e.g., under the *Environmental Assessment Act, Planning Act* processes
- maintained by the property owner, proponent or approval authority

Instructions

Please have the following available, when requesting information related to the screening questions below:

- a clear map showing the location and boundary of the property or project area
  - large scale and small scale showing nearby township names for context purposes
- the municipal addresses of all properties within the project area
- the lot(s), concession(s), and parcel number(s) of all properties within a project area

In this context, the following definitions apply:

- **consultant archaeologist** means, as defined in Ontario regulation as an archaeologist who enters into an agreement with a client to carry out or supervise archaeological fieldwork on behalf of the client, produce reports for or on behalf of the client and provide technical advice to the client. In Ontario, these people also are required to hold a valid professional archaeological licence issued by the Ministry of Tourism, Culture and Sport.
- **proponent** means a person, agency, group or organization that carries out or proposes to carry out an undertaking or is the owner or person having charge, management or control of an undertaking.

1. Is there a pre-approved screening checklist, methodology or process in place?

An existing checklist, methodology or process may be already in place for identifying archaeological potential, including:

- one prepared and adopted by the municipality e.g., archaeological management plan
- an environmental assessment process e.g., screening checklist for municipal bridges
- one that is approved by the Ministry of Tourism, Culture and Sport under the Ontario government's Standards & Guidelines for Conservation of Provincial Heritage Properties [s. B.2.]

2. Has an archaeological assessment been prepared for the property (or project area) and been accepted by MTCS?

Respond 'yes' to this question, if all of the following are true:

- an archaeological assessment report has been prepared and is in compliance with MTCS requirements
  - a letter has been sent by MTCS to the licensed archaeologist confirming that MTCS has added the report to the Ontario Public Register of Archaeological Reports (Register)
- the report states that there are no concerns regarding impacts to archaeological sites

Otherwise, if an assessment has been completed and deemed compliant by the MTCS, and the ministry recommends further archaeological assessment work, this work will need to be completed.

For more information about archaeological assessments, contact:

- approval authority
- proponent
- consultant archaeologist
- Ministry of Tourism, Culture and Sport at archaeology@ontario.ca

3. Are there known archaeological sites on or within 300 metres of the property (or project area)?

MTCS maintains a database of archaeological sites reported to the ministry.

For more information, contact MTCS Archaeological Data Coordinator at archaeology@ontario.ca.

4. Is there Aboriginal or local knowledge of archaeological sites on or within 300 metres of the property?

Check with:

- Aboriginal communities in your area
- local municipal staff

They may have information about archaeological sites that are not included in MTCS' database.

Other sources of local knowledge may include:

- property owner
- local heritage organizations and historical societies
- local museums
- municipal heritage committee
- published local histories

5. Is there Aboriginal knowledge or historically documented evidence of past Aboriginal use on or within 300 metres of the property (or property area)?

Check with:

- Aboriginal communities in your area
- local municipal staff

Other sources of local knowledge may include:

- property owner
- local heritage organizations and historical societies
- local museums
- municipal heritage committee
- published local histories

6. Is there a known burial site or cemetery on the property or adjacent to the property (or project area)?

For more information on known cemeteries and/or burial sites, see:

- Cemeteries Regulation Unit, Ontario Ministry of Consumer Services – for database of registered cemeteries
- Ontario Genealogical Society (OGS) – to locate records of Ontario cemeteries, both currently and no longer in existence; cairns, family plots and burial registers
- Canadian County Atlas Digital Project – to locate early cemeteries

In this context, 'adjacent' means 'contiguous', or as otherwise defined in a municipal official plan.

7. Has the property (or project area) been recognized for its cultural heritage value?

There is a strong chance there may be archaeological resources on your property (or immediate area) if it has been listed, designated or otherwise identified as being of cultural heritage value by:

- your municipality
- Ontario government
- Canadian government

This includes a property that is:

- designated under *Ontario Heritage Act* (the OHA), including:
  - individual designation (Part IV)
  - part of a heritage conservation district (Part V)
  - an archaeological site (Part VI)
- subject to:
  - an agreement, covenant or easement entered into under the OHA (Parts II or IV)
  - a notice of intention to designate (Part IV)
  - a heritage conservation district study area by-law (Part V) of the OHA
- listed on:
  - a municipal register or inventory of heritage properties
  - Ontario government's list of provincial heritage properties
  - Federal government's list of federal heritage buildings
- part of a:
  - National Historic Site
  - UNESCO World Heritage Site
- designated under:
  - *Heritage Railway Station Protection Act*
  - *Heritage Lighthouse Protection Act*
- subject of a municipal, provincial or federal commemorative or interpretive plaque.

To determine if your property or project area is covered by any of the above, see:

- Part A of the MTCS Criteria for Evaluating Potential for Built Heritage and Cultural Heritage Landscapes

Part VI – Archaeological Sites

Includes five sites designated by the Minister under Regulation 875 of the Revised Regulation of Ontario, 1990 (Archaeological Sites) and 3 marine archaeological sites prescribed under Ontario Regulation 11/06.

For more information, check Regulation 875 and Ontario Regulation 11/06.

8. Has the entire property (or project area) been subjected to recent extensive and intensive ground disturbance?

Recent: after-1960

Extensive: over all or most of the area

Intensive: thorough or complete disturbance

Examples of ground disturbance include:

- quarrying
- major landscaping – involving grading below topsoil
- building footprints and associated construction area
  - where the building has deep foundations or a basement
- infrastructure development such as:
  - sewer lines
  - gas lines
  - underground hydro lines
  - roads
  - any associated trenches, ditches, interchanges. **Note**: this applies only to the excavated part of the right-of-way; the remainder of the right-of-way or corridor may not have been impacted.

A ground disturbance does **not** include:

- agricultural cultivation
- gardening
- landscaping

Site visits

You can typically get this information from a site visit. In that case, please document your visit in the process (e.g., report) with:

- photographs
- maps
- detailed descriptions

If a disturbance isn't clear from a site visit or other research, you need to hire a licensed consultant archaeologist to undertake an archaeological assessment.

9. Are there present or past water bodies within 300 metres of the property (or project area)?

Water bodies are associated with past human occupations and use of the land. About 80-90% of archaeological sites are found within 300 metres of water bodies.

Present

- Water bodies:
  - primary - lakes, rivers, streams, creeks
  - secondary - springs, marshes, swamps and intermittent streams and creeks
- accessible or inaccessible shoreline, for example:
  - high bluffs
  - swamps
  - marsh fields by the edge of a lake
  - sandbars stretching into marsh

Water bodies not included:

- man-made water bodies, for example:
    - temporary channels for surface drainage
    - rock chutes and spillways
    - temporarily ponded areas that are normally farmed
    - dugout ponds
- artificial bodies of water intended for storage, treatment or recirculation of:
    - runoff from farm animal yards
    - manure storage facilities
    - sites and outdoor confinement areas

Past

Features indicating past water bodies:

- raised sand or gravel beach ridges – can indicate glacial lake shorelines
- clear dip in the land – can indicate an old river or stream
- shorelines of drained lakes or marshes
- cobble beaches

You can get information about water bodies through:

- a site visit
- aerial photographs
- 1:10,000 scale Ontario Base Maps - or equally detailed and scaled maps.

10. Is there evidence of two or more of the following on the property (or project area)?

- elevated topography
- pockets of well-drained sandy soil
- distinctive land formations
- resource extraction areas
- early historic settlement
- early historic transportation routes

- **Elevated topography**

  Higher ground and elevated positions - surrounded by low or level topography - often indicate past settlement and land use.

  Features such as eskers, drumlins, sizeable knolls, plateaus next to lowlands, or other such features are a strong indication of archaeological potential.

  Find out if your property or project area has elevated topography, through:

  - site inspection
  - aerial photographs
  - topographical maps

- **Pockets of well-drained sandy soil, especially within areas of heavy soil or rocky ground**

  Sandy, well-drained soil - in areas characterized by heavy soil or rocky ground - may indicate archaeological potential

  Find out if your property or project area has sandy soil through:

  - site inspection
  - soil survey reports

- **Distinctive land formations**

  Distinctive land formations include – but are not limited to:

  - waterfalls
  - rock outcrops
  - rock faces
  - caverns
  - mounds, etc.

  They were often important to past inhabitants as special or sacred places. The following sites may be present – or close to – these formations:

  - burials
  - structures
  - offerings
  - rock paintings or carvings

  Find out if your property or project areas has a distinctive land formation through:

  - a site visit
  - aerial photographs
  - 1:10,000 scale Ontario Base Maps - or equally detailed and scaled maps.

- **Resource extraction areas**

  The following resources were collected in these extraction areas:

  - food or medicinal plants e.g., migratory routes, spawning areas, prairie
  - scarce raw materials e.g., quartz, copper, ochre or outcrops of chert
  - resources associated with early historic industry e.g., fur trade, logging, prospecting, mining

  Aboriginal communities may hold traditional knowledge about their past use or resources in the area.

- **Early historic settlement**

  Early Euro-Canadian settlement include – but are not limited to:

  - early military or pioneer settlement e.g., pioneer homesteads, isolated cabins, farmstead complexes
  - early wharf or dock complexes
  - pioneers churches and early cemeteries

  For more information, see below – under the early historic transportation routes.

- **Early historic transportation routes** - such as trails, passes, roads, railways, portage routes, canals.

  For more information, see:

  - historical maps and/or historical atlases
    - for information on early settlement patterns such as trails (including Aboriginal trails), monuments, structures, fences, mills, historic roads, rail corridors, canals, etc.
    - Archives of Ontario holds a large collection of historical maps and historical atlases
    - digital versions of historic atlases are available on the Canadian County Atlas Digital Project
  - commemorative markers or plaques such as local, provincial or federal agencies
  - municipal heritage committee or other local heritage organizations
    - for information on early historic settlements or landscape features (e.g., fences, mill races, etc.)
    - for information on commemorative markers or plaques

Project or Property Name

Flood Mitigation Opportunities Study Lower Morrison and Lower Wedgewood Creeks

Project or Property Location (upper and lower or single tier municipality)

Cornwall Road Park, 439 Cornwall Road,Oakville. Property location is the west side

Proponent Name

Town of Oakville

Proponent Contact Information

Telephone Number	Fax Number	Email Address
		Diana Michalakos@oakville.ca

Screening Questions

[illegible]

- [ ] Yes
- [x] No

[illegible]

[illegible]

- [ ] Yes
- [x] No

[illegible]

[illegible]

- [ ] Yes
- [x] No

[illegible]

- [ ] Yes
- [x] No

[illegible]

- [ ] Yes
- [x] No

[illegible]

- [ ] Yes
- [x] No

[illegible]

- [ ] Yes
- [x] No

[illegible]

[illegible]

- [ ] Yes
- [x] No

[illegible]

[illegible]

☐ Yes ☒ No

[illegible]

☐ Yes ☒ No

[illegible]

11. [illegible]

☐ Yes ☒ No

[illegible]

☐ Yes ☒ No

[illegible]

☐ Yes ☒ No

[illegible]

☐ Yes ☒ No

[illegible]

- [illegible] *Environmental Assessment Act Planning Act* [illegible]
- [illegible]

Instructions

[illegible]

- [illegible]
- [illegible]
- [illegible]
- [illegible]

[illegible]

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[illegible]

[illegible]

- [illegible]
- [illegible]
- [illegible] *Environmental Assessment Act*
- [illegible] [Standards & Guidelines for Conservation of Provincial Heritage Properties](#) [s. B.2.]

[illegible]

[illegible]

- [illegible]
- [illegible]

[illegible]

[illegible]

- [illegible]
- [illegible] archaeology@ontario.ca

[illegible]

[illegible] archaeology@ontario.ca.

[illegible]

[illegible]

- local heritage organizations and historical societies, Association for Great Lakes Maritime History
  [illegible] (Save Ontario Shipwrecks, Ontario Underwater Council), Preserve Our Wrecks, Ontario Marine Heritage Committee)
- [illegible]
- municipal heritage committees

[illegible]

- local heritage organizations and historical societies
- municipal heritage committees

[illegible]

- [illegible] database of registered cemeteries
  [illegible] to locate records of Ontario cemeteries, both currently and no longer [illegible]
- [illegible] locate early cemeteries

[illegible]

- Ontario Heritage Act

- *Heritage Railway Station Protection Act*
- *Heritage Lighthouse Protection Act*

- Criteria for Evaluating Potential for Built Heritage and Cultural Heritage Landscapes

For more information, refer to Regulation 875 and Ontario Regulation 11/06.

11. [illegible]

[illegible]

[Criteria for Evaluating Potential for Built Heritage Resources and Cultural Heritage Landscapes]

[illegible]

...n, the following resources were collected in these extraction ar...

- ...medicinal plants e.g. migratory routes, spawning areas, prairie
- ...aw materials e.g. quartz, copper, ochre or outcrops of chert
- ...s associated with early historic industry e.g. fur trade, logging, ...

...unities may hold traditional knowledge about their past use or ...

- ... maps or atlases
  - ...formation on early settlement patterns such as trails (including Aboriginal trails), monuments, ...tures, fences, mills, historic roads, rail corridors, canals, etc.
  - [Archives of Ontario](#) holds a large collection of historical maps and atlases
  - ... [Canadian County Atlas Digital Project](#)
- ... [provincial](#) or [federal](#) agencies
- [municipal heritage committees](#) or [other local heritage organizations](#)

Ministry of Tourism,
Culture and Sport
Programs & Services Branch
401 Bay Street, Suite 1700
Toronto ON M7A 0A7

Criteria for Evaluating Potential for Built Heritage Resources and Cultural Heritage Landscapes

A Checklist for the Non-Specialist

The **purpose of the checklist** is to determine:

- if a property(ies) or project area:
    - is a recognized heritage property
    - may be of cultural heritage value
- it includes all areas that may be impacted by project activities, including – but not limited to:
    - the main project area
    - temporary storage
    - staging and working areas
    - temporary roads and detours

Processes covered under this checklist, such as:

- *Planning Act*
- *Environmental Assessment Act*
- *Aggregates Resources Act*
- *Ontario Heritage Act* – Standards and Guidelines for Conservation of Provincial Heritage Properties

Cultural Heritage Evaluation Report (CHER)

If you are not sure how to answer one or more of the questions on the checklist, you may want to hire a qualified person(s) (see page 5 for definitions) to undertake a cultural heritage evaluation report (CHER).

The CHER will help you:

- identify, evaluate and protect cultural heritage resources on your property or project area
- reduce potential delays and risks to a project

Other checklists

Please use a separate checklist for your project, if:

- you are seeking a Renewable Energy Approval under Ontario Regulation 359/09 – separate checklist
- your Parent Class EA document has an approved screening criteria (as referenced in Question 1)

Please refer to the Instructions pages for more detailed information and when completing this form.

Project or Property Name
Flood Mitigation Opportunities Study Lower Morrison and Lower Wedgewood Creeks

Project or Property Location (upper and lower or single tier municipality)
Cornwall Road Park, 439 Cornwall Road, Oakville. Property loaction is the west side of the park

Proponent Name
Town of Oakville

Proponent Contact Information
Diana Michalakos, Diana.Michalakos@oakville.ca

Screening Questions

	Yes	No
1. Is there a pre-approved screening checklist, methodology or process in place?		4

If Yes, please follow the pre-approved screening checklist, methodology or process.

If No, continue to Question 2.

Part A: Screening for known (or recognized) Cultural Heritage Value

	Yes	No
2. Has the property (or project area) been evaluated before and found **not** to be of cultural heritage value?		4

If Yes, do **not** complete the rest of the checklist.

The proponent, property owner and/or approval authority will:

- summarize the previous evaluation and
- add this checklist to the project file, with the appropriate documents that demonstrate a cultural heritage evaluation was undertaken

The summary and appropriate documentation may be:

- submitted as part of a report requirement
- maintained by the property owner, proponent or approval authority

If No, continue to Question 3.

	Yes	No
3. Is the property (or project area):		
a. identified, designated or otherwise protected under the *Ontario Heritage Act* as being of cultural heritage value?		4
b. a National Historic Site (or part of)?		4
c. designated under the *Heritage Railway Stations Protection Act*?		4
d. designated under the *Heritage Lighthouse Protection Act*?		4
e. identified as a Federal Heritage Building by the Federal Heritage Buildings Review Office (FHBRO)?		4
f. located within a United Nations Educational, Scientific and Cultural Organization (UNESCO) World Heritage Site?		4

If Yes to any of the above questions, you need to hire a qualified person(s) to undertake:

- a Cultural Heritage Evaluation Report, if a Statement of Cultural Heritage Value has not previously been prepared or the statement needs to be updated

If a Statement of Cultural Heritage Value has been prepared previously and if alterations or development are proposed, you need to hire a qualified person(s) to undertake:

- a Heritage Impact Assessment (HIA) – the report will assess and avoid, eliminate or mitigate impacts

If No, continue to Question 4.

Part B: Screening for Potential Cultural Heritage Value

	Yes	No
4. Does the property (or project area) contain a parcel of land that:		
a. is the subject of a municipal, provincial or federal commemorative or interpretive plaque?		4
b. has or is adjacent to a known burial site and/or cemetery?		4
c. is in a Canadian Heritage River watershed?		4
d. contains buildings or structures that are 40 or more years old?		4

Part C: Other Considerations

	Yes	No
5. Is there local or Aboriginal knowledge or accessible documentation suggesting that the property (or project area):		
a. is considered a landmark in the local community or contains any structures or sites that are important in defining the character of the area?		4
b. has a special association with a community, person or historical event?		4
c. contains or is part of a cultural heritage landscape?		4

If Yes to one or more of the above questions (Part B and C), there is potential for cultural heritage resources on the property or within the project area.

You need to hire a qualified person(s) to undertake:

- a Cultural Heritage Evaluation Report (CHER)

If the property is determined to be of cultural heritage value and alterations or development is proposed, you need to hire a qualified person(s) to undertake:

- a Heritage Impact Assessment (HIA) – the report will assess and avoid, eliminate or mitigate impacts

If No to all of the above questions, there is low potential for built heritage or cultural heritage landscape on the property.

The proponent, property owner and/or approval authority will:

- summarize the conclusion
- add this checklist with the appropriate documentation to the project file

The summary and appropriate documentation may be:

- submitted as part of a report requirement e.g. under the *Environmental Assessment Act, Planning Act* processes
- maintained by the property owner, proponent or approval authority

Instructions

Please have the following available, when requesting information related to the screening questions below:

- a clear map showing the location and boundary of the property or project area
  - large scale and small scale showing nearby township names for context purposes
- the municipal addresses of all properties within the project area
- the lot(s), concession(s), and parcel number(s) of all properties within a project area

For more information, see the Ministry of Tourism, Culture and Sport's Ontario Heritage Toolkit or Standards and Guidelines for Conservation of Provincial Heritage Properties.

In this context, the following definitions apply:

- **qualified person(s)** means individuals – professional engineers, architects, archaeologists, etc. – having relevant, recent experience in the conservation of cultural heritage resources.
- **proponent** means a person, agency, group or organization that carries out or proposes to carry out an undertaking or is the owner or person having charge, management or control of an undertaking.

1. Is there a pre-approved screening checklist, methodology or process in place?

An existing checklist, methodology or process may already be in place for identifying potential cultural heritage resources, including:

- one endorsed by a municipality
- an environmental assessment process e.g. screening checklist for municipal bridges
- one that is approved by the Ministry of Tourism, Culture and Sport (MTCS) under the Ontario government's Standards & Guidelines for Conservation of Provincial Heritage Properties [s.B.2.]

Part A: Screening for known (or recognized) Cultural Heritage Value

2. Has the property (or project area) been evaluated before and found not to be of cultural heritage value?

Respond 'yes' to this question, if all of the following are true:

A property can be considered not to be of cultural heritage value if:

- a Cultural Heritage Evaluation Report (CHER) - or equivalent - has been prepared for the property with the advice of a qualified person and it has been determined not to be of cultural heritage value and/or
- the municipal heritage committee has evaluated the property for its cultural heritage value or interest and determined that the property is not of cultural heritage value or interest

A property may need to be re-evaluated, if:

- there is evidence that its heritage attributes may have changed
- new information is available
- the existing Statement of Cultural Heritage Value does not provide the information necessary to manage the property
- the evaluation took place after 2005 and did not use the criteria in Regulations 9/06 and 10/06

Note: Ontario government ministries and public bodies [prescribed under Regulation 157/10] may continue to use their existing evaluation processes, until the evaluation process required under section B.2 of the Standards & Guidelines for Conservation of Provincial Heritage Properties has been developed and approved by MTCS.

To determine if your property or project area has been evaluated, contact:

- the approval authority
- the proponent
- the Ministry of Tourism, Culture and Sport

3a. Is the property (or project area) identified, designated or otherwise protected under the *Ontario Heritage Act* as being of cultural heritage value e.g.:

i. designated under the *Ontario Heritage Act*

- individual designation (Part IV)
- part of a heritage conservation district (Part V)

Individual Designation – Part IV

A property that is designated:

- by a municipal by-law as being of cultural heritage value or interest [s.29 of the *Ontario Heritage Act*]
- by order of the Minister of Tourism, Culture and Sport as being of cultural heritage value or interest of provincial significance [s.34.5]. **Note**: To date, no properties have been designated by the Minister.

Heritage Conservation District – Part V

A property or project area that is located within an area designated by a municipal by-law as a heritage conservation district [s. 41 of the *Ontario Heritage Act*].

For more information on Parts IV and V, contact:

- municipal clerk
- Ontario Heritage Trust
- local land registry office (for a title search)

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ii. subject of an agreement, covenant or easement entered into under Parts II or IV of the *Ontario Heritage Act*

An agreement, covenant or easement is usually between the owner of a property and a conservation body or level of government. It is usually registered on title.

The primary purpose of the agreement is to:

- preserve, conserve, and maintain a cultural heritage resource
- prevent its destruction, demolition or loss

For more information, contact:

- Ontario Heritage Trust - for an agreement, covenant or easement [clause 10 (1) (c) of the *Ontario Heritage Act*]
- municipal clerk – for a property that is the subject of an easement or a covenant [s.37 of the *Ontario Heritage Act*]
- local land registry office (for a title search)

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iii. listed on a register of heritage properties maintained by the municipality

Municipal registers are the official lists - or record - of cultural heritage properties identified as being important to the community.

Registers include:

- all properties that are designated under the *Ontario Heritage Act* (Part IV or V)
- properties that have not been formally designated, but have been identified as having cultural heritage value or interest to the community

For more information, contact:

- municipal clerk
- municipal heritage planning staff
- municipal heritage committee

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iv. subject to a notice of:

- intention to designate (under Part IV of the *Ontario Heritage Act*)
- a Heritage Conservation District study area bylaw (under Part V of the *Ontario Heritage Act*)

A property that is subject to a **notice of intention to designate** as a property of cultural heritage value or interest and the notice is in accordance with:

- section 29 of the *Ontario Heritage Act*
- section 34.6 of the *Ontario Heritage Act.* **Note**: To date, the only applicable property is Meldrum Bay Inn, Manitoulin Island. [s.34.6]

An area designated by a municipal by-law made under section 40.1 of the *Ontario Heritage Act* as a **heritage conservation district study area**.

For more information, contact:

- municipal clerk – for a property that is the subject of notice of intention [s. 29 and s. 40.1]
- Ontario Heritage Trust

v. included in the Ministry of Tourism, Culture and Sport's list of provincial heritage properties

Provincial heritage properties are properties the Government of Ontario owns or controls that have cultural heritage value or interest.

The Ministry of Tourism, Culture and Sport (MTCS) maintains a list of all provincial heritage properties based on information provided by ministries and prescribed public bodies. As they are identified, MTCS adds properties to the list of provincial heritage properties.

For more information, contact the MTCS Registrar at registrar@ontario.ca.

3b. Is the property (or project area) a National Historic Site (or part of)?

National Historic Sites are properties or districts of national historic significance that are designated by the Federal Minister of the Environment, under the *Canada National Parks Act*, based on the advice of the Historic Sites and Monuments Board of Canada.

For more information, see the National Historic Sites website.

3c. Is the property (or project area) designated under the *Heritage Railway Stations Protection Act*?

The *Heritage Railway Stations Protection Act* protects heritage railway stations that are owned by a railway company under federal jurisdiction. Designated railway stations that pass from federal ownership may continue to have cultural heritage value.

For more information, see the Directory of Designated Heritage Railway Stations.

3d. Is the property (or project area) designated under the *Heritage Lighthouse Protection Act*?

The *Heritage Lighthouse Protection Act* helps preserve historically significant Canadian lighthouses. The Act sets up a public nomination process and includes heritage building conservation standards for lighthouses which are officially designated.

For more information, see the Heritage Lighthouses of Canada website.

3e. Is the property (or project area) identified as a Federal Heritage Building by the Federal Heritage Buildings Review Office?

The role of the Federal Heritage Buildings Review Office (FHBRO) is to help the federal government protect the heritage buildings it owns. The policy applies to all federal government departments that administer real property, but not to federal Crown Corporations.

For more information, contact the Federal Heritage Buildings Review Office.

See a directory of all federal heritage designations.

3f. Is the property (or project area) located within a United Nations Educational, Scientific and Cultural Organization (UNESCO) World Heritage Site?

A UNESCO World Heritage Site is a place listed by UNESCO as having outstanding universal value to humanity under the Convention Concerning the Protection of the World Cultural and Natural Heritage. In order to retain the status of a World Heritage Site, each site must maintain its character defining features.

Currently, the Rideau Canal is the only World Heritage Site in Ontario.

For more information, see Parks Canada – World Heritage Site website.

Part B: Screening for potential Cultural Heritage Value

4a. Does the property (or project area) contain a parcel of land that has a municipal, provincial or federal commemorative or interpretive plaque?

Heritage resources are often recognized with formal plaques or markers.

Plaques are prepared by:

- municipalities
- provincial ministries or agencies
- federal ministries or agencies
- local non-government or non-profit organizations

For more information, contact:

- municipal heritage committees or local heritage organizations – for information on the location of plaques in their community
- Ontario Historical Society's Heritage directory – for a list of historical societies and heritage organizations
- Ontario Heritage Trust – for a list of plaques commemorating Ontario's history
- Historic Sites and Monuments Board of Canada – for a list of plaques commemorating Canada's history

4b. Does the property (or project area) contain a parcel of land that has or is adjacent to a known burial site and/or cemetery?

For more information on known cemeteries and/or burial sites, see:

- Cemeteries Regulations, Ontario Ministry of Consumer Services – for a database of registered cemeteries
- Ontario Genealogical Society (OGS) – to locate records of Ontario cemeteries, both currently and no longer in existence; cairns, family plots and burial registers
- Canadian County Atlas Digital Project – to locate early cemeteries

In this context, adjacent means contiguous or as otherwise defined in a municipal official plan.

4c. Does the property (or project area) contain a parcel of land that is in a Canadian Heritage River watershed?

The Canadian Heritage River System is a national river conservation program that promotes, protects and enhances the best examples of Canada's river heritage.

Canadian Heritage Rivers must have, and maintain, outstanding natural, cultural and/or recreational values, and a high level of public support.

For more information, contact the Canadian Heritage River System.

If you have questions regarding the boundaries of a watershed, please contact:

- your conservation authority
- municipal staff

4d. Does the property (or project area) contain a parcel of land that contains buildings or structures that are 40 or more years old?

A 40 year 'rule of thumb' is typically used to indicate the potential of a site to be of cultural heritage value. The approximate age of buildings and/or structures may be estimated based on:

- history of the development of the area
- fire insurance maps
- architectural style
- building methods

Property owners may have information on the age of any buildings or structures on their property. The municipality, local land registry office or library may also have background information on the property.

Note: 40+ year old buildings or structure do not necessarily hold cultural heritage value or interest; their age simply indicates a higher potential.

A building or structure can include:

- residential structure
- farm building or outbuilding
- industrial, commercial, or institutional building
- remnant or ruin
- engineering work such as a bridge, canal, dams, etc.

For more information on researching the age of buildings or properties, see the Ontario Heritage Tool Kit Guide Heritage Property Evaluation.

Part C: Other Considerations

5a. Is there local or Aboriginal knowledge or accessible documentation suggesting that the property (or project area) is considered a landmark in the local community or contains any structures or sites that are important to defining the character of the area?

Local or Aboriginal knowledge may reveal that the project location is situated on a parcel of land that has potential landmarks or defining structures and sites, for instance:

- buildings or landscape features accessible to the public or readily noticeable and widely known
- complexes of buildings
- monuments
- ruins

5b. Is there local or Aboriginal knowledge or accessible documentation suggesting that the property (or project area) has a special association with a community, person or historical event?

Local or Aboriginal knowledge may reveal that the project location is situated on a parcel of land that has a special association with a community, person or event of historic interest, for instance:

- Aboriginal sacred site
- traditional-use area
- battlefield
- birthplace of an individual of importance to the community

5c. Is there local or Aboriginal knowledge or accessible documentation suggesting that the property (or project area) contains or is part of a cultural heritage landscape?

Landscapes (which may include a combination of archaeological resources, built heritage resources and landscape elements) may be of cultural heritage value or interest to a community.

For example, an Aboriginal trail, historic road or rail corridor may have been established as a key transportation or trade route and may have been important to the early settlement of an area. Parks, designed gardens or unique landforms such as waterfalls, rock faces, caverns, or mounds are areas that may have connections to a particular event, group or belief.

For more information on Questions 5.a., 5.b. and 5.c., contact:

- Elders in Aboriginal Communities or community researchers who may have information on potential cultural heritage resources. Please note that Aboriginal traditional knowledge may be considered sensitive.
- municipal heritage committees or local heritage organizations
- Ontario Historical Society's "Heritage Directory" - for a list of historical societies and heritage organizations in the province

An internet search may find helpful resources, including:

- historical maps
- historical walking tours
- municipal heritage management plans
- cultural heritage landscape studies
- municipal cultural plans

Information specific to trails may be obtained through Ontario Trails.