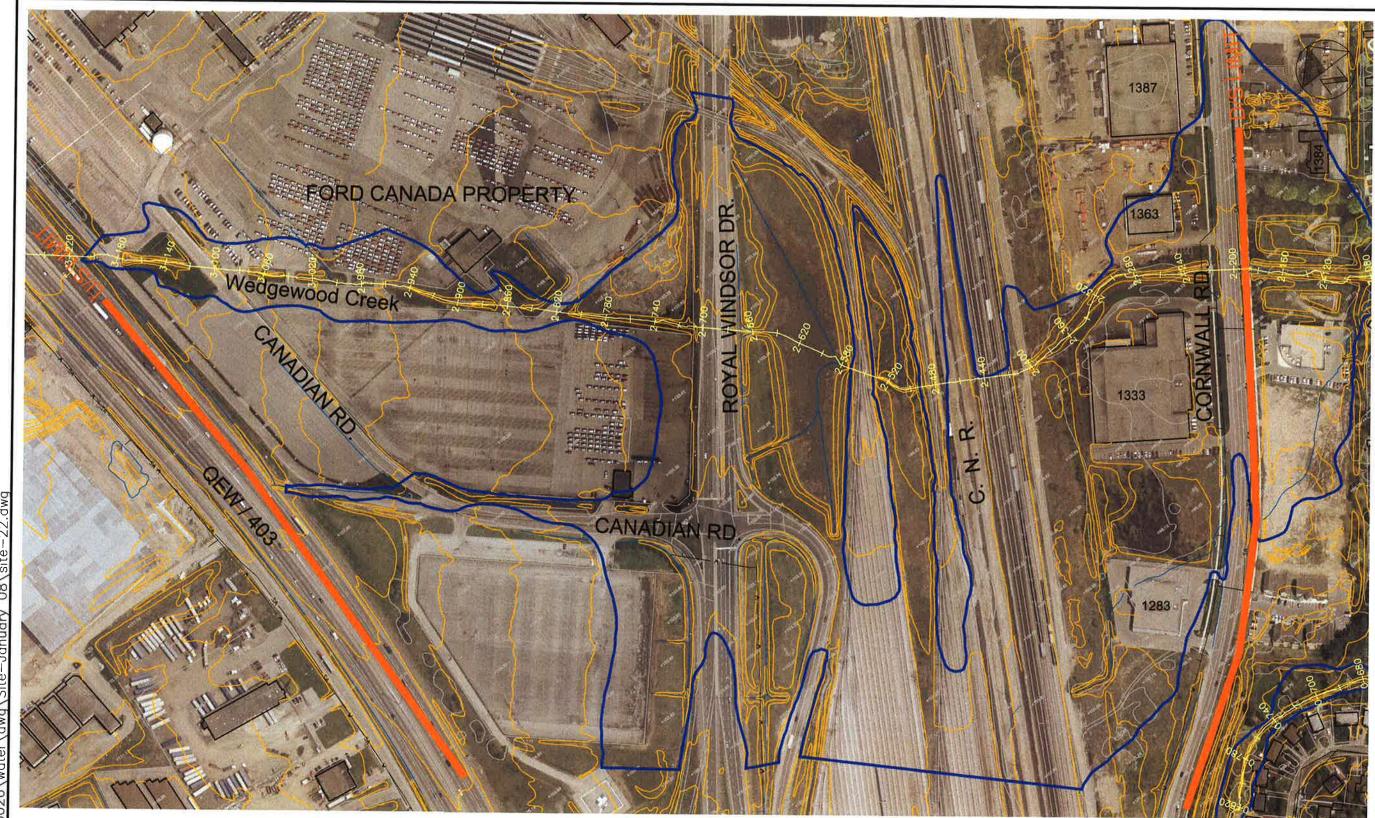
# Appendix B Information Tracking Sheet, Field Reconnaissance, and Terrestrial and Aquatic Background Review





LEGEND:

REGULATORY FLOODLINE

TOWNWIDE FLOODING STUDY TOWN OF OAKVILLE SITE # 22 - WEDG2190M WEDGEWOOD CREEK

	I
WILLOS	
ENGINEERING	Ī

Project No.	106026
Date	January 2008
Scale	1:3,000
Figure No.	22

### Site #22 (WEDG2190M) Implementation Program

### Recommended Management Approach/Project Scope:

 Further assessment of CNR and Royal Windsor Crossings. Assessment would require updated topographic survey of crossings to update the existing HEC-2 modeling. Assessment would determine potential culvert upgrades and possible road profile improvements. Detail design would follow the assessment completion.

### Appropriate Lead for Undertaking:

• Timing and phasing as per Town of Oakville Capital Works Program based on priority ranking established herein.

### Governing Protocol Legislation:

- Town of Oakville's Policies and protocols
- Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
- Ministry of Natural Resources Lakes and Rivers Act
- Department of Fisheries and Oceans Fisheries Act
- Ministry of Environment Water Taking (required for damming and pumping operations)

### Approval Requirements:

- Town of Oakville
- Conservation Halton Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Permit
- Regional Municipality for water and wastewater servicing alterations at Morrison Road (Site 23)
- Ministry of Environment Permit to Take Water (should dam and pumping for creek diversion or dewatering be required)
- Potentially Department of Fisheries and Oceans (i.e. should a Harmful Alteration Disruption or Destruction (HADD) be identified to occur based on the proposed works)
- Input from Utility companies for utility locations

### Need for, and Scope of Follow-Up Assessment/Analysis:

- Detailed topographic survey of area
- Vegetation assessment
- Hydraulic modeling refinement
- Approval process with CNR

### Suggested Timing, Need for Phasing:

 Timing of project dependant on Capital Works Program budget and priority of project within the Program.

### Possible Implementation Issues:

CNR consent to proposed culvert upgrades

### Possible Monitoring Requirements:

Potentially Department of Fisheries and Oceans monitoring requirements

### Need for Maintenance:

- Potential vegetation replacement and seeding
- Potential creek stabilization resulting from local grading impacts
- Crossing maintenance

### Potential Interface with Other Town/Agency Programs:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Potential opportunities with Town's Creek Erosion Study and road work
- Potential projects already identified by Conservation Halton

### Other Funding Opportunities:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Canada/ Ontario Municipal Renewal Infrastructure Fund
- Others

# Site #22 (WEDG2190M) Specific Flood Management Alternative Assessment

# Data/Information:

# Flooding mechanisms:

- Various CNR culverts creating high tail water conditions downstream of Royal Windsor Drive.
- Royal Windsor Culvert size and channel inverts creating flooding conditions on roadway.
  Flooding conditions allow both private and emergency vehicle access as flow depths are
  always below 0.3m with low flow velocities. The roadway floods for all storms, 2 year
  through to the Regional Storm. Minimum flooding depth is 0.10 m. The crossing does not
  meet the road classification flood requirements, but does prevent vehicle ingress/egress.

### Screened Alternatives:

- Crossing upgrades of CNR and Royal Windsor, or just Royal Windsor
- Road profile improvement
- Floodplain/channel upgrades
- Regulate TBD

# Preferred Management Approach:

• The preferred approach would require further assessment of the CNR and Royal Windsor crossings, as the original HEC-2 floodplain model appears to have coding issues and elevations used in the modeling require checking. There is approximately just under a 2 m drop through the Royal Windsor crossing. Therefore, further hydraulic assessment and topographic survey data would be required.

# Potential Linkage to Adjacent Sites:

Linkage to Site 26

					able 7		-			
				Summary of Site	Evaluation Resul	ts				
			Cater	gory Evaluation Pr	oducts					
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products
22	20.0	0.0	0.0	0.0	0.0	0.0	9.0	16.0	8.0	53.0

											F	Road I	Floodi		able 4 ood Cr		Evalu	ation																		
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation		T)	Floo	d Eleva	tions (r	n)			Ro	pad Flo	oding E	Depth (i	m)			FI	ow Vel	ocities	(m/s)			Sto	orm Ev	ent Fred	quency	Modif	iers		Storm Event Flooding Starts/ or Criteria Not Met	Storm Event Frequency Modifier Selected	Evaluation Scale Category Importance/ Significance	Product (Measure Weighting * Storm
		(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5	10	25	50	100 F	Reg	2	5	10 2	5 5	0 1	00 R	Reg	(2-100, Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significance
22	Design Flood Criteria	Arterial	10	102,40	102.6	102,6	3 102	,6 102	7 102.	7 102.7	102.6	0.2	0.2	0.2	0.3	0,3	0.3	0.2	0.5	0.5	0.6	0.7	0.7	0.7	0.6	1 (		2 0.0			02 0	.01	2-yr - Arterial	1.0	2	20
22	Private Vehicle	EMS Route	10	102_40	1						1		1			- 1		0.2	- 1				191	- 1	-	- 1		2 0.0					25-уг	0.0	5	0.0
22	Emergency Vehicle	EMS Route	10	102.40	102.6	102.6	102	6 102	7 102.7	102.7	102.6	0.2	0,2	0.2	0.3	0.3	0.3	0.2	0.5	0.5	0.6	0.7	0.7	0.7	0.6	1 0	.4 0	.2 0.0	0.0	04 0.	02 0.	.01	None	0.0	6	0
22	Private Vehicle Acess to Facilities	Yes	10	1														0.2	- 1	- 1	- 1	- 1					9	2 0.0	- 1				2-yr - Arterial	0.0	3	0
22	Emergency Vehicle Access to Facilities	Yes	10	102,40	102.6	102.6	102	6 102	7 102.7	102.7	102,6	0.2	0.2	0,2	03	0,3	0.3	0.2	0.5	0.5	0.6	0.7	0.7	0.7	0.6	1 0	4 0	2 0.0	0.0	0.4	02 0.	.01	25-vr	0.0	7	0
22	Private Vehicle Driveway Access (Multiuser)	Med-High Usage	8	102.40		10.0												0.2			0.6	- 1	- 1	0.7				2 0.0	- 1 ^			`	2-yr	0.0	4	0

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

																		Threat to	Tal Life Floor	ble 5 d Criteria E	valuation																						
			Site Downs	treem Flood I	Elevations (m)	)				Reside	ential Units Fic	ooded (#)				Industria	Area (ha)			Comme	rolel Area (h	a)		In	stitutional (	(Isa)	L	nd Use De	nsities (per /unit)	re/ha or		People E	ndangere	d	4	torm Eve	nt Frequenc	y Modifiers				Composite	T
Site No	<b>32</b> €	5	10	25	50	100	Rog	2	5	10	25	50	100	Reg	2	5 10	25 50	100 F	leg 2	5 10	25 50	100 R	leg 2	5 10	25	50 10	0 Reg f	es Ind	Com	Instit	2 5	10 2		100 R	eg 2	5 10	) 25	50 100	Norr No. o Usin Mul	f People g Storm	Evaluation Scale Measure Weighting (1- 10)	Category Importance Significance (1- (0 - Day Usag (10 - Day and N Usage)	10) Pi
22	105.12	105:14	105.17	105.25	105.29	105:34	105 16	0	0	0	0	0	o	0	0.0	01 00	0.0 0.0	0,0	0 0	0. 0	0 0	0 (	0 0	0 0	0	0 0	0	125	90	40	0.0 0.3	0.0 0	0.0 0.0	0.0 0	0 50	20 10	) 4	2 1	0.4	5	- 1	9	-

- Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)

  Determine flooding conditions that results in life endagerment (separate spreadsheet direct damages). Note that for residential units, life endagerment has been included if the basement has been predicted to flood.

  Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)

  Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered

  Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm

  Apply adjustment factor (Value of Step 5 divided by 10)

- 7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

	Finished		Downstream	Upstream 2		Dint	Interpolated						1	
	Floor	Lowest	2-100/ Reg	100/ Reg	0 41	Distance	Property 2-	Buildina	Damage	First Floor	Floor	Damage	1 1	
Building No.	Elevation	Opening	Flood	Flood	Section	from	100/ Reg	Flood Depth	Costs	Flooding	Area	Costs		Frequency
	(m)	(m)	Elevations	Elevations	Distance	Downstream	Flood	(m)	(\$)/m <sup>2</sup>	(Yes/ No)	(m²)	(\$)		requericy
	(111)		(m)	(m)		Section	Elevations	2.7	(Ψ/////	(100,110)	(1117)	(Ψ)		
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Ford Canada Out	105.6	105.6	105.29	105.72	30			-100.00	1.00.0	0	0	0		5
Ford Canada Out	105.6	105.6	105.25	105.68	30				1.01.0	o o	0	0		2
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Ford Canada Plan	109	109.0	106.2	107,12	55	24	106.60	-100.00		ō	0	0		
Ford Canada Plan	109	109.0	106.16	107.1	55	24	106.57	-100.00	\$0.00	0	0	0		
Ford Canada Plan	109	109.0	106.12	107.08	55	24	106.54	-100.00	\$0.00	0	0	o		
Ford Canada Plan	109	109.0	106.07	107.05	55	24	106.50	-100.00	\$0.00	o	o	0		
Ford Canada Plan	109	109.0	106.03	107.02	55	24	106.46	-100.00	\$0.00	0	0	Ö		
Ford Canada Plan	109	109.0	105.98	106.99	55	24	106.42	-100.00	\$0.00	0	0	0		
1283 Cornwall Rd	99.28	99.3	98.34	98,34	20	10	98.34	-100.00	\$0.00	0	0	Ö		
1283 Cornwall Rd	99.28	99.3	98.66	98.66	20	10	98.66	-100.00	\$0.00	0	0	0		
1283 Cornwall Rd	99.28	99.3	98.57	98.57	20	10	98.57	-100.00	\$0.00	0	0	0		
1283 Cornwall Rd	99.28	99.3	98.47	98.47	20	10	98.47	-100.00	\$0.00	0	0	0		
1283 Cornwall Rd	99.28	99.3	98.34	98.34	20	10	98.34	-100.00	\$0.00	0	0	0		
1283 Cornwall Rd	99.28	99.3	98.2	98.2	20	10	98.20	-100.00	\$0.00	0	0	0		
1283 Cornwall Rd	99,28	99.3	98.12	98.12	20	10	98.12	-100.00	\$0.00	0	0	0		
1333 Cornwall Rd	98.82 98.82	98.8	98.34	98.34	20	10	98.34		\$0.00	0	0	0		
1333 Cornwall Rd	98.82	98.8	98.66	98.66	20	10	98.66	-100.00	\$0.00	0	0	0		
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1333 Cornwall Rd	98.82	98.8	98.34	98.34	20	10	98.34	-100.00	\$0.00	0	0	0		
1333 Cornwall Rd	98.82	98.8	98.2	98.2 98.12	20	10	98.20	-100.00	\$0.00	0	0	.0		
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363Cornwall Rd	98.6	98.6	98.66	98.66	20	10	98.34	-100.00	\$0.00	O	0	0		
363Cornwall Rd	98.6	98.6	98.57	98.57	20	10	98.66 98.57	0.06	\$3.18	1	900	2865		
363Cornwall Rd	98.6	98.6	98.47	98.47	20	10	98.47	-100.00	\$0.00	0	0	0		
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363Cornwall Rd	98.6	98.6	98.2	98.2	20	10	98.20	-100.00	\$0.00 \$0.00	0	0	0		
363Cornwall Rd	98.6	98.6	98.12	98.12	20	10	98.12	-100.00	\$0.00	0	0	0		
387 Cornwall Rd	98.89	98.9	98.34	98.34	20	10	98.34	-100.00	\$0.00	0	0	0		
387 Cornwall Rd	98.89	98.9	98.66	98.66	20	10	98.66	-100.00	\$0.00	0	0	0		
387 Cornwall Rd	98.89	98.9	98.57	98.57	20	10	98.57	-100.00	\$0.00	0	0	0		
387 Cornwall Rd	98.89	98.9	98.47	98.47	20	10	98.47	-100.00	\$0.00	o	0	0		
387 Cornwall Rd	98.89	98.9	98.34	98.34	20	10	98.34	-100.00	\$0.00	0		0		
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													-3	

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangerment

(\$)

\$0.00 \$0.00

										Table 6								
						-		Flooding D	amages Evalua	tion Scale Catego	ry: Site Assessr	nent						
Site	Event	WSEL	Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth ( 50 Year, 5%) Direct Damages	Measure Weight	Category Importance/ Significance	Prodi
	(Yr)	(m)	(No.)	(No.)	(No.)	(\$)	(ha)	(\$)	(ha)	(S)	(ha)	(S)	(S)	(\$)	(S)	(1-10)	(1-10)	

10

93.00

93.51

93.74

93.64

50 93.69

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not

SO

- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
- 4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
- 5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

0.09

52,865

			Marking and a second		V								
			Downstra										_
n. auli -	Finished	Lowest	am 2-				Interpolated Property				Floor		
Building	Floor	Opening		Upstream 2-100/ Reg	Section Distance	Distance from	2-100/ Reg	Building Flood Depth	Damage Cosls	First Floor Flooding			
No	Elevation	(m)	Flood	Flood Elevations (m)	Dootton Diotanoc	Downstream Section	Flood Elevations	(m)	(\$)/m <sup>2</sup>	(Yes/No)	Area	Damage Costs	(\$
- 0	(m)	` ′	Elevations			SHOOT WEST PRINTS OF THE STATE	(m)				(m <sup>2</sup> )	1	
ord Cana	105.6	205.5	(m)										
ord Cana	105.6	105.6 105.6	105.16		30		105.41	-100.00	50 00	0			
ord Cana	105.6	105.6	105.34		30		105.56		\$0.00	0			
ord Cana	105.6	105.6	105.29 105.25		30	16			\$0.00	0		of a	
ord Cana	105.6	105.6	105.25		30		105.48		\$0.00	0			
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rd Cana	105.6	105.6	105 14		30			-100 00	\$0.00	9	0		
rd Cana	109	109.0	106.06		30 58		105.33	-100.00	\$0.00	.0	0		
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rd Cana	109	109.0	106.10		55			-100 00	\$0.00	0		1	- 3
rd Cana	109	109.0	106.12		55		106.57	-100.00	\$0.00	0		1	- 1
rd Cana	109	109.0	106.07		56		106.54	-100.00	\$0.00	0		1	
rd Cana	109	109.0	106.03		55		106.50	-100 00	\$0.00	0	0		
rd Cana	109	109.0	105.98		58		106.46 106.42	-100.00 -100.00	\$0.00	0	0	1	
83 Corn	99.28	99.3	98.34		20		98.34	-100.00	\$0.00				
33 Corn	99.28	99.3	98 66		20				\$0.00	0	0		
83 Com	99 28	99,3	98.57		20		98.57	-100.00 -100.00	\$0.00	0	0		3
83 Com	99.28	99,3	98.47		20		96.47	-100,00	\$0.00 \$0.00	0	0	1	
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33 Corn	99.28	99.3	98.2		20		98.20	-100.00	\$0.00 \$0.00	0			- /
33 Com	99 28	99.3	98.12		20			-100,00	\$0.00	0	.0	1	
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33 Corre	98.82	98.8	98.57	98.57	20		98.57	100.00	\$0.00	0	0	]	
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3Com	98.6	98.6	98 34	98.34	20	10	98.34	-100.00	\$0.00	0	0		-
63Corriv	98.6	98.6	98 66		20	10	98 66	0.06	\$3.18	i	900		2865
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37 Corr	98.89	98.9	98.34	98.34	20	10	95.34	-100.00	\$0.00	0	0		- 3
7 Coriu	98.89	98.9	98.66 98.57	98.66	20	10	98.66	-100 00	\$0.00	0	.0		(
7 Com	98.89	98.9		98.57	20	10	98.57	-100.00	\$0.00	0	0		
7 Com	98.89	98.9	98.47 98.34	98.47	20	10	98.47	-100.00	S0.00	0	0		- 1
37 Com	98 89	98 9	98.2	98.34 98.2	20	10	98,34	-100.00	\$0.00	0	0		- 3
7 Com	98.89	98.9	98 12	98.12	20	10	98.20	-100,00	\$0.00	0	0		
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											900	\$2,865	
											900	\$2,	865

Frequency		Summarized Damage Costs (\$)
	Reg	\$0,00
	100	\$2,864,81
	50	\$0.00
	25	\$0.00
	10	SO 00
	5	\$0.00
	2	\$0.00

Average Annual

Damages 2007 Indirect Damages \$523

( 50 Year, 5%)

Indirect

Damages

(\$)

\$78

Category

mportance/

Significance

(1-10)

Measure

Weight

(1-10)

SO

50

S2,865 S0 Total

Indirect Damage

Value

(S)

\$0

SO

50

\$0 \$0

\$430

S0

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine flooding damages for each return period based on the flooding depths and damage curve equations

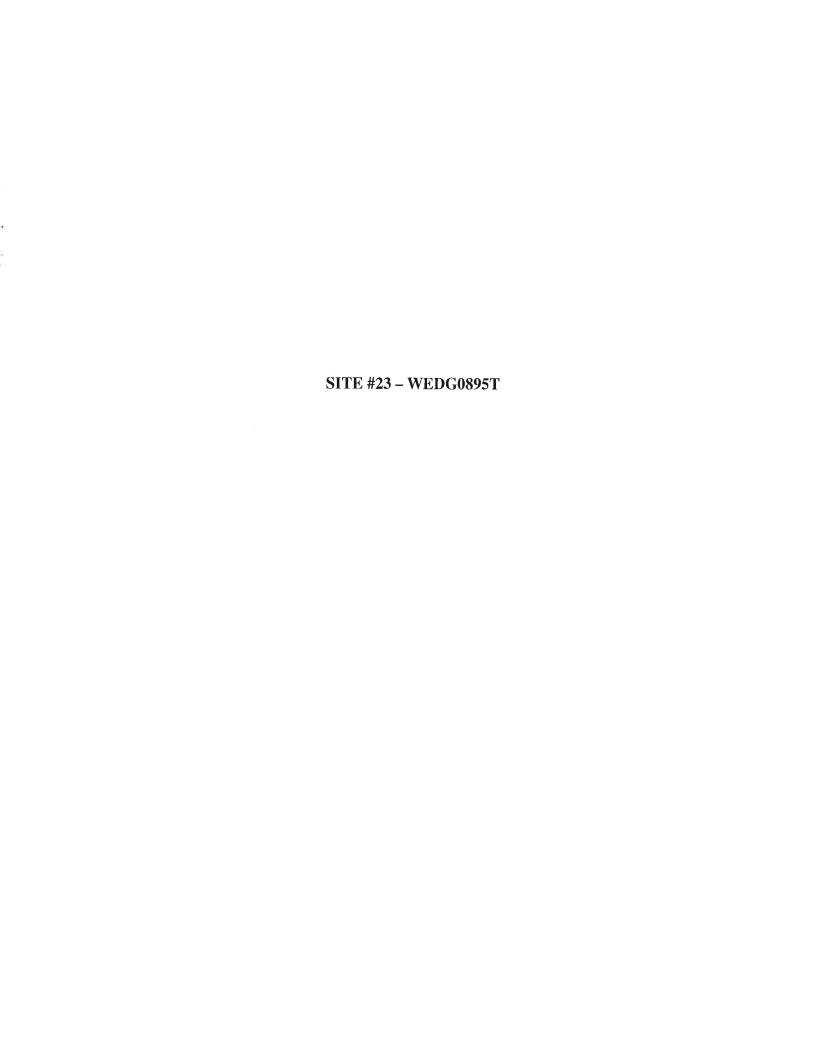




Figure No.

Feb 11/08 - avogt

23

# Site #23 (WEDG0895T) Implementation Program

# Recommended Management Approach/Project Scope:

Morrison Road culvert upgrade from 1.88 m by 1.26 m CSP arch culvert to 6 m by 1.2 m box culvert

### Appropriate Lead for Undertaking:

• Timing and phasing as per Town of Oakville Capital Works Program based on priority ranking established herein.

### Governing Protocol Legislation:

- Town of Oakville's Policies and protocols
- Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
- Ministry of Natural Resources Lakes and Rivers Act
- Department of Fisheries and Oceans Fisheries Act
- Ministry of Environment Water Taking (required for damming and pumping operations)

### Approval Requirements:

- Town of Oakville
- Conservation Halton Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Permit
- Regional Municipality for water and wastewater servicing alterations
- Ministry of Environment Permit to Take Water (should dam and pumping for creek diversion or dewatering be required)
- Potentially Department of Fisheries and Oceans (i.e. should a Harmful Alteration Disruption or Destruction (HADD) be identified to occur based on the proposed works)
- Input from Utility companies for utility locations

# Need for, and Scope of Follow-Up Assessment/Analysis:

- Detailed topographic survey of culvert and upstream and downstream creek
- Vegetation assessment
- Natural channel design assessment
- Hydraulic modeling refinement
- Approval process with private land owners

### Suggested Timing, Need for Phasing:

- Timing of project dependant on Capital Works Program budget and priority of project within the Program.
- Project should be conducted in conjunction with Site 23 works if possible

### Possible Implementation Issues:

- Private land owners consent to proposed grading (watercourse not owned by Town of Oakville)
- Town of Oakville potential easement requirements
- Vegetation loss, requiring mitigation
- Wetland area upstream of Morrison Road

### Possible Monitoring Requirements:

Potentially Department of Fisheries and Oceans monitoring requirements

### Need for Maintenance:

- Potential vegetation replacement and seeding
- Potential creek stabilization resulting from local grading impacts
- Crossing maintenance

# Potential Interface with Other Town/Agency Programs:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Potential opportunities with Town's Creek Erosion Study and road work
- Potential projects already identified by Conservation Halton

### Other Funding Opportunities:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Canada/ Ontario Municipal Renewal Infrastructure Fund (Morrison Road culvert works for Site 23)
- Others

# Site #23 (WEDG0895T) Specific Flood Management Alternative Assessment

# Data/Information:

# Flooding mechanisms:

- Morrison Road 1.88 m by 1.26 m CSP arch culvert crossing
- Floodplain capacity of approximately the 2 year storm 3.0 m³/s in vicinity of 1197 Cynthia La.
- Encroachment

### Screened Alternatives:

- Morrison Road culvert upgrade using 6m by 1.2 m box culvert
- Floodplain/ channel improvements not practical due to marsh area and limited hydraulic improvements
- Roadway profile could not be improved much based on existing grades
- Flood proofing homes that are not flooded on all sides. There are homes flooded on all sides; therefore flood proofing would not protect all homes.
- Acquisition of 3 homes would be expensive
- Regulate

# Preferred Management Approach:

Upgrade Morrison Road culvert

# Potential Linkage to Adjacent Sites:

• Linkage to Site 24, spill across Morrison Road eliminated with upgraded culvert. 1219 Baldwin Dr. would be removed from the Regional floodplain.

					able 7 Evaluation Resul	ts				
			Cate	gory Evaluation Pr						
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products
23	8.0	0.0	0.0	0.0	0.0	0.0	50.0	48.0	24.0	130.0

											R	oad F	loodin		able 4 od Cri	teria E	/aluati	on																	
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation		T	Flood I	Elevatio	ons (m)				Roa	d Floor	ding De	oth (m)				Flow V	/elociti	ies (m/s	;)		s	torm E	vent F	requer	тсу Мо	difier	s	Storm Event Flooding Starts/ or Criteria Not Met		Evaluation Scale Category Importance/ Significance	Product (Measure Weighting *
		(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5	10	25	50 10	) Reg	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	(2-100, Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significance
23	Design Flood Criteria	Arterial	10	98,74	98,9	99.0	99.0	99.1	99.1	99.1	99.1	0.1	0.2	0,3	0,3	0.4	0.4	0,0	0.5	0.6	0.6	0.7	0.7	0.7	1	0.4	0.2	0.08	0.04	0.02	0_01	5-yr / 1:100 - Reg	0.4	2	8
23	Private Vehicle	Level 3 Road/ 100-Regional	6	98.74	98,9	99.0	99.0	99.1	99,1	99,1	99.1	0.1	0.2	0.3	0,3	4 0.4	0.4	0.0	0.5	0.6	0.6	0.7	0.7	0.7	1	0.4	0.2	0.08	0.04	0.02	0.01	, .	0.0	5	0
23	Emergency Vehicle	Level 3 Road/ 100-Regional	6	98.74	98,9	99.0	99.0	99.1	99.1	99.1	99.1	0.1	0.2	0.3	0,3	4 0.4	0.4	0,0	0.5	0.6	0.6	0.7	0.7	0.7	1	0.4	0.2	0.08	0.04	0.02	0.01	None	0.0	6	0
23	Private Vehicle Acess to Facilities	Partial	5												- 1	4 0.4											0,2						0.0	3	0
23	Emergency Vehicle Access to Facilities	Partial	5	98.74	98.9	99.0	99.0	99.1	99.1	99_1	99.1	0.1	0.2	0.3	0.3	.4 0.4	0.4	0.0	0.5	0.6	0.6	0.7	0.7	0.7	1	0.4	0.2	0.08	0.04	0.02	0.01	None	0.0	7	0
23	Private Vehicle Driveway Access (Multiuser)	Medium Vehicle Usage	6		1										1	4 0.4				0.6	1			0.7	- 1	0.4			0.04				0.0	4	0

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

																		Th	reat to L	Tab Life Flood	ile 5 I Criteria I	Evaluation	1																					
ŀ		i	Site Downs	stream Flood I	Elevations (n	0)				Rosid	ontial Units FI	ooded (#)				Indu	strini Area	(ha)			Commerc	lal Area (hi	0		In	stitutiona	il (ha)			e Densities or /unit)	(pers/ ha		Peop	e Endange	bered		Storm	Event Fre	equency A	doditiers			Composi	ite
te No	2	5	10	25	50	100	Reg	2	: 60	10	25	50	100	Reg	2	5	10 25	50 1	00 Reg	2 5	10	25 50	100 Re	ng 2	5 1	0 25	50 1	00 Reg	Res I	nd Com	Instit	2	5 10	25 (	50 100	Reg	2 5	10:	25 50	100	Normal No. of Pi Using S leg Muttipl	ople Meas		ce/ (1-10) age)
	98,86	98.95	99	99.05	99.09	99.12	99.08	3	3	3	3	3	3	3	0	0	0 0	0	0 0	0 0	0	0 0	0 0	0 0	0 0	0 0	0	0 0	3 1	25 90	40	9 1	9 9	9	9 9	9	50 20	10	4 2	1	3.4 786	5	10	

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)
  2 Determine flooding conditions that results in life endagerment (separate spreadsheet direct damages). Note that for residential units, life endagerment has been included if the basement has been predicted to flood.
  3 Determine number of people endagered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)
  4 Determine number of people endagered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered
  5 Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm

- 6 Apply adjustment factor (Value of Step 5 divided by 10)
- 7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

Building No.	Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream 2-100/ Reg Flood Elevations (m)	Upstream 2 100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
528 Morrison	99.2	96,8	98.6	99.08	99.08	10	9	99.08	0.49	\$20,740.54	- 1	0
528 Morrison	99.2	96.8	98.6	99.12	99,12	10	9	99.12	0.53	\$21,363.37	1	0
528 Morrison	99.2	96_8	98.6	99.09	99.09	10	9	99.09	0.50	\$20,894.52		0
528 Morrison	99.2	96.8	98.6	99.05	99.05	10	9	99.05	0.46	\$20,285.35		0
528 Morrison	99.2	96.8	98.6	99	99	10	9	99.00	0.41	\$19,548.80	1	0
528 Morrison	99.2	96.8	98.6	98.95	98.95	1.0	9	98.95	0.36	\$18,839.00	1	0
528 Morrison	99.2	96.8	98.6	98.86	98.86	10	9	98.86	0.27	\$17,625.66	1	0
1197 Cynthia	99.15	96.7	98.5	99.08	99.09	40	29	99.09	0.55	\$21,637.71	1	0
1197 Cynthia	99.15	96.7	98.5	99 12	99.13	40	29	99.13	0.59	\$22,287.50	1	0
1197 Cynthia	99.15	96.7	98.5	99.09	99.09	40	29	99.09	0.55	\$21,681.77	1	0
1197 Cynthia	99.15	96.7	98.5	99.05	99.06	40	29	99.06	0.52	\$21,162.84	1	0
1197 Cynthia	99.15	96.7	98,5	99	99	40	29	99.00	0.46	\$20,285.35	1	o
1197 Cynthia	99.15	96.7	98.5	98.95	98.95	40	29	98.95	0.41	\$19,548.80	1	o
1197 Cynthia	99.15	96.7	98,5	98.86	98.87	40	29	98.87	0.33	\$18,388.10	1	0
203 Cynthia	99.15	96.7	98.5	99.09	99.09	50	9	99.09	0,55	\$21,681.77	1	0
203 Cynthia	99.15	96.7	98.5	99.13	99.13	50	9	99.13	0.59	\$22,332.88	1	o
203 Cynthia	99.15	96.7	98.5	99.09	99.09	50	9	99.09	0.55	\$21,681,77	1	0
203 Cynthia	99.15	96.7	98.5	99.06	99.06	50	9	99.06	0.52	\$21,205,93	1	0
203 Cynthia	99.15	96.7	98.5	99	99	50	9	99.00	0.46	\$20,285.35	1	o
203 Cynthia	99.15	96.7	98.5	98.95	98.95	50	9	98.95	0.41	\$19,548.80	1	o
203 Cynthia	99.15	96,7	98.5	98.87	98.87	50	9	98.87	0.33	\$18,425.54	1	اه

Frequency	Summarized Damage Costs (\$)
Reg	\$64,060.02
100	\$65,983.75
50	\$64,258.07
25	\$62,654.12
10	\$60,119.50
5	\$57,936.60
2	\$54,439.31

- 1 Determine flooding elevations for all storm events at buildings that potentially flood 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
  5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangermer

Table 6	
Flooding Damages Evaluation Scale Category: Site Assessment	ent

Site	Event	Chosti	Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth (50 Year, 5%) Direct Damages	Measure Weight	Category Importance/ Significance	100
	(Yr)	(m)	(No.)	(No.)	(No.)	(\$)	(ha)	(\$)	(ha)	(\$)	(ha)	(\$)	(S)	(\$)	(\$)	(1-10)	(1-10)	
	2	92.69	3	3	3	\$80,570	0	0	0	0	0	0	\$80,570					
	5	93.00	3	3	3	\$85,746	0	0	0	0	0	0	\$85,746				)	
	10	93,51	3	3	3	\$88,977	0	0	0	0	0	0	\$88,977					
23	25	93.64	- 3	3	3	\$92,728	0	0	0	0	0	0	\$92,728	\$42,986	\$784,749	6	8	48
	50	93.69	3	3	3	\$95,102	0	0	0	0	0	0	\$95,102	V	11 1000000			5-40
	100	93.74	3	3	3	\$97,656	0	0	0	0	0	0	\$97,656					
	Reg	93.61	3	3	3	\$94,809	0	0	0	0	0	0	\$94,809					
													Total Indirect Damage	Average Annual Damages 2007	Present Worth (50 Year, 5%)	Measure	Category Importance/	

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not
- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
- 4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
- 5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

Building No.	Finished Floor Elevation	Basement Floor Elevation	Lowest Opening (m)	Downstream Reg Elevations	2-100/ Flood (m)	Upstream 2-100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Pro 100/ Reg	Flood	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
F00 11	(m)	(m)		Elovations	, ,				Elevations	(m)	. , ,		(1001110)	(100/140)
528 Morris	98.67	96.2	98.1		99,08	99.08	10	9		99.08	1.02	\$30,695.96	- 1	
528 Morris	98 67	96.2	98,1		99.12	99.12	10	9		99.12	1.06	\$31,617.76	1	
28 Morris	98.67	96.2	98.1		99 09	99.09	10	9		99.09	1.03	\$30,923.86	1	
28 Morris	98.67	96.2	98.1		99,05	99.05	10	9		99.05	0.99	\$30,022.29	1	
28 Morris	98 67	96.2	98.1		99	99	10	9		99.00	0.94	\$28,932.20	1	
28 Morris	98.67	96.2	98.1		98,95	98.95	10	9		98.95	0.89	\$27,881.68	1	
528 Morris	98.67	96.2	98.1		98.86	98.86	10	9		98.86	0.80	\$26,085.95	1	
197 Cynti	98.62	96.2	98.0		99.08	99.09	40	29		99.09	1.08	\$32,023.78	1	
197 Cyntl	98.62	96.2	98.0		99.12	99.13	40	29		99.13	1.12	\$32,985.46	1	
197 Cynti	98.62	96.2	98.0		99.09	99,09	40	29		99.09	1.08	\$32,088.99	1	
197 Cynth	98.62	96.2	98.0		99.05	99.06	40	29		99.06	1.05	\$31,320.97	1	
197 Cyntr	98,62	96.2	98.0		99	99	40	29		99.00	0.99	\$30,022.29	1	
197 Cynth	98.62 98.62	96.2	98.0		98 95	98.95	40	29		98.95	0.94	\$28,932.20	1	
197 Cynti		96.2	98.0		98.86	98.87	40	29		98.87	0.86	\$27,214,36	1	
203 Cynth	98.62 98.62	96.2	98.0		99.09	99.09	50	9		99.09	1.06	\$32,088.99	1	
203 Cynth		96.2	98.0		99.13	99.13	50	9		99.13	1.12	\$33,052.63	1	
203 Cynti	98.62	96.2	98.0		99.09	99.09	50	9		99.09	1.08	\$32,088.99	1	
203 Cynll	98.62	96.2	98.0		99.06	99.06	50	9	l'i	99.06	1.05	\$31,384.75	1	
203 Cynll	98.62	96.2	98.0		99	99	50	9	1	99.00	0.99	\$30,022,29	1	
203 Cynll	98.62	96.2	98.0		98.95	98 95	50	9		98.95	0.94	\$28,932.20	1	
203 Cynll	98.62	96.2	98.0		98.87	98.87	50	9		98.87	0.86	\$27,269.78	1	

Frequency	Summarized Damage Costs (\$)
Reg	\$94,808.73
100	\$97,655.84
50	\$95,101.84
25	\$92,728.00
10	\$88,976,77
5	\$85,746.07
2	\$80,570.09

Indirect Damages

(\$)

\$6,448

Value

(\$)

\$12,086

\$12,862

\$13,347

\$13,909

\$14,265

\$14,648

\$14,221

Indirect

Damages

(\$)

\$117,712

Weight

(1-10)

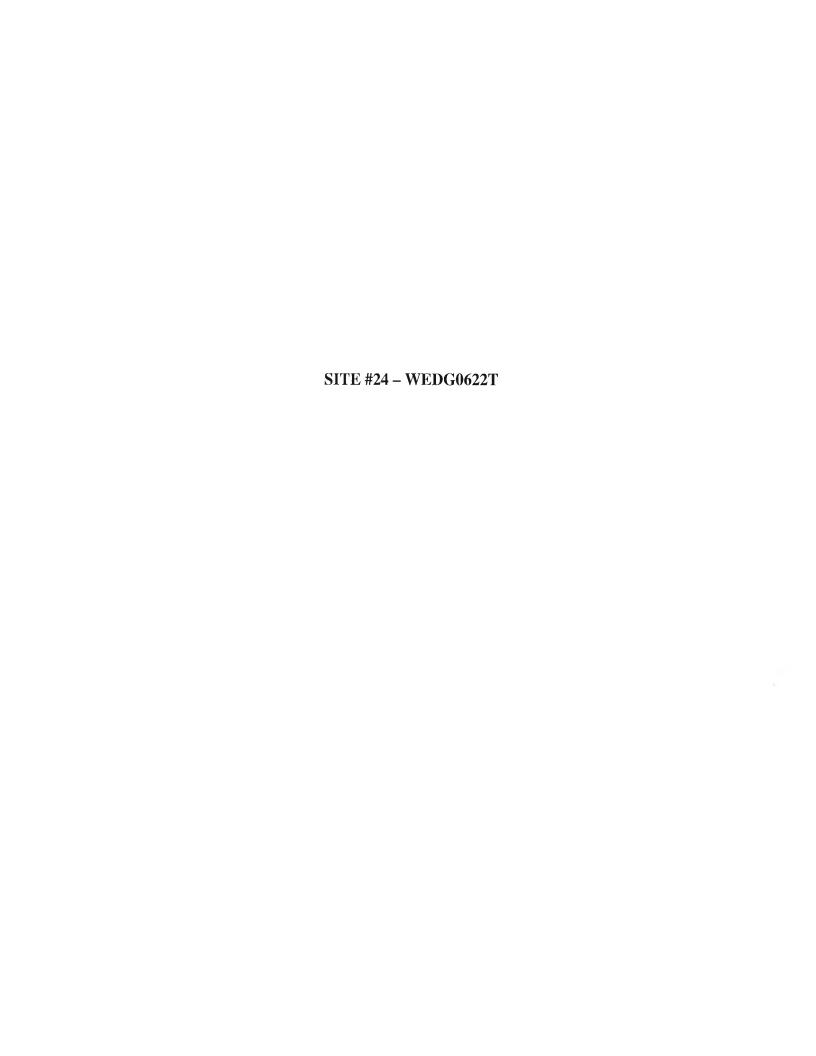
Product

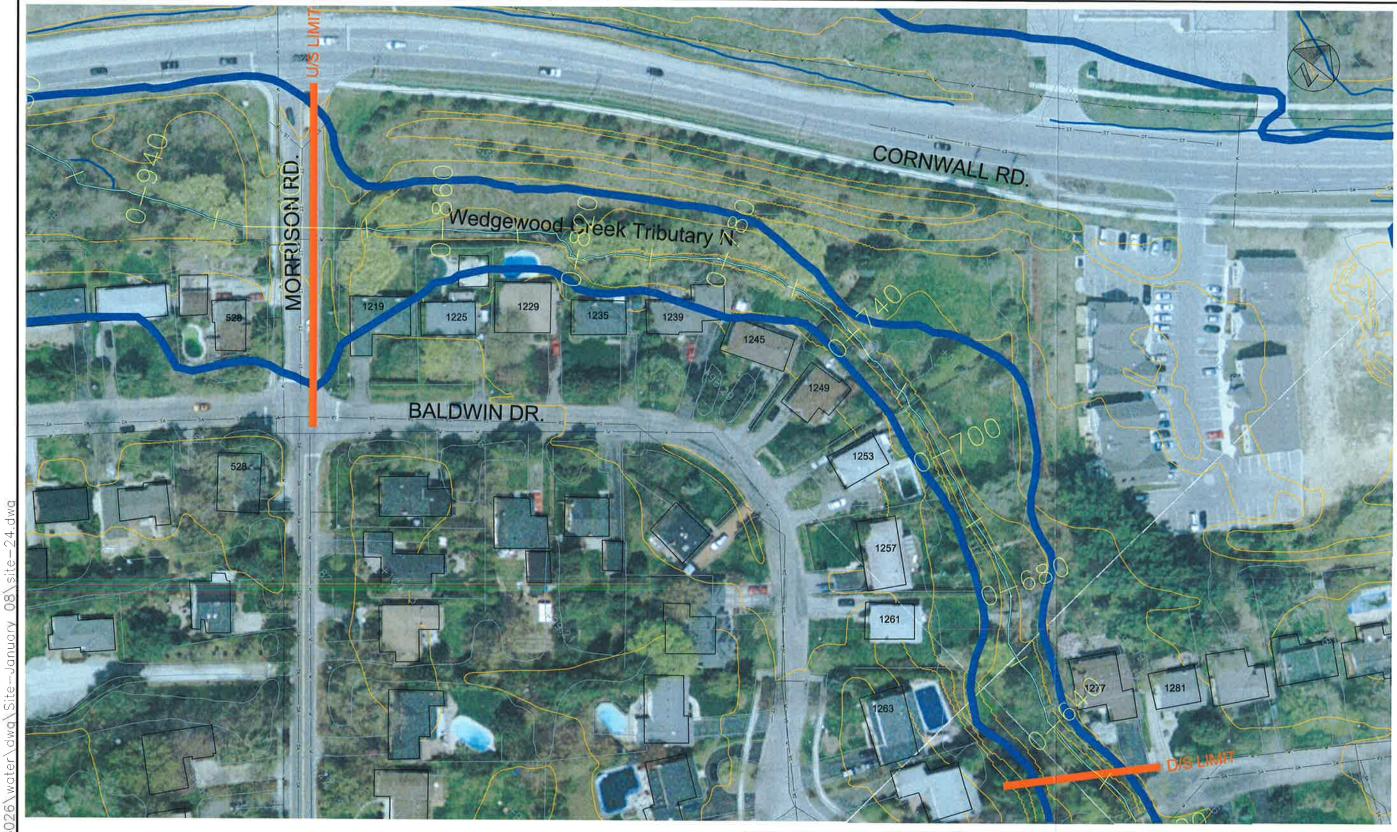
24

Significance

(1-10)

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine flooding damages for each return period based on the flooding depths and damage curve equations





LEGEND:

REGULATORY FLOODLINE

TOWNWIDE FLOODING STUDY TOWN OF OAKVILLE SITE # 24 - WEDG0622T WEDGEWOOD CREEK

	Р
HILLOS	S
ENGINEERING	F

	Project No.	106026	•
	Date	January 2008	
	Scale	1:1,000	•
3	Figure No.	24	•

# Site #24 (WEDG0622T) Implementation Program

### Recommended Management Approach/Project Scope:

- Floodplain grading improvements
- Morrison Road culvert upgrades (Site 23)

### Appropriate Lead for Undertaking:

• Timing and phasing as per Town of Oakville Capital Works Program based on priority ranking established herein.

### Governing Protocol Legislation:

- Town of Oakville's Policies and protocols
- Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
- Ministry of Natural Resources Lakes and Rivers Act
- Department of Fisheries and Oceans Fisheries Act
- Ministry of Environment Water Taking (required for damming and pumping operations)

### Approval Requirements:

- Land owners approval for grading
- Town of Oakville
- Conservation Halton Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Permit
- Regional Municipality for water and wastewater servicing alterations at Morrison Road (Site 23)
- Ministry of Environment Permit to Take Water (should dam and pumping for creek diversion or dewatering be required)
- Potentially Department of Fisheries and Oceans (i.e. should a Harmful Alteration Disruption or Destruction (HADD) be identified to occur based on the proposed works)
- Input from Utility companies for utility locations

### Need for, and Scope of Follow-Up Assessment/Analysis:

- Detailed topographic survey of area
- Vegetation assessment
- Natural channel design assessment
- Hydraulic modeling refinement
- Approval process with private land owners

### Suggested Timing, Need for Phasing:

- Timing of project dependant on Capital Works Program budget and priority of project within the Program.
- Project should be conducted in conjunction with Site 23 works if possible

### Possible Implementation Issues:

- Private land owners consent to proposed grading
- Town of Oakville potential easement requirements
- Vegetation loss, requiring mitigation
- Wetland area upstream of Morrison Road

### Possible Monitoring Requirements:

• Potentially Department of Fisheries and Oceans monitoring requirements

### Need for Maintenance:

- Potential vegetation replacement and seeding
- Potential creek stabilization resulting from local grading impacts
- Crossing maintenance

### Potential Interface with Other Town/Agency Programs:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Potential opportunities with Town's Creek Erosion Study and road work
- Potential projects already identified by Conservation Halton

### Other Funding Opportunities:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Canada/ Ontario Municipal Renewal Infrastructure Fund (Morrison Road culvert works for Site 23)
- Others

# Site #24 (WEDG0622T) Specific Flood Management Alternative Assessment

### Data/Information:

# Flooding mechanisms:

- Floodplain capacity is approximately 2 year at 5.2 m<sup>3</sup>/s in vicinity of 1239 Baldwin Dr.
- Spill from Morrison Road flooding (Site 23)
- Encroachment

### Screened Alternatives:

- Floodplain grading improvements are possible in vicinity of 1253 to 1239 Baldwin Dr.
- Morrison Road culvert upgrades (Site 23)
- Floodproofing of 1219 Baldwin Dr. This would not resolve the property flooding occurring on neighbouring lots.
- Regulate

# Preferred Management Approach:

- Floodplain grading improvements
- Morrison Road culvert upgrades (Site 23)

# Potential Linkage to Adjacent Sites:

• Linkage to Site 23

					ible 7 Evaluation Resul	ts				
	-		Cate	rgory Evaluation Pro	oducts			***		
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	16.0	8.0	24

											F	load F	loodir		able 4 od Cri	teria E	valuat	ion																	
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation		1	Flood	Elevati T	ons (m	)			Roa	d Floor	ding De	pth (m)				Flow \	/elociti	ies (m/s	)		S	torm E	vent Fr	equenc	y Mod	ifiers		Storm Event Flooding Starts/ or Criteria Not Met	Storm Event Frequency Modifier Selected	Evaluation Scale Category Importance/ Significance	Product (Measure Weighting * Storm
		(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5	10	25	50 10	0 Re	2 2	5	10	25	50	100	Reg	2	5	10	25	50 1	100	Reg	(2-100, Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significance
24	Design Flood Criteria	N ot Applicable	0	0.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0	0.0	0.0	0.0 0.	0.0	0.0	0.0	0.0						0.4	0.2	.08 (	04 0	102	0.01	NA	0.0	2	0
24	Private Vehicle	N ot Applicable	0	0.00	0.0	0.0								- 1	- 1	0.0		4						- 1	- 1	- 1	0.2			- 1	0	NA	0.0	5	0
24	Emergency Vehicle	N ot Applicable	0	0.00	0.0	0.0	0.0	0.0	0.0	0.0	0,0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1	0.4	0.2	.08 0	.04	102	0.01	NA	0.0	6	0
24	Private Vehicle Acess to Facilities	N ot Applicable	0	0.00				1			- 1			- 1		0.0								- 1			0.2			.		NA	0.0	3	0
24	Emergency Vehicle Access to Facilities	N ot Applicable	0	0.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1	0.4	0.2	.08	.04 0	.02	0.01	NA	0.0	7	0
24	Private Vehicle Driveway Access (Multiuser)	N ot Applicable	0	0.00	1		1		1 1							0.0 0.0	- 1						0.0				0.2				^	NA NA	0.0	4	0

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

																		Three	it to Life	Table 5 Flood Crit	oria Evalu	ation																					
+			Site Downs	ream Flood E	levations (m)					fleskie	ntial Units Flo	oded (#)				Indu	strial Area (h	n)		Con	nmercial Ar	oa (tin)			Institutione	ol (ba)		Land Use I	Jonsities (; /unit)	pers/ha or		People	Endange	red		Storm	Event Fre	equency M	lodifiers			Compos	ite
e No	2	5	10	25	Sa	100	Reg	2	6	10	25	50	100	Reg	323	5:	10 25	50 100	Reg 1	2 5 1	0 25	50 100	Reg 2	5	10 25	50 10	ió Reg	Res Inc	d Com	Instit	2 5	10	25 56	100	Reg 5	2 5	10 2	15 50	100 F	Normali No. of Pe Using St Multipli	ple Measu		ry ion/ (1-10) Pr ioge) 5 Night
	96.38	06.52	96.63	96.75	96.84	96.95	96.83	0	0	a	0	0	0	0	0	0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0	0 0	0 0	0	3 12	5 90	40	0 0	0	0 0	0	0 5	0 20	10	4 2	7 4	04 0	0	10	

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)
  2 Determine flooding conditions that results in life endangerment (separate spreadsheet direct damages). Note that for residential units, life endangerment has been included if the basement has been predicted to flood.
  3 Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)
  4 Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered
  5 Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm
  6 Apply adjustment factor (Value of Step 5 divided by 10)
  7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

Building No	Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream 2-100/ Reg Flood Elevations (m)	Upstream 2 100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
1245 Baldwin	98.1	95.7	97.5	96,83	97,25	40	31	97.16	-100.00	\$0.00	0	- (
1245 Baldwin	98.1	95. <b>7</b>	97.5	96.95	97,33	40	31	97.24			0	
1245 Baldwin	98.1	95.7	97.5	96,84	97,26	40	31	97.17	-100.00		o	1 8
1245 Baldwin	98.1	95.7	97.5	96.75	97.17	40	31	97.08	-100.00			
1245 Baldwin	98.1	95.7	97.5	96.63	97.05	40	31	96.96	-100.00	\$0.00	0	i
1245 Baldwin	98.1	95.7	97.5	96.52	96.95	40	31	96.85	-100.00			Ċ
1245 Baldwin	98.1	95.7	97.5	96.38		40	31	96.72	-100.00	\$0.00	0	
1239 Baldwin	98.15	95.7	97.5	96,83		40	38	97.23	-100.00	\$0.00	0	(
1239 Baldwin	98.15	100.00	97.5	96,95	97 33	40	38	97.31	-100.00	\$0.00	o	(
1239 Baldwin	98.15		97.5	96.84	97,26	40	38	97.24	-100.00	\$0.00	0	(
1239 Baldwin	98.15	95.7	97.5	96.75	- 1,111	40	38	97.15	-100.00	\$0.00	0	
1239 Baldwin	98.15	95.7	97.5	96,63	97,05	40	38	97.03	-100.00	\$0.00	0	10
1239 Baldwin	98.15	95.7	97.5	96.52	96.95	40		96.93	-100.00	\$0.00	0	- 0
1239 Baldwin	98,15	95.7	97.5	96.38		40	38	96.80	-100.00	\$0.00	0	- (
1219 Baldwin	99.1	96.7	98.5	97.68	25 (3)	1	1	97.68	-100.00	\$0.00	0	(
1219 Baldwin	99.1	96.7	98.5	97.69	97.69	1	1	97.69		\$0.00	0	0
1219 Baldwin	99.1	96.7	98.5	97.68	97.68	1	1	97.68	-100.00	\$0.00	0	0
1219 Baldwin	99.1	96.7	98.5	97.7	97.7	1	1	97.70	-100.00	\$0.00	0	C
1219 Baldwin	99.1	96.7	98.5	97.69	97.69	1	1	97.69		\$0.00	0	
1219 Baldwin	99.1	96.7	98.5	97.7	97.7	1	1	97.70		\$0.00	0	
1219 Baldwin	99.1	96.7	98.5	97.7	97.7	1	1	97.70	-100.00	\$0.00	0	
										Rea	0	

Frequency	Summarized Damage Costs (\$)
Reg	\$0.00
100	\$0.00
50	\$0.00
25	\$0.00
10	\$0.00
5	\$0,00
2	\$0.00

- Determine flooding elevations for all storm events at buildings that potentially flood
   Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/ Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangerment

Building No.	Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream 2-100/ Reg Flood Elevations (m)	Upstream 2- 100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
1245 Baldwin	98.1	95.7	97.5	96.83	97.25	40	31	97.16	-100.00	\$0.00	0	- (
1245 Baldwin	98.1	95.7	97.5	96.95	97.33	40	31	97.24	-100.00	\$0.00	o	
1245 Baldwin	98.1	95.7	97.5	96.84	97.26	40	31	97.17	-100.00	\$0.00	0	Ĉ
1245 Baldwin	98.1	95.7	97.5	96.75	97.17	40	31	97.08	-100.00	\$0.00	0	· ·
1245 Baldwin	98,1	95.7	97,5	96.63	97.05	40	31	96.96	-100.00	\$0.00	0	
1245 Baldwin	98.1	95.7	97.5	96.52	96.95	40	31	96.85	-100.00	\$0.00	0	(
1245 Baldwin	98.1	95.7	97.5	96.38	96,82	40	31	96.72	-100.00	\$0.00	0	
1239 Baldwin	98.15	95.7	97.5	96.83	97.25	40	38	97.23	-100,00	\$0.00	Ö	
1239 Baldwin	98.15	95.7	97.5	96,95	97.33	40	38	97.31	-100.00	\$0.00	o	C
1239 Baldwin	98.15	95.7	97.5	96.84	97,26	40	38	97.24	-100.00	\$0.00	o	0
1239 Baldwin	98.15	95.7	97.5	96.75	97.17	40	38	97.15	-100.00	\$0.00	0	C
1239 Baldwin	98.15	95.7	97.5	96.63	97.05	40	38	97.03	-100.00	\$0.00	0	C
1239 Baldwin	98.15	95.7	97.5	96.52	96.95	40	38	96.93	-100.00	\$0.00	0	C
1239 Baldwin	98.15	95.7	97.5	96.38	96.82	40	38	96.80	-100.00	\$0.00	0	
1219 Baldwin	99.1	96.7	98.5	97.68	97.68	1	1	97.68	-100.00	\$0.00	0	C
1219 Baldwin	99.1	96.7	98.5	97.69	97.69	1	1	97.69	-100.00	\$0.00	0	C
1219 Baldwin	99.1	96.7	98.5	97.68	97.68	1	1	97.68	-100.00	\$0.00	0	C
1219 Baldwin	99.1	96.7	98.5	97.7	97.7	1	1	97.70	-100.00	\$0.00	0	0
1219 Baldwin	99.1	96.7	98.5	97,69	97.69	1	1	97.69	-100.00	\$0.00	0	0
1219 Baldwin	99.1	96.7	98.5	97.7	97.7	1	1	97.70	-100.00	\$0.00	0	0
1219 Baldwin	99.1	96.7	98.5	97.7	97.7	1.	1	97.70	-100.00	\$0.00	0	0

Frequency	Summarized Damage Costs (\$)
Reg	\$0.00
100	\$0.00
50	\$0.00
25	\$0.00
10	\$0.00
5	\$0.00
2	\$0.00

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
  2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangerment

Table 6	
Flooding Damages Evaluation Scale Category: Site Assessment	

Site	Event		Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth ( 50 Year, 5%) Direct Damages	Measure Weight	Category Importance/ Significance	
	(Yr)	(m)	(No.)	(No.)	(No.)	(\$)	(ha)	(\$)	(ha)	(\$)	(ha)	(\$)	(\$)	(\$)	(\$)	(1-10)	(1-10)	
	2	92.69	0	0	0	\$0	0	0	0	0	0	0	\$0	320			0242_515555	
	5	93.00	0	0	0	\$0	0	0	0	0	0	0	\$0					
	10	93.51	0	0	0	\$0	0	0	0	0	0	0	\$0		]			
24	25	93,64	2	2	0	\$31,024	0	0	0	0	0	0	\$31,024	\$2,257	\$41,209	2	8	16
	50	93.69	2	2	0	\$33,160	0	0	0	0	0	ő	\$33,160	N N	95 (Capper)			ine
	100	93.74	2	2	0	\$35,063	0	0	0	0	0	0	\$35,063					
	Reg	93.61	2	2	0	\$32,915	0	0	0	0	0	0	\$32,915					
													Total	Average Appuel	Present Worth		0.4	_

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not
- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
- 4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
- 5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

Building No.	Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream Reg Elevations	Flood (m)	Upstream 2-100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
1245 Baldy	97.6	95.2	97.0		96,83	97.25	40	31	97.16	0,17	\$16,314.55		
1245 Baldv	97.6	95,2	97.0		96,95	97_33	40	31	97.24	0.25	\$17,424.73		
1245 Baldy	97.6	95.2	97.0		96.84	97.26	40	31	97.17	0.18	\$16,435.68		
1245 Baldw	97.6	95.2	97.0		96,75	97_17	40	31	97.08	0.09	\$15,377.13	1	
1245 Baldy	97.6	95.2	97.0		96,63	97.05	40	31	96.96	-100.00	\$0.00		
1245 Baldy	97.6	95.2	97.0		96.52	96.95	40	31	96.85	-100 00	\$0.00		(
1245 Baldy	97.6	95.2	97.0		96.38	96.82	40	31	96.72	-100.00	\$0.00	0	
1239 Baldv	97.65	95.2	97.0		96.83	97.25	40	38	97.23	0.19	\$16,600.62	1	
1239 Baldy	97 65	95.2	97.0		96.95	97,33	40	38	97.31	0.27	\$17,638.71	1	
1239 Baldy	97.65	95.2	97.0		96.84	97.26	40	38	97.24	0.20	\$16,723.87	1	1
1239 Baldy	97.65	95.2	97.0		96.75	97.17	40	38	97.15	0.11	\$15,646.77		
1239 Baldy	97.65	95.2	97.0		96.63	97.05	40	38	97.03	100.00	\$0.00		
1239 Baldy	97.65	95.2	97.0		96.52	96.95	40	38	96.93	-100.00	\$0.00	,	i
1239 Baldv	97.65	95.2	97.0		96.38	96.82	40	38	96.80	-100.00	\$0.00	9	i
219 Baldy	98.6	96.2	98.0		97.68	97 68	1	1	97.68	-100.00	\$0.00	0	
219 Baldy	98.6	96.2	98.0		97.69	97_69	4	i	97.69		\$0.00	,	i
219 Baldy	98.6	96.2	98.0		97.68	97.68	1	1	97.68	-100.00	\$0.00	0	i
219 Baldy	98.6	96.2	98.0		97.7	97.7	- 1	1	97.70	-100.00	\$0.00	9	
219 Baldy	98.6	96.2	98.0		97.69	97.69	i	1	97.69	-100.00	\$0.00	U.	
219 Baldy	98.6	96.2	98.0		97.7	97.7	il	1	97.70	-100.00	\$0.00	0	
219 Baldy	98.6	96.2	98.0		97.7	97.7	il	1	97.70	-100.00	\$0.00	9	
								i	31.10		Reg	2	

Frequency Summarized Damage	Reg \$32,915.17	\$4,937		
	Reg \$32,915.17			
	Reg \$32,915.17			
1-1-1-1-1			Reg 100	Costs (\$) \$32,915,17 \$35,063,44
100 \$35,063,4* 50 \$33,159,5* 25 \$31,023,9(	***************************************		Reg 100 50	\$32,915.17 \$35,063.44 \$33,159.55

Average Annual

Damages 2007

Indirect Damages

\$339

(50 Year, 5%)

Indirect

Damages

(\$)

\$6,181

\$0.00

Category

Importance/

Significance

(1-10)

Product

Measure

Weight

(1-10)

Total

Indirect Damage

Value

(\$)

\$0

\$0

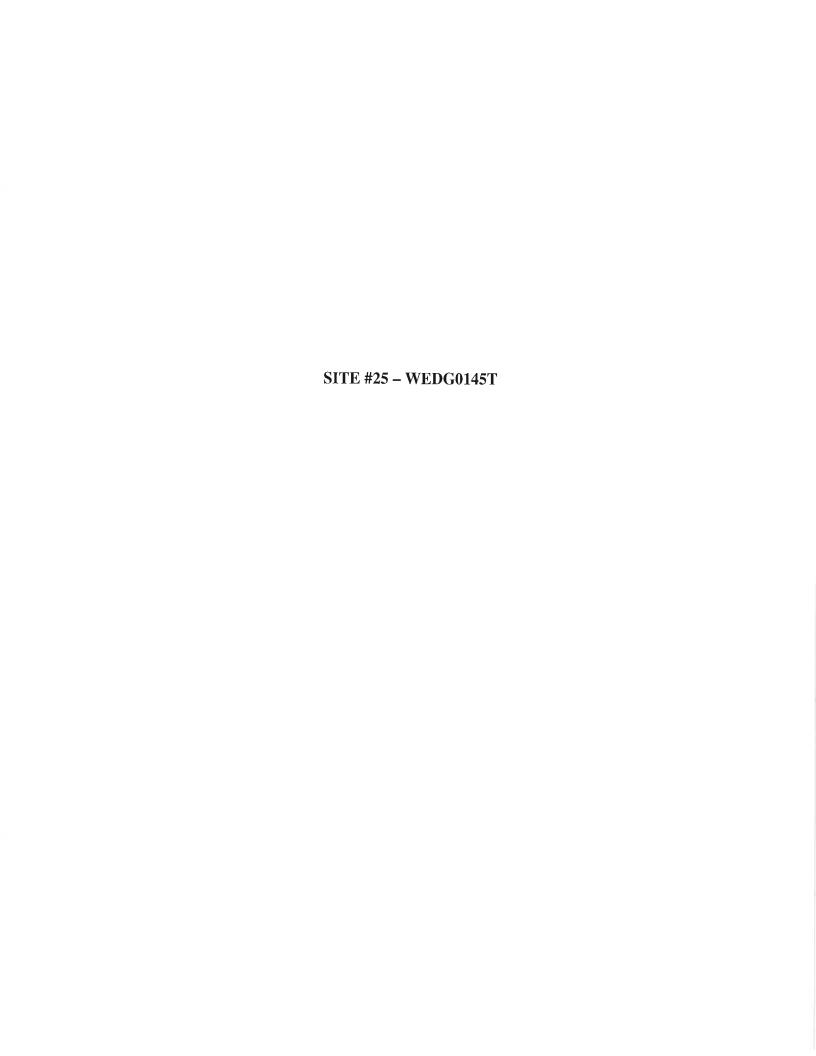
\$0

\$4,654

\$4,974

\$5,260

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine flooding damages for each return period based on the flooding depths and damage curve equations



LEGEND:

REGULATORY FLOODLINE

TOWNWIDE FLOODING STUDY

TOWN OF OAKVILLE

SITE # 25 - WEDG0145T

WEDGEWOOD CREEK

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	L
HILLOS	
ENGINEERING	ľ

	Project No.	106026
0	Date	January 2008
1	Scale	1:1000
>	Figure No.	25

### Site #25 (WEDG0145T) Implementation Program

### Recommended Management Approach/Project Scope:

- Flood proof homes on Drummond Road: 410, 420, 426, 432, 438, 444, 448 to a height of 0.33m
- Drummond Road culvert upgrade from existing 1. m by 1.2 m box culvert to 6 m by 1.8 m box culvert

### Appropriate Lead for Undertaking:

• Timing and phasing as per Town of Oakville Capital Works Program based on priority ranking established herein.

### Governing Protocol Legislation:

- Town of Oakville's Policies and protocols
- Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
- Ministry of Natural Resources Lakes and Rivers Act
- Department of Fisheries and Oceans Fisheries Act
- Ministry of Environment Water Taking (required for damming and pumping operations)

### Approval Requirements:

- Town of Oakville
- Conservation Halton Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Permit
- Regional Municipality for water and wastewater servicing alterations at Morrison Road (Site 23)
- Ministry of Environment Permit to Take Water (should dam and pumping for creek diversion or dewatering be required)
- Potentially Department of Fisheries and Oceans (i.e. should a Harmful Alteration Disruption or Destruction (HADD) be identified to occur based on the proposed works)
- Input from Utility companies for utility locations

### Need for, and Scope of Follow-Up Assessment/Analysis:

- Detailed topographic survey of creek, crossing and homes requiring flood proofing
- Vegetation assessment
- Natural channel design assessment
- Hydraulic modeling refinement
- Approval process with private land owners for flood proofing

### Suggested Timing, Need for Phasing:

 Timing of project dependant on Capital Works Program budget and priority of project within the Program.

### Possible Implementation Issues:

- Private land owners consent to proposed flood proofing
- Town of Oakville potential easement requirements
- Vegetation loss, requiring mitigation

### Possible Monitoring Requirements:

• Potentially Department of Fisheries and Oceans monitoring requirements

### Need for Maintenance:

- Potential vegetation replacement and seeding
- Potential creek stabilization resulting from local grading impacts
- Crossing maintencance

### Potential Interface with Other Town/Agency Programs:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Potential opportunities with Town's Creek Erosion Study and road work
- Potential projects already identified by Conservation Halton

### Other Funding Opportunities:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Canada/ Ontario Municipal Renewal Infrastructure Fund
- Others

# Site #25 (WEDG0145T) Specific Flood Management Alternative Assessment

### Data/Information:

### Flooding mechanisms:

- Drummond Road culvert crossing 1.2m by 1.2 m box with 1m +/- Regional storm backwater affect.
- Flood plain capacity of less than the 2 year storm 5.20 m<sup>3</sup>/s
- Encroachment

### Screened Alternatives:

- Culvert upgrade to 6m by 1.8 m concrete box.
- Road Profile improvements would be limited due to site constraints and existing road elevation
- Floodplain/ channel improvements not practical based on extent of flooding
- Flood proofing homes not flooded on all sides
- Acquisition of 8 homes would be prohibitive
- Regulate

# Preferred Management Approach:

- Upgrade culvert crossing on Drummond Road
- Flood proof homes on Drummond Road –Nos. 410,420, 426, 432, 438, 444, and 448 to an height of 0.33m. Topographic survey required to verify building elevations and flood proofing required.
- Regulate

### Potential Linkage to Adjacent Sites:

Site 27, spill across Drummond Road eliminated due to culvert upgrade

					ible 7 Evaluation Resul	ts				
			Cater	gory Evaluation Pr	oducts					
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products
25	0.6	0.0	0.0	0.0	0.0	0.0	60.0	80.0	40.0	180.6

															Table	4															_					
		<u> </u>			,							Road	Flood	ing Fl	lood C	riteri	a Eva	luatio	n																	
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation			Flood	Elevat	ions (r	m)			Ro	ad Flo	oding [	Depth (i	m)			F	low Ve	elocitie	es (m/s	)		s	torm E	vent F	requen	ісу Мо	difiers	s	Storm Event Flooding Starts/ or Criteria Not Met	Storm Event Frequency Modifier Selected	Evaluation Scale Category Importance/ Significance	Product (Measure Weighting * Storm
		(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	(2-100, Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significance
25	Design Flood Criteria	Collector	8	93,50	93.6	93,7	93,7	93.8	93.8	93.8	93.8	0.1	0.2	0,2	0,3	0.3	0,3	0,3					0.6					0.2	0.08	0.04	0.02	0.01	Collector / 1:50-yr	0.04	2	0.64
25	Private Vehicle	Level 4 Road/ 100-Regional	4	93,50	93,6	93.7	93_7	93.8	93.8	93.8	93.8	0,1	0.2	0.2	0.3	0,3	0.3	0,3	0.4	0.5	0.5	0,6	0.6	0,7	0,6	4	0.4	0.2	0.08	0.04	0.02	0.01	None	0	5	0
25	Emergency Vehicle	Level 4 Road/ 100-Regional	4	93,50	93,6	93.7	93.7	93.8	93,8	93.8	93,8	0.1	0,2	0.2	0,3	0.3	0,3	0,3	0.4	0.5	0.5	0.6	0.6	0,7	0,6	iq.	0.4	0.2	0.08	0.04	0,02	0.01	None	0.0	6	0
25	Private Vehicle Acess to Facilities	No	0	93.50	93.6	93.7	93.7	93.8	93.8	93,8	93.8	0,.1	0,2	0.2	0.3	0,3	0,3	0.3	0.4	0.5	0,5	0.6	0,6	0.7	0,6	4	0,4	0,2	0.08	0.04	0.02	0.01	None	0.0	3	0
25	Emergency Vehicle Access to Facilities	No	0	93.50	93.6	93.7	93.7	93.8	93.8	93.8	93.8	0,1	0,2	0.2	0.3	0,3	0,3	0.3	0.4	0.5	0,5	0.6	0,6	0.7	0.6	1	0,4	0,2	0.08	0,04	0,02	0.01	None	0.0	7	0
25	Private Vehicle Driveway Access (Multiuser)	NA NA	0	93,50	93.6	93.7	93.7	93.8	93.8	93.8	93.8	0.1	0.2	0.2	0.3	0.3	0.3	0.3	0.4	0.5	0.5	0.6	0.6	0.7	0.6	1	0.4	0.2	0.08	0.04	0.02	0.01	NA	0.0	4	-0

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

								,							,			т	hreat to I	Tal Life Floor	ble 5 d Criteria	Evaluat	ion																					- 0	
			Sile Downs	tream Flood E	levations (m	1)	_			Reside	ntial Units Flo	oded (#)	,			Indus	strial Area	(ha)			Commer	rcial Area (	ha)			Institution	nal (ha)		Land U	se Densiti or /uni		ha	F	eople En	dangered	4		Slorm E	vent Frequ	ency Mo	lifiers			Composite	T
ite No	2	5	10	25	50	2100	Reg	2	5	10	25	50	100	Reg	2	5	10 25	50 1	00 Reg	2 5	10	25 50	100	Reg 2	5	10 25	50	100 Res	g Res	ind Co	ari mo	tit 2	5	10 25	5 50	100 8	Reg 2	5	10 25	50	100 Re	Normalized I of People Using Storr Multipliers	Evaluation Scale Measure Welghting 10)		·10) F e) ight
<	90.27	90,36	90 44	90.63	90 77	90 91	90,86	4	7	7	7	7	7.	7	0	0	0 0	0	0 0	0 0	0	0 0	0	0 0	0	0 0	0	0 0	3	125 90	0 40	) 12	21	21 21	1 21	21	21 50	20	10 348	2	1 03	1385.4	6	10	+

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)
  2 Determine flooding conditions that results in life endangerment (separate spreadsheet direct damages). Note that for residential units, life endagerment has been included if the basement has been predicted to flood.
- 3 Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)
  4 Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered
- 5 Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm
- 6 Apply adjustment factor (Value of Step 5 divided by 10)
- 7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

	Finished	Basement		Downstream	Upstream 2		Distance	Interpolated Property 2-				
Building No.	Floor	Floor	Lowest	2-100/ Reg Flood	100/ Reg	Section	from	100/ Reg	Building	Damage	Basement	First Floor
building No.	Elevation	Elevation	Opening (m)	Elevations	Flood Elevations	Distance	Downstream	Flood	Flood Depth (m)	Costs (\$)	Flooding (Yes/ No)	Flooding (Yes/ No)
1 1	(m)	(m)	(****)	(m)	(m)		Section	Elevations (m)	(111)	(Ψ)	(165/140)	(165/140)
448 Drummon	94.2	91,8	93.6	93.81	94.24	40	4	93.85	0.26	\$17,534.64	1	
448 Drummon	94.2	91.8	93.6	93.86	94,31	40	4	93.91	0.31	\$18,222,23	. 1	
448 Drummon	94 2 94 2	91.8 91.8	93.6 93.6	93,81 93,74	94 25 94 21	40 40	4	93.85 93.79	0 26 0 20	\$17,547.61	1	
448 Drummon	94.2	91.8	93.6	93 67	94.11	40	4	93.79	0.12	\$16,699,15 \$15,821,34	1	
448 Drummon	94.2	91.8	93.6	93,62	94 04	40	4	93.66	0.07	\$15,224.34	1	
448 Drummon	94.2	91.8	93.6	93.54	93.95	40	4	93.58	-100.00	\$0.00	.0	
444 Drummon 444 Drummon	94.2 94.2	91.8 91.8	93.6 93.6	93.79 93.82	93.81 93.86	40 40	31 31	93.81	0.22	\$16,929.24	9	
444 Drummon	94.2	91.8	93.6	93 79	93.81	40	31	93,85 93,81	0.26 0.22	\$17,508.71 \$16,929.24	1	
444 Drummor	94.2	91.8	93.6	93.77	93.74	40	31	93.75	0.16	\$16,209.30	i	
444 Drummon	94.2	91.8	93.6	93.73	93 67	40	31	93,68	0.09	\$15,468.40	1	
444 Drummon 444 Drummon	94.2 94.2	91.8 91.8	93.6 93.6	93.69 93.64	93 62 93 54	40	31	93.64	0.05 -100.00	\$14,931.58	1	
438 Drummon	94.2	91,8	93.6	93.81	93.81	40	31	93.56 93.81	0.22	\$0.00	.0	
438 Drummor	94.2	91.8	93.6	93.86	93.86	1	i	93.86	0.27	\$17,625.66	1	
438 Drummor	94.2	91.8	93.6	93,81	93.81	1	1	93,81	0.22	\$16,985,69	1	
438 Drummon 438 Drummon	94 2 94 2	91.8 91.8	93.6 93.6	93.74	93.74	1	1	93.74	0.15	\$16,128.57		
438 Drummon	94.2	91.8	93.6	93.67 93.62	93.67 93.62	1		93,67 93,62	0.08	\$15,314 70 \$14,758 63	1	
438 Drummon	94.2	91.8	93.6	93.54	93.54	i	i	93.54	-100.00	\$0.00	.0	
432 Drummon	93.1	90.7	92.5	93.79	93.79	29	9	93.79	1.30	\$37,759.87	.1	
432 Drummor	93.1	90.7	92.5	93.82	93.82	29	9	93.82	1.33	\$38,607 17	1	
432 Drummon 432 Drummon	93.1 93.1	90.7 90.7	92.5 92.5	93.8 93.77	93.79 93.77	29 29	9	93.80 93.77	1.31 1.28	\$37,952.99	1	
432 Drummon	93.1	90.7	92.5	93.73	93.73	29	9	93.73	1.24	\$37,205.37 \$36,120.66	1	
432 Drummoir	93.1	90.7	92.5	93.69	93,69	29	9	93.69	1.20	\$35,067.58	i	
432 Drummor	93.1	90.7	92.5	93.64	93.64	29	9	93.64	1.15	\$33,794.29	1	
426 Drummon	93.6 93.6	91.2 91.2	93.0	93.79	93.79	31	20	93.79	0,80	\$26,085.95	1	
426 Drummon	93.6	91.2	93.0 93.0	93.82 93.8	93,82 93,8	31 31	20 20	93.82 93.80	0,83 0,81	\$26,671.30 \$26,279.63	1 3	
426 Drummon	93.6	91.2	93.0	93.77	93.77	31	20	93.77	0.78	\$25,702.88	i il	
426 Drummon	93.6	91.2	93.0	93.73	93.73	31	20	93.73	0.74	\$24,953.52	1	
426 Drummor	93.6	91.2	93.0	93.69	93,69	31	20	93.69	0.70	\$24,226.01	1	
426 Drummon 420 Drummon	93.6 93.2	91.2	93.0 92.6	93.64 93.79	93.64 93.79	31	20	93.64 93.79	0.65 1.20	\$23,346,38	1	
420 Drummon	93.2	90.8	92.6	93.82	93.82	1	1	93.79	1.20	\$35,067.58 \$35,854.46	3	
420 Drummor	93.2	90.8	92 6	93.8	93.8	1	1	93.80	1.21	\$35,327.93	3	
420 Drummon	93.2	90.8	92.6	93.77	93.77		-1	93.77	1.18	\$34,552.61	1	
420 Drummon 420 Drummon	93 2 93 2	90.8	92.6	93.73	93.73	1	1	93.73	1.14	\$33,545,24	1	
420 Drummon	93 2	90.8	92.6 92.6	93.69 93.64	93.69 93.64	1	- 4	93.69 93.64	1.10 1.05	\$32,567.24	1	
410 Drummon	93_1	90.7	92.5	93.79	93.79	30	7	93.79	1,30	\$31,384.75 \$37,759.87	i	
410 Drummor	93.1	90.7	92.5	93.82	93.82	30	7	93.82	1.33	\$38,607.17	1	
410 Drummon	93.1	90.7	92.5	93.79	93.8	30	7	93.79	1.30	\$37,825,10	1	
410 Drummon 410 Drummon	93.1 93.1	90.7 90.7	92.5 92.5	93.77 93.73	93.77 93.73	30 30	7 7	93.77 93.73	1.28	\$37,205.37	1	
410 Drummon	93.1	90.7	92.5	93.69	93.69	30	7	93.69	1,24	\$36,120.66 \$35,067.58	1	
410 Drummon	93.1	90.7	92.5	93.64	93.64	30	7	93.64	1.15	\$33,794.29	1	
1300 Amber C	93.2	90.8	92.6	92.43	92,43	1	- 1	92.43	-100.00	\$0.00	0	
1300 Amber 0 1300 Amber 0	93 2 93 2	90 8 90 8	92.6 92.6	92.47 92.43	92.47 92.43	- 1		92.47 92.43	-100.00	\$0,00	0	
1300 Amber C	93.2	90.8	92.6	92.43	92.43	i		92.43	-100.00 -100.00	\$0.00 \$0.00	0	
1300 Amber C	93.2	90.8	92.6	92.42	92.42	i	i i	92.42	-100.00	\$0.00	o	
1300 Amber C	93.2	90.8	92.6	92.42	92.42	1	- 1	92.42	-100.00	\$0.00	0	
1300 Amber C	93.2	90.8	92.6 92.7	92.42	92.42	30	1 22	92.42	-100.00	\$0.00	0	
1306 Amber C	93.3	90.9	92.7	90,86	91.46	30	22	91.30 91.36	-100.00 -100.00	\$0.00	0	
1306 Amber C	93,3	90.9	92.7	90.77	91.46	30	22	91.28	-100,00	\$0.00	0	
1306 Amber C	93,3	90.9	92.7	90.63	91.4	30	22	91.19	-100.00	\$0.00	ő	
1306 Amber 0	93,3	90.9	92.7	90.44	91 16	30	22	90.97	-100,00	\$0.00	0	
1306 Amber C 1306 Amber C	93.3 93.3	90. <b>9</b> 90. <b>9</b>	92.7 92.7	90,36 90,27	91.04 90.91	30	22 22	90.86 90.74	-100.00 -100.00	\$0.00 \$0.00	0	
1286 Cumnoc	95	92.6	94.4	93,79	93.79	1	1	93.79	-100.00	\$0.00	0	
1286 Cumnoc	95	92.6	94.4	93.82	93.82	1	1	93.82	-100,00	\$0.00	0	
1286 Cumnoc	95	92.6	94,4	93.8	93.8	1	1	93.80	-100,00	\$0.00	0	
1286 Cumnoc 1286 Cumnoc	95 95	92. <b>6</b> 92. <b>6</b>	94.4 94.4	93.77 93.73	93.77 93.73	1	1	93.77	-100,00	\$0.00	0	
1286 Cumnoc	95	92.6	94.4	93,73	93.73	1	1	93.73 93.69	-100.00 -100.00	\$0.00 \$0.00	0	
1286 Cumnoc	95	92.6	94.4	93.64	93.64	1	i	93.64	-100.00	\$0.00	0	
										Reg	7	
										100 50	7	
										25	7	
										10	7	
										5	7	
										2	4	3

Frequency	Summarized Damage Costs (S)
Reg	\$188,122.84
100	\$193,096.71
50	\$188,848,19
25	\$183,703,23
10	\$177,344.52
5	\$171,842,96
2	¢122 210 72

- Determine flooding elevations for all storm events at buildings that potentially flood
  Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/Determine basement floor elevation by substracting 2.44m from the first floor elevation
  Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
  Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
  Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangermer

Table 6
Flooding Damages Evaluation Scale Category: Site Assessment

Site	Event	WSEL	Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth ( 50 Year, 5%) Direct Damages	Measure Weight	Category Importance/ Significance	
	(Yr)	(m)	(No.)	(No.)	(No.)	(\$)	(ha)	(\$)	(ha)	(\$)	(ha)	(\$)	(\$)	(\$)	(\$)	(1-10)	(1-10)	
	2	92.69	4	4	4	\$122,320	0	0	0	0	0	0	\$122,320					-
	5	93,00	7	7	4	\$171,843	0	0	0	0	0	0	\$171,843					
	10	93.51	7	7	4	\$177,345	0	0	0	0	0	0	\$177,345		1 1			80
25	25	93.64	7	7	4	\$183,703	0	0	0	0	0	0	\$183,703	\$80,044	\$1,461,281	10	8	
	50	93.69	7	7	4	\$188,848	0	0	0	0	0	0	\$188,848		1			
	100	93.74	7	7	4	\$193,097	0	0	0	0	0	0	\$193,097					
	Reg	93,61	7	7	4	\$188,123	0	0	0	0	0	0	\$188,123					

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
  2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not

- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
  4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
  5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5%
- for Direct and Indirect Damages (for information purposes only)
  6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

Building No.	Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream Reg Elevations	2-100/ Flood (m)	Upstream 2-100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
448 Drumn	94.2	91.8	93.6		93.81	94.24	40	4	93.85	0.26	\$17,534.64	1	
448 Drumn	94.2	91.8	93.6		93.86	94.31	40	4	93.91	0.31	\$18,222.23	1	
448 Drumr	94.2	91.8	93.6	1	93.81	94.25	40	4	93.85	0.26	\$17,547.61	1	(4
448 Drumn	94.2	91.8	93.6		93.74	94,21	40	4	93.79	0.20	\$16,699.15	1 1	1.
448 Drumn	94.2	91.8	93.6		93,67	94.11	40	4	93.71	0.12	\$15,821.34	- 1	
448 Drumr	94.2	91.8	93.6		93.62	94.04	40	4	93.66	0.07	\$15,224.34	1	
448 Drumr	94.2	91.8	93.6		93,54	93.95	40	4	93.58	-100.00	\$0.00	0	
444 Drumn	94.2	91.8			93.79	93.81	40	31	93.81	0.22	\$16,929.24	1	
444 Drumr	94.2	91.8	93.6		93.82	93.86	40	31	93.85	0.26	\$17,508.71	1	
444 Drumn	94.2	91.8	93.6		93.79	93,81	40	31	93.81	0.22	\$16,929.24	1	
444 Drumn	94.2	91.8	93.6		93.77	93.74	40	31	93.75	0.16	\$16,209.30	1	
444 Drumn	94.2	91.8	93.6		93.73	93.67	40	31	93.68	0.09	\$15,468.40	1	
444 Drumr	94.2	91.8	93.6		93.69	93.62	40	31	93.64	0.05	\$14,931.58	1	
444 Drumr	94.2	91.8	93.6		93.64	93.54	40	31	93.56	-100.00	\$0.00	0	
438 Drumr	94.2	91.8	93.6		93.81	93,81	1		93.81	0.22	\$16,985.69	1	
438 Drumr	94.2	91.8	93.6		93.86	93.86	1	1	93.86	0.27	\$17,625.66	1	
438 Drumr	94.2	91.8	93.6		93.81	93.81	1	-1	93.81	0.22	\$16,985.69	1	
438 Drumr	94.2	91.8	93.6		93.74	93,74	1	1	93.74	0.15	\$16,128.57	1	
438 Drumr	94.2	91.8	93.6		93.67	93.67	1	1	93.67	0.08	\$15,314.70	1	
438 Drumr	94.2	91.8	93.6		93.62	93.62	1	1	93.62	0.03	\$14,758.63	1	
438 Drumr	94.2	91.8	93.6		93.54	93.54	1	1	93.54	-100.00	\$0.00	0	
432 Drumr	93_1	90.7	92.5		93.79	93,79	29	9	93.79	1,30	\$37,759.87	1	
432 Drumr	93.1	90.7	92,5		93.82	93.82	29	9	93.82	1.33	\$38,607.17	1	
432 Drumr	93.1	90.7	92.5		93.8	93.79	29	9	93.80	1.31	\$37,952.99	1	
432 Drumi	93.1	90.7	92.5		93.77	93.77	29	9	93.77	1.28	\$37,205.37	1	
432 Drumr	93.1	90.7	92.5		93.73	93.73	29	9	93.73	1.24	\$36,120.66	1	
432 Drumr	93.1	90.7	92.5		93.69	93.69	29	9	93.69	1.20	\$35,067.58	1	
432 Drumr	93.1	90.7	92.5		93.64	93.64	29	9	93.64	1.15	\$33,794.29	1	
426 Drumr	93.6	91.2	93.0		93.79	93.79	31	20	93.79	0.80	\$26,085.95		
426 Drumn	93.6	91.2	93.0		93.82	93.82	31	20	93.82	0.83	\$26,671.30	1	
426 Drumr	93.6	91.2	93.0		93.8	93.8	31	20	93.80	0.81	\$26,279.63	1	
426 Drumr	93.6	91,2	93.0		93.77	93.77	31	20	93.77	0.78	\$25,702.88	1	/
426 Drumr	93.6	91.2	93.0		93.73	93.73	31	20	93.73	0.74	\$24,953.52	1.	5

	\$188,123						
	Total Indirect Damage Value	Average Annual Damages 2007 Indirect Damages	Present Worth ( 50 Year, 5%) Indirect Damages	Measure Weight	Category Importance/ Significance	Product	
	(\$)	(\$)	(\$)	(1-10)	(1-10)		
	\$18,348						
	\$25,776			10			
į	\$26,602				4		
	\$27,555	\$12,007	\$219,192			40	
	\$28,327						
	\$28,965						
	\$28,218						

Frequency	Cost
Reg	\$188,122.84
100	\$193,096,71
50	\$188,848.19
25	\$183,703,23
10	\$177,344.52
5	\$171,842,96
2	\$122,319.72

Building No	Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream Reg Elevations	2-100/ Flood (m)	Upstream 2-100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
426 Drumr	93.6	91.2	93.0		93.69	93,69	31	20	93.69	0.70	\$24,226.01	1	
426 Drumr	93.6	91.2	93.0		93.64	93.64	31	20	93.64	0.65	\$23,346.38	1	
420 Drumr	93.2	90.8	92.6		93.79	93,79	1	1	93,79		\$35,067.58	1	
420 Drumr	93.2	90.8	92.6		93.82	93.82	1	1	93.82		\$35,854.46	1	
420 Drumr	93.2	90,8	92.6		93.8	93.8	1	1	93.80	1.21	\$35,327.93	1	
420 Drumr	93.2	90.8	92.6		93.77	93.77	1	1	93.77		\$34,552.61	1	
420 Drumr	93.2	90.8	92.6		93.73	93.73	1	1	93,73		\$33,545,24	1	
420 Drumr	93.2	90.8	92.6		93.69	93.69	1	1	93,69		\$32,567,24	1	
420 Drumr	93.2	90.8	92.6		93.64	93.64	1	1	93.64		\$31,384.75	1	
410 Drumr	93.1	90.7	92.5		93.79	93.79	30	7	93,79	1 (200.1)	\$37,759.87	1	
410 Drumr	93.1	90.7	92.5		93.82	93.82	30	7	93,82		\$38,607.17	1	-
410 Drumr	93.1	90.7	92.5		93.79	93.8	30	7	93.79	1:30	\$37,825.10		
410 Drumr	93.1	90,7	92.5		93.77	93.77	30	7	93,77	1.28	\$37,205.37	1	
410 Drumr	93.1	90.7	92.5		93.73	93.73	30	7	93.73		\$36,120.66	- 1	
410 Drumr	93.1	90.7	92.5		93.69	93.69	30	7	93,69		\$35,067.58	1	1
410 Drumr	93.1	90.7	92.5		93.64	93.64	30	7	93.64	10000	\$33,794.29	1	1
1300 Amb	93.2	90.8	92.6		92.43	92.43	1	1	92.43	-100.00	\$0.00	0	(
1300 Ambi	93.2	90.8	92.6		92 47	92.47	1	1	92.47	-100.00	\$0.00	0	(
1300 Ambi	93.2	90.8	92.6		92,43	92.43	1	1	92.43	-100.00	\$0.00	0	(
1300 Amb	93.2	90_8	92.6		92.47	92,47	1	1	92.47	-100.00	\$0.00	0	(
1300 Amb	93.2	90.8	92.6		92.42	92.42	1	1	92.42	-100.00	\$0.00	0	
1300 Amb	93.2	90.8	92.6		92.42	92,42	1	1	92.42	-100.00	\$0.00	0	
1300 Amb	93.2	90.8	92.6		92.42	92.42	1	1	92.42		\$0.00		
1306 Amb	93,3	90.9	92.7		90.86	91.46	30	22	91.30	-100.00	\$0.00	0	
1306 Amb	93.3	90.9	92.7		90.91	91,53	30	22	91.36	0. 9	\$0.00	0	
1306 Amb	93,3	90.9	92.7		90,77	91.46	30	22	91.28		\$0.00	0	(
1306 Amb	93,3	90.9	92.7		90.63	91.4	30	22	91,19	- AU 21	\$0.00	0	(
1306 Amb	93.3	90.9	92.7		90.44	91.16	30	22	90.97	-100.00	\$0.00	0	(
1306 Ambi	93.3	90.9	92.7		90.36	91.04	30	22	90.86	- 1	\$0.00	0	(
1306 Amb	93.3	90.9	92.7		90.27	90.91	30	22	90.74		\$0.00	0	
1286 Cumi	95	92.6	94.4		93.79	93.79	1	1	93.79	-100.00	\$0.00	0	(
1286 Curri	95	92.6	94.4		93.82	93.82	1	1	93.82		\$0.00	0	0
1286 Cum	95	92.6	94.4		93.8	93,8	.1	1	93.80	-100.00	\$0.00	0	(
1286 Cumi	95	92.6	94.4		93.77	93.77	1	1	93.77		\$0.00	0	(
1286 Cumi	95	92.6	94.4		93.73	93.73	1	1	93.73	-100.00	\$0.00	0	(
1286 Cumi	95	92.6	94.4		93.69	93,69	-1	1	93.69	-100.00	\$0,00	0	C
1286 Cumi	95	92.6	94.4		93.64	93.64	1	1	93.64	-100.00	\$0.00	0	

Frequency	Cost

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
  2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
  4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding depths and damage curve equations
  6 Determine flooding damages for each return period based on the flooding depths and damage curve equations



LEGEND:

REGULATORY FLOODLINE

TOWNWIDE FLOODING STUDY

TOWN OF OAKVILLE

SITE # 26 - WEDG1810M

WEDGEWOOD CREEK



	The state of the s
Project No.	106026
Date	January 2008
Scale	1:2,000
Figure No.	26

# Site #26 (WEDG1810M) Specific Flood Management Alternative Assessment

## Data/Information:

## Flooding mechanisms:

- Duncan Road crossing 2.3 m by 1.8 m elliptical CSP with Regional storm backwater of 1.2 m +/-
- Floodplain capacity of 2-5 year storm 16.2 m<sup>3</sup>/s to 20.7 m<sup>3</sup>/s
- Encroachment

## Screened Alternatives:

- Crossing upgrades 6 m by 2.1 m box culvert at Duncan Road
- Road profile improvement not practical due to existing driveways, lot grading and culvert configuration
- Floodplain/channel upgrades not practical due to natural vegetation and resulting limited hydraulic improvement
- Flood-proofing not a stand alone alternative
- Acquisition
- Regulate

# Preferred Management Approach:

- Culvert upgrades
- Flood-proofing of 1373 and 1379, by 0.15 m and 0.25 m respectively. Topographic survey required to verify building elevations and flood proofing required after culvert upgrades complete.
- Regulate

## Potential Linkage to Adjacent Sites:

• Site 22

## Site #26 (WEDG1810M) Implementation Program

# Recommended Management Approach/Project Scope:

- Flood proofing of 1373 and 1379 Duncan Road by 0.15m and 0.25 m respectively
- Duncan Road crossing upgrade from 2.3 m by 1.8 m elliptical CSP to 6 m by 2.1 m box culvert

## Appropriate Lead for Undertaking:

 Timing and phasing as per Town of Oakville Capital Works Program based on priority ranking established herein.

#### Governing Protocol Legislation:

- Town of Oakville's Policies and protocols
- Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
- Ministry of Natural Resources Lakes and Rivers Act
- Department of Fisheries and Oceans Fisheries Act
- Ministry of Environment Water Taking (required for damming and pumping operations)

## Approval Requirements:

- Town of Oakville
- Conservation Halton Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Permit
- Regional Municipality for water and wastewater servicing alterations
- Ministry of Environment Permit to Take Water (should dam and pumping for creek diversion or dewatering be required)
- Potentially Department of Fisheries and Oceans (i.e. should a Harmful Alteration Disruption or Destruction (HADD) be identified to occur based on the proposed works)
- Input from Utility companies for utility locations

## Need for, and Scope of Follow-Up Assessment/Analysis:

- Detailed topographic survey of creek, crossing and homes to be flood proofed
- Vegetation assessment at crossing
- Natural channel design assessment
- Hydraulic modeling refinement
- Approval process with private land owners

#### Suggested Timing, Need for Phasing:

 Timing of project dependant on Capital Works Program budget and priority of project within the Program.

### Possible Implementation Issues:

- Private land owners consent to proposed flood proofing
- Town of Oakville potential easement requirements
- Vegetation loss, requiring mitigation

### Possible Monitoring Requirements:

Potentially Department of Fisheries and Oceans monitoring requirements

#### Need for Maintenance:

- Potential vegetation replacement and seeding
- Potential creek stabilization resulting from local grading impacts
- Crossing maintenance

## Potential Interface with Other Town/Agency Programs:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Potential opportunities with Town's Creek Erosion Study and road work
- Potential projects already identified by Conservation Halton

#### Other Funding Opportunities:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Canada/ Ontario Municipal Renewal Infrastructure Fund
- Others

Tal	ble 7		
Summary of Site	Evaluation Resu	lts	
gory Evaluation Pro	ducts		AN
Drivate Vehicle	Emorgonov	Drivete Multi	T T

	Catergory Evaluation Products												
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products			
26	0.6	30.0	0.0	0.0	0.0	0.0	50.0	32.0	16.0	128.6			

												Road	Flood		able ood C		Eval	uatio	1													-				
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation			Flood	l Eleva	tions (r	m)	-		Ro	ad Flo	oding [	Depth (	m)			F	low Ve	locitie	es (m/s)			S	torm E	vent Fr	equenc	y Mod	ifiers		Storm Event Flooding Starts/ or Criteria Not Met	Storm Event Frequency Modifier Selected	Evaluation Scale Category Importance/ Significance	Product (Measure Weighting *
		(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Rea	(2-100, Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significance
26	Design Flood Criteria	Collector	8	93,85	94,2	94.3	94.4	94.5	94.6	94.7	7 94.4	0.4	0.4	0.5	0.7	0.7	0.8	0,6						1.3			0.4							0.04	2	0.64
26	Private Vehicle	Level 3 Road/ 100-Regional	6	93.85	1			1	1											- 1				1.3		- 1	0.4	- 1	- 1					1.0	5	30
26	Emergency Vehicle	Level 3 Road/ 100-Regional	6	93.85	94.2	94,3	94.4	94.5	94.6	94.7	7 94.4	0.4	0,4	0.5	0.7	0.7	0.8	0,6	0.6	0.8	0.9	1.1	1,2	1,3	1.0	1	0.4	0.2	0.08	.04	0.02	0.01	None	0.0	6	0
26	Private Vehicle Acess to Facilities	No	0									1							1	- 1				1.3		- 1	0.4					- 1	None	0.0	3	0
26	Emergency Vehicle Access to Facilities	No	0	93.85	94.2	94.3	94.4	94.5	94.6	94.7	94.4	0.4	0.4	0,5	0.7	0.7	0.8	0.6	0.6	0.8	0.9	1.1	1,2	1.3	1.0	1	0.4	0.2	.08	.04	0.02	0.01	None	0.0	7	0
26	Private Vehicle Driveway Access (Multiuser)	NA	0	93.85	1	1	m			1	94.4	1	1 1						- 1	- 1	- 1			1.3		- 1	-	0.2						0.0	4	0

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

			_														т	hreat to	Ta Life Floo	ble 5 d Criteria	Evaluatio	n																					
-			Site Downs	tream Flood E	levations (m)	)			,	Resid	ential Units Flo	oded (#)				Indu	striol Area (ha)			Commer	ial Area (h	1)		lns	ututional (ha	)	Land	Use Densi	the first of the same of the same	ha or		People E	ndangere	нd		Storm E	vent Frequ	rency Mo	idiors			Compo	site
e No	2	184	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5	10 25 50 1	00 Reg	2 6	5 10	25 50	100 Re	ng 2	5 10	25 5	100	Reg Res	Ind	Com to	stit 2	5	10 2	25 50	100	Reg 2	5	10 25	50	100 Re	Normalize No. of Peop Using Stor Multipliers	m	Categ Imports Significand 1- (7 - Day L (10 - Day an Usag	ory incel ie (1-10) Isago) ad Night
	93.24	94.34	94.58	9431	91.24	94.18	94 02	2	2	2	2	2	2	2	0	0	0 0 0	0 0	0 (	0	0 0	0 0	0	0 0	0 0	0	0 3	125	50 4	6 6	6	6	6 6	3	0 50	20	10 4	2	1 04	519	5	10	

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)
  2 Determine flooding conditions that results in life endangerment (separate spreadsheet direct damages). Note that for residential units, life endagerment has been included if the basement has been predicted to flood.
  3 Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)
- 4 Determine number of people endagered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered
- 5 Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm 6 Apply adjustment factor (Value of Step 5 divided by 10)
  7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

		r — — —										
	Finished Floor	Basement Floor	Lowest	Downstream 2-100/ Reg	Upstream 2- 100/ Reg	Section	Distance from	Interpolated Property 2- 100/ Reg	Building	Damage	Basement	First Floor
Building No.	Elevation	Elevation	Opening	Flood	Flood	Distance	Downstream	Flood	Flood Depth	Costs	Flooding	Flooding
	(m)	(m)	(m)	Elevations	Elevations	Didiano	Section	Elevations	(m)	(\$)	(Yes/ No)	(Yes/ No)
	(,	\ <i>,</i>		(m)	(m)		Codion	(m)				
1373 Duncan	94.6	92.2	94.0	94,39	94.53	50	8		0.42	\$19,728.93	1	0
1373 Duncan	94.6	92.2	94.0	94.6	94.84	50	8	94.64	0.65	\$23,318.77	1	1
1373 Duncan	94.6	92.2	94.0	94.53	94.73	50	8	94.56	0.57	\$22,037.50	1	0
1373 Duncan	94_6	92,2	94.0	94,45	94,61	50	8	94.48	0.49	\$20,673.14	1	0
1373 Duncan	94.6	92,2	94.0	94,34	94.46	50	8	94.36	0.37	\$18,967.64	1	0
1373 Duncan	94.6	92,2	94.0	94.25	94.35	50	8	94.27	0.28	\$17,704.06	1	0
1373 Duncan	94.6	92.2	94_0	94.19	94.25	50	8	94.20	0.21	\$16,855.52	1	0
1379 Duncan	94.7	92.3	94.1	94.39	94.53	50	8	94.41	0.32	\$18,322.25	1	0
1379 Duncan	94.7	92.3	94.1	94.6	94.84	50	8	94.64	0.55	\$21,656.13	1	0
1379 Duncan	94.7	92.3	94.1	94.53	94.73	50	8	94.56	0.47	\$20,466.21	1	0
1379 Duncan	94.7	92.3	94.1	94.45	94.61	50	8	94,48	0.39	\$19,199.14	1	0
1379 Duncan	94.7	92.3	94.1	94.34	94.46	50	8	94.36	0.27	\$17,615.24	1	0
1379 Duncan	94.7	92.3	94.1	94.25	94.35	50	8	94.27	0.18	\$16,441.76	1	0
1379 Duncan	94.7	92.3	94.1	94.19	94.25	50		94.20	0:11	\$15,653.71	1	0
1380 Acton Ct	96.1	93.7	95.5	94.54	94.44	40	3	94,53	-100.00	\$0.00	0	0
1380 Acton C	96.1	93.7	95.5	94.84	94.75	40	3	94.83	-100.00	\$0.00	0	0
1380 Acton C	96.1	93.7	95.5	94.73	94.64	40	3	94.72	-100.00	\$0.00	0	0
1380 Acton C	96.1	93.7	95.5	94.62	94.52	40	3	94.61	-100.00	\$0.00	0	0
1380 Acton Ct	96.1	93.7	95.5	94.47	94.37	40	3	94.46	-100.00	\$0.00	0	0
1380 Acton C	96.1	93.7	95.5	94.35	94.25	40	3	94.34	-100.00	\$0.00	0	0
1380 Acton Cl	96.1	93.7	95.5	94,25	94.17	40	3	94.24	-100.00	\$0.00	0	0
1372 Acton C	96.1	93.7	95.5	94.54	94.44	40	11	94.51	-100.00	\$0.00	0	0
1372 Acton Ct	96.1	93.7	95.5	94.84	94.75	40	11	94.82	-100.00	\$0.00	0	0
1372 Acton C	96_1	93.7	95.5	94.73	94.64	40	11	94.71	-100.00	\$0.00	0	0
1372 Acton C	96.1	93.7	95.5	94.62	94.52	40	11	94.59	-100.00	\$0.00	0	0
1372 Acton C	96.1	93.7	95.5	94.47	94.37	40	11	94.44	-100.00	\$0,00	0	0
1372 Acton Cl	96.1	93.7	95.5	94.35	94.25	40	11	94.32	-100.00	\$0,00	0	0
1372 Acton Cl	96.1	93.7	95.5	94.25	94.17	40	11	94.23	-100.00	\$0.00	- 0	0
1368 Acton C	96.2	93,8	95.6	94.54	94,44	40	22	94.49	-100.00	\$0.00	0	0
1368 Acton C	96.2	93.8	95.6	94.84	94.75	40	22	94.79	-100.00	\$0.00	0	0
1368 Acton Ci	96.2	93.8	95.6	94.73	94.64	40	22	94.68	-100.00	\$0.00	0	0
1368 Acton C	96.2	93.8	95.6	94.62	94.52	40	22	94.57	-100.00	\$0.00	0	0
1368 Acton C	96.2	93.8	95.6	94.47	94,37	40	22	94.42	-100.00	\$0.00	0	0
1368 Acton Ci	96.2	93.8	95.6	94.35	94.25	40	22	94.30	-100.00	\$0.00	0	0
1368 Acton C	96.2	93.8	95.6	94.25	94.17	40	22	94.21	-100.00	\$0.00	0	0
										Rea	2	0

requency	Summarized Damage Costs (\$)
Reg	\$38,051.19
100	\$44,974.90
50	\$42,503.71
25	\$39,872,28
10	\$36,582.87
5	\$34,145.82
2	\$32,509.23

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangerment

Table 6	
Flooding Damages Evaluation Scale Category: Site Assessment	

Site	Event	WSEL	Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth (50 Year, 5%) Direct Damages	Measure Weight	Category Importance/ Significance	Produc
	(Yr)	(m)	(No.)	(No.)	(No.)	(S)	(ha)	(S)	(ha)	(S)	(ha)	(\$)	(S)	(S)	(S)	(1-10)	(1-10)	
	2	92.69	2	2	0	\$32,509	0	0	0	0	0	0	\$32,509			3.71.7.00		
	5	93.00	2	2	0	\$34,146	0	0	0	0	0	0	\$34,146	1				
	10	93.51	2	2	0	\$36,583	0	0	0	0	0	0	\$36,583	1				
26	25	93.64	2	2	0	\$39,872	0	0	0	0	0	0	\$39.872	\$17,524	\$319,914	4	8	32
	50	93.69	2	2	0	\$42,504	0	0	0	0	0	0	\$42,504		1900,000,000		_	
	100	93.74	2	2	1	\$44,975	0	0	0	0	0	0	\$44,975					
	Reg	93.61	2	2	0	\$38,051	0	ò	0	0	0	0	\$38,051					1
													Total	Average Annual	Present Worth	Massura	Category	

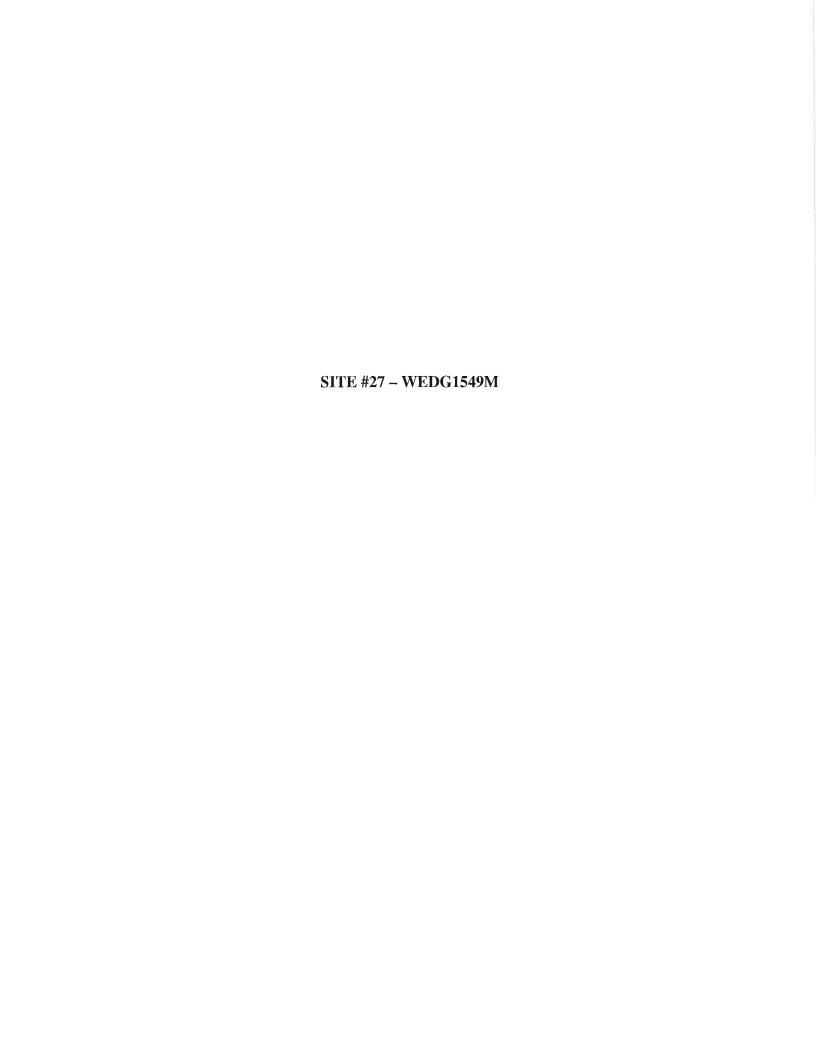
- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not
- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
- 4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
- 5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

Building No.	Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream Reg Elevations	2-100/ Flood (m)	Upstream 2-100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Floodin (Yes/ No)
373 Dunc	94.6	92.2	94.0		94.39	94.53	50	8	94.41	0.42	\$19,728.93		
373 Dunc	94.6	92.2			94.6	94 84	50	8	94.64	0.65	\$23,318.77	l i	}
373 Dunc	94.6	92.2			94.53	94.73	50	8	94.56	0.57	\$22,037,50		
373 Dune	94.6	92.2			94.45	94.61	50	8	94.48	0.49	\$20,673.14	1 1	
373 Dunc	94.6	92.2	94.0		94.34	94.46	50	8	94.36	0.37	\$18,967.64	l i	
373 Dune	94.6	92.2			94.25	94.35	50	8	94.27	0.28	\$17,704.06	1	
373 Dunc 379 Dunc	94.6	92.2	94.0		94.19	94.25	50	8	94.20	0.21	\$16,855.52		
379 Dunc	94.7 94.7	92.3	94.1		94.39	94.53	50	8	94.41	0.32	\$18,322.25	1	
379 Dune		92.3			94.6	94.84	50	8	94.64	0.55	\$21,656.13	1	
379 Dunc	94.7	92 3 92 3	94.1 94.1		94.53	94.73	50	- 8	94.56	0.47	\$20,466.21	1	
379 Dune	94.7	92 3	94.1		94.45	94,61	50	8	94.48	0,39	\$19,199_14	1	
379 Dune	94.7	92.3	94.1		94.34	94.46	50	8	94,36	0.27	\$17,615.24	1	
379 Dunc	94.7	92.3	94.1		94.25	94,35	50	8	94.27	0.18	\$16,441.76	1	
380 Actor	96.1	93.7	95.5		94.54	94.25	.50	8	94.20	0.11	\$15,653.71	1	
380 Actor	96.1	93.7	95.5		94.84	94.44	40	3	94.53	-100.00	\$0.00	0	
380 Actor	96.1	93.7	95.5		94.64	94.75 94.64	40	3	94,83	-100,00	\$0.00	0	
380 Actor	96.1	93.7	95.5		94.62	94.52	40	3	94,72	-100.00	\$0.00	0	
380 Actor	96.1	93.7	95.5		94.47	94.37	40	3	94.61	-100.00	\$0.00	0	Į.
380 Actor	96.1	93.7	95.5		94.35	94.37	40	3	94.46	-100.00	\$0.00	0	
380 Actor	96.1	93.7	95.5		94 25	94 17	40	3	94.34	-100.00	\$0.00	0	
372 Actor	96.1	93.7	95.5		94.54	94.44	40	11	94.24	-100.00	\$0.00	0	
372 Actor	96.1	93.7	95.5		94.84	94 75	40	11	94.51	-100.00	\$0.00	0	
372 Actor	96.1	93.7	95.5		94.73	94.64	40	11	94.82 94.71	-100.00	\$0.00	9	<u>(</u>
372 Actor	96.1	93.7	95.5		94.62	94.52	40	11	94.71	-100.00	\$0.00	0	l .
372 Actor	96.1	93.7	95.5		94.47	94.37	40	11	94 44	-100.00 -100.00	\$0.00	.0	
372 Actor	96.1	93.7	95.5		94.35	94,25	40	11	94.32	-100.00	\$0.00	0	
372 Actor	96.1	93.7	95.5		94.25	94.17	40	11	94.23	-100.00	\$0.00 \$0.00	0	
368 Actor	96.2	93.8	95.6		94.54	94.44	40	22		-100.00	\$0.00	- 0	
368 Actor	96.2	93.8	95.6		94.84	94.75	40	22		-100.00	\$0.00	0	
368 Actor	96.2	93.8	95.6		94.73	94,64	40	22	94.68	-100.00	\$0.00	0	
368 Actor	96.2	93.8	95.6		94.62	94.52	40	22	94.57	-100.00	\$0.00	0	
368 Actor	96.2	93.8	95.6		94.47	94.37	40	22	94.42	-100.00	\$0.00	0	
368 Actor	96.2	93.8	95.6		94.35	94.25	40	22	94 30	-100.00	\$0.00	0	
368 Actor	96.2	93.8	95.6		94.25	94.17	40	22	94.21	-100.00	\$0.00	0	
										100.00	Reg	2	
											100	2	
											50	2	
											25	2	

			Damages	2303-8500	Significance	Prod
	(S)	(S)	(\$)	(1-10)	(1-10)	
s	4,876					
\$	5,122					
\$	5,487					
s	5,981	\$2,629	\$47,987	4	- 4	16
S	6,376					
S	6,746					
\$	5,708					

Frequency	Summarized Damage Costs (\$)
Reg	\$38,051.19
100	\$44,974.90
50	\$42,503,71
25	\$39,872.28
10	\$36,582.87
5	\$34,145.82
2	\$32,509.23

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine flooding damages for each return period based on the flooding depths and damage curve equations



LEGEND:

REGULATORY FLOODLINE

TOWNWIDE FLOODING STUDY TOWN OF OAKVILLE SITE # 27 - WEDG1549M WEDGEWOOD CREEK



_		
	Project No.	106026
	Date	January 2008
	Scale	1:750
	Figure No.	27

### Site #27 (WEDG1549M) Implementation Program

# Recommended Management Approach/Project Scope:

- Amber Crescent crossing upgrade from 2.7 m by 2.2 m CSP arch to 6 m by 1.2 m concrete box
- Flood proofing of homes still flooded after crossing upgrade
- Implement Devon Road Culvert Improvements separate Town of Oakville Project

## Appropriate Lead for Undertaking:

• Timing and phasing as per Town of Oakville Capital Works Program based on priority ranking established herein.

## Governing Protocol Legislation:

- Town of Oakville's Policies and protocols
- Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
- Ministry of Natural Resources Lakes and Rivers Act
- Department of Fisheries and Oceans Fisheries Act
- Ministry of Environment Water Taking (required for damming and pumping operations)

### Approval Requirements:

- Town of Oakville
- Conservation Halton Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Permit
- Regional Municipality for water and wastewater servicing alterations at Morrison Road (Site 23)
- Ministry of Environment Permit to Take Water (should dam and pumping for creek diversion or dewatering be required)
- Potentially Department of Fisheries and Oceans (i.e. should a Harmful Alteration Disruption or Destruction (HADD) be identified to occur based on the proposed works)
- Input from Utility companies for utility locations

## Need for, and Scope of Follow-Up Assessment/Analysis:

- Detailed topographic survey of creek, Amber Road and Devon Road culverts and homes within Regulatory floodplain
- Vegetation assessment
- Natural channel design assessment
- Hydraulic modeling refinement
- Approval process with private land owners for flood proofing

### Suggested Timing, Need for Phasing:

• Timing of project dependant on Capital Works Program budget and priority of project within the Program.

### Possible Implementation Issues:

- Private land owners consent to proposed grading of creek adjacent to culvert upgrade
- Town of Oakville potential easement requirements
- Vegetation loss, requiring mitigation

### Possible Monitoring Requirements:

Potentially Department of Fisheries and Oceans monitoring requirements

## Need for Maintenance:

- Potential vegetation replacement and seeding
- Potential creek stabilization resulting from local grading impacts
- Crossing(s) maintenance

# Potential Interface with Other Town/Agency Programs:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Potential opportunities with Town's Creek Erosion Study and road work
- Potential projects already identified by Conservation Halton

#### Other Funding Opportunities:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Canada/ Ontario Municipal Renewal Infrastructure Fund
- Others

# Site #27 (WEDG1549M) Specific Flood Management Alternative Assessment

## Data/Information:

## Flooding mechanisms:

- Devon Road to Amber Cres. floodplain capacity and culvert capacity
- Amber Cres. and upstream floodplain capacity and culvert capacity
- Encroachment

## Screened Alternatives:

- Floodplain improvements not very practical based on private property and existing natural vegetation
- Devon Road culvert improvements being undertaken by the Town of Oakville under separate study twin 4.27 m span Conspan culverts
- Culvert improvement on Amber Cres. from 2.7 m by 2.2 m CSP arch to 6 m by 1.2 m concrete box
- Flood-proofing
- Regulate

## Preferred Management Approach:

- Amber Cres. culvert improvement
- Flood-proof homes to extent possible, would require topographic survey to verify building elevations and flood proofing possible.
- Consider acquisition of 1355 Devon Road
- Regulate

## Potential Linkage to Adjacent Sites:

No linkage

				Summary of Site	able 7 Evaluation Resul	ts				
			Cate	gory Evaluation Pr						
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Direct Damages	Combined Products
27	0.0	0.0	0.0	0.0	0.0	0.0	50.0	32.0	16.0	98.0

														Tal	ole 4																				
			-								R	ad Flo	oding	Floo	d Crit	eria Ev	aluatio	on																	
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation			Flood	Elevatio	ons (m)	)			Road	Flood	ing De	oth (m)				Flow V	'elocitic	es (m/s	s)			Storm	Event f	reque	ency M	odifier	s	Storm Event Flooding Starts/ or Criteria Not Met	Storm Event Frequency Modifier Selected	Evaluation Scale Category Importance/ Significance	Weighting
		(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5	10	25	50 10	) Reg	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	(2-100, Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significance
27	Design Flood Criteria	Collector	8	90,80	89.0	89,1	89.3	89,4	89,8	90,1	90.0	0.0	0.0	0.0	0.0	0.0	0,0	0.0	0.0	0,0	0,0	0,0	0.0	0.0	î	0.4	0.2	0_08	0.04	0,02	0.01	None	0.0	2	0
27	Private Vehicle	Level 3 Road/ 100-Regional	6	90.80	89.0	89.1	89.3	89,4	89.8	90,1	90,0	0.0	0.0	0.0	0,0	0 0.0	0.0	0,0	0,0	0.0	0,0	0,0	0.0	0,0	1	0.4	0.2	0.08	0.04	0.02	0.01	None	0.0	5	0
27	Emergency Vehicle	Level 3 Road/ 100-Regional	6	90,80	89,0	89,1	89.3	89.4	89.8	90.1	90,0	0.0	0.0	0.0	0.0	0 0.0	0.0	0,0	0,0	0.0	0,0	0.0	0.0	0.0	1	0.4	0,2	0.08	0.04	0.02	0.01	None	0.0	6	0
27	Private Vehicle Acess to Facilities	No	0	90.80	89.0	89.1	89.3	89.4	89.8	90.1	90,0	0.0	0.0	0.0	0,0	.0 0.0	0.0	0.0	0,0	0.0	0.0	0.0	0.0	0.0	1	0.4	0.2	0.08	0.04	0.02	0.01	None	0.0	3	0
27	Emergency Vehicle Access to Facilities	No	0	90.80	89.0	89.1	89.3	89.4	89.8	90.1	90.0	0.0	0.0	0,0	0,0	.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0	0.0	1	0.4	0.2	0,08	0.04	0.02	0.01	None	0.0	7	0
27	Private Vehicle Driveway Access (Multiuser)	NA NA	0	90,80	89.0	89.1	89.3	89.4	89.8	90,1	90.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1	0.4	0.2	0.08	0.04	0.02	0.01	None	0.0	4	0

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

																			Thre	at to Life	Table 5 Flood Crite	ria Evalu	ation																					
			Site Down	stream Flood	Elevations	s (m)					Reside	antial Units FI	ooded (#)				Indus	rial Area (7	10)		Com	mercial An	ea (ha)			Institution	al (ha)		Land U	se Densille or /unil)	s (pers/ ha		People	e Endange	red		Storn	Event Fr	equency M	difiers			Composite	
Site No	2	5	10	25	50		100	Reg	2	5	10	26	50	100	Reg	2	5	0 25	50 100	Reg	2 5 14	25	50 100	Reg 2	5	10 25	50	100 Reg	Res	Ind Con	n Instit	2	5 10	25 5	100	Reg	2 5	10	25 50	100	Normalize No. of Peo Using Stor Multiplier	Evaluation Scale Measure Weighting	Category Importance/ Significance (1- (7 - Day Usage (10 - Day and Ni Usage)	-10) Prod e) ght
27	89.32	89.45	89.65	89.85	90	- 1	90.13:	90.09	3	2	3.	4	6	7	6	0	0	0 0	0 0	0	0 0	0	0 0	0 0	0	0 0	0	0 0	3	125 90	40	9 (	6 9	12 1	8 21	18	50 20	10	4 2	3 3	0.4 772.2	5	10	50

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)
  2 Determine flooding conditions that results in life endangerment (separate spreadsheet direct damages). Note that for residential units, life endagerment has been included if the basement has been predicted to flood.
- 3 Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)
- 4 Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered
- 5 Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm
- 6 Apply adjustment factor (Value of Step 5 divided by 10)
- 7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

	Finished	Basement		Downstream	Upstream 2			interpolated				
	Floor	Floor	Lowest	2-100/ Reg	100/ Reg	Section	Distance from	Property 2-	Building	D	Basement	First Floor
Building No.	Elevation	Elevation	Opening	Flood	Flood	Distance	Downstream	100/ Reg Flood	Flood Depth	Damage	Flooding	Flooding
1 1	(m)	(m)	(m)	Elevations	Elevations	Distance	Section	Elevations	(m)	Costs (\$)	(Yes/No)	(Yes/ No
		(,		(m)	(m)			(m)				
1347 Devon F	91,2	88.8	90.6	90,01	90.78	60	30		-100.00	\$0.00		
1347 Devon R	91.2	88.8	90,6		90,86	60	30		+100.00	\$0.00		
1347 Devon F	91.2	88.8	90.6		90,51	60	30	90.15	-100.00	\$0.00	0	
1347 Devon F	91.2	88.8	90.6	90_13	90,91	60	30	90.52	-100,00	\$0.00	0	
1347 Devon F	91.2	88.8	90.6	89.64	90,36	60	30	90.00	-100.00	\$0.00	0	
1347 Devon F	91.2 91.2	8.88 8.88	90,6	90	90.76	60	30	90,38	-100.00	\$0.00	0	
1351 Devon F	90.7	88,3	90.6	89.48	90.22	60	30	89.85	-100.00	\$0.00	0	
1351 Devon F	90.7	88,3	90.1	90.09 90.13	90.9 90.94	50 50	10	90.25	0.16	\$16,272.37	[ 1]	
1351 Devon F	90.7	88.3	90.1	90	90,78	50	10 10	90.29	0.20	\$16,761.03		
1351 Devon F	90.7	88 3	90.1	89.85	90.61	50	10	90.16 90.00	0.07 -100.00	\$15,156.92	1	
1351 Devon F	90.7	88.3	90 1	89.65	90,36	50	10	89.79	-100.00	\$0.00 \$0.00	0	
1351 Devon F	90.7	88.3	90.1	89.45	90.19	50	10	89.60	-100.00	\$0.00	0	
1351 Devon F	90.7	88.3	90.1	89.32	90.01	50	10	89.46	-100.00	\$0.00	ő	
1355 Devon H	90.2	87.8	89.6	90.09	90.9	50	25	90.50	0.90	\$28,192.77	ĭ	
1355 Devon F	90.2	87.8	89.6	90 13	90.94	50	25	90.54	0.94	\$29,039 40	1	
1355 Devon F	90.2	87.8	89.6	90	90.78	50	25	90.39	0.80	\$26,085.95	1	
1355 Devon F	90.2	87.8	89.6	89.85	90.61	50	25	90.23	0.64	\$23,174.33	1	
1355 Devon F	90 2	87.8	89.6	89.65	90.36	50	25	90.01	0_41	\$19,621.24	1	
1355 Devon F 1355 Devon F	90.2	87 8	89.6	89,45	90.19	50	25	89.82	0.23	\$17,111.80	1	
1372 Devon F	90.2	87.8 89.0	89.6 90.8	89.32	90.01	50	25	89.67	0.07	\$15,258.16	1	
1372 Devon F	91.4	89.0	90.8	90.09 90.13	90.94	50 50	31	90.59	-100.00	\$0.00	0	
1372 Devon F	91.4	89.0	90.8	90	90.78	50	31 31	90.63	-100,00	\$0.00	0	
1372 Devon F	91.4	89.0	90.8	89.85	90.61	50	31	90.48 90.32	-100.00 -100.00	\$0.00 \$0.00	0	
1372 Devon F	91.4	89.0	90.8	89.65	90.36	50	31	90.09	-100,00	\$0.00	0	
1372 Devon F	91.4	89.0	90.8	89.45	90.19	50	31	89.91	-100.00	\$0.00	0	
1372 Devon F	91.4	89.0	90.8	89.32	90.01	50	31	89.75	-100.00	\$0.00	o o	
396 Ash Rd	91.5	89.1	90.9	90.9	91.18	30	12	91.01	0.12	\$15,797.95	1	
396 Ash Rd	91.5	89.1	90.9	90 94	91.43	30	12	91.14	0.25	\$17,315.52	1	
396 Ash Rd	91.5	89.1	90.9	90.78	91.36	30	12	91.01	0.12	\$15,797 95	1	
396 Ash Rd 396 Ash Rd	91.5	89.1	90.9	90,61	91.26	30	12	90.87	-100.00	\$0.00	0	
396 Ash Rd	91.5 91.5	89.1 89.1	90.9	90.36	91.08	30	12	90.65	-100.00	\$0.00	0	
396 Ash Rd	91.5	89.1	90.9	90.19	90.85	30	12	90.45	-100 00	\$0.00	0	
402 Ash Rd	91.5	89.1	90.9	91.18	91.18	30	12	90.29	-100.00	\$0.00	0	
402 Ash Rd	91.5	89.1	90.9	91 43	91.43	- 1	1	91.43	0.29 0.54	\$17,888.36 \$21,521.99		
402 Ash Rd	91.5	89.1	90.9	91.36	91.36	il	1	91.36	0.47	\$20,435.96	1	
402 Ash Rd	91.5	89.1	90.9	91.26	91.26	il	il	91.26	0.37	\$18,978.87	41	
402 Ash Fld	91.5	89.1	90.9	91.08	91.08	1	1	91.08	0.19	\$16,612.91	1	
402 Ash Rd	91.5	B9 1	90.9	90.85	90.85	1	1	90.85	-100.00	\$0.00	0	
402 Ash Rd	91.5	89.1	90.9	90.7	90.7	-1	1	90.70	-100.00	\$0.00	0	
1356 Amber Q	92	89.6	91.4	91.18	91.18	1	1	91.18	-100.00	\$0.00	0	
1356 Amber C	92 92	89.6 89.6	91.4 91.4	91.43	91.43			91.43	0.04	\$14,868.20	1	
1356 Amber C	92	89.6	91.4	91.36 91.26	91 36	1		91.36	-100.00	\$0.00	0	
1356 Amber C	92	89.6	91.4	91.26	91.26 91.08	11		91.26	-100.00	\$0.00	0	
1356 Amber C	92	89.6	91.4	90.85	90.85	41	- 1	91.08 90.85	-100.00 -100.00	\$0.00	0	
1356 Amber C	92	89.6	91.4	90.7	90.7	1	- 1	90.70	-100.00	\$0.00 \$0.00	0	
1357 Amber 0	93.3	90.9	92.7	92.88	92.95	30	4	92.89	0.20	\$16,728.00	- 1	
1357 Amber C	93.3	90.9	92.7	93.13	93.23	30	4	93.14	0.45	\$20,185.56	1	
1357 Amber Q	93.3	90.9	92.7	93.04	93.13	30	4	93.05	0.36	\$18,866.89	1	
1357 Amber G	93.3	90.9	92.7	92.95	93.03	30	4	92.96	0.27	\$17,634.36	4	
1357 Amber 0	93.3	90.9	92.7	92.83	92.89	30	4	92.84	0.15	\$16,104.72	4	
1357 Amber C	93.3	90.9	92.7	92,71	92.77	30	4	92.72	0.03	\$14,736.81	- 1	
1365 Amber C	93.5	90.9	92.7 92.9	93.01	93.03	30	4	93.01	0.32	\$18,325.87	1	
1365 Amber C	93.5	91.1	92.9	92.88	92.95	30	17	92.92	0.03	\$14,754.99	1	
1365 Amber C	93.5	91.1	92.9	93.13	93.23	30 30	17	93.19 93.09	0.30	\$17,976.79	1]	
1365 Amber C	93.5	91-1	92.9	92.95	93.03	30	17 17	93.09	0.20	\$16,748.63		
1365 Amber C	93.5	91.1	92.9	92.83	92.89	30	17	92.86	-100.00	\$15,604.39 \$0.00	0	
1365 Amber C	93.5	91.1	92.9	92.71	92.77	30	17	92.74	-100.00	\$0.00	0	
1365 Amber C	93.5	91.1	92.9	93.01	93.03	30	17	93.02	0.13	\$15,907.40	1	
					-				00	Reg	6	
										100	7	
										50	6	
										25	4	
										10	3	1
										5	2	4

Frequency	Summarized Damage Costs (S)
Reg	\$109,634.43
100	\$137,668.49
50	\$113,092.31
25	\$75,391 93
10	\$52,338.87
5	\$31,848,61
2	\$49 491 43

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
  2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
  4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
  5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
  6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangerment

Table 6
Flooding Damages Evaluation Scale Category: Site Assessment

Site	Event	WSEL	Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth (50 Year, 5%) Direct Damages	Measure Weight	Category Importance/ Significance	
	(Yr)	(m)	(No.)	(No.)	(No.)	(\$)	(ha)	(\$)	(ha)	(\$)	(ha)	(\$)	(\$)	(\$)	(\$)	(1-10)	(1-10)	1
	2	92,69	3	3	0	\$49,491	0	0	0	0	0	0	\$49,491					
	5	93.00	2	2	0	\$31,849	0	0	0	0	0	0	\$31,849					
	10	93.51	3	3	0	\$52,339	0	0	0	0	0	0	\$52,339		1			
27	25	93.64	4	4	1	\$75,392	0	0	0	0	0	0	\$75,392	\$24,645	\$449,918	4	8	32
	50	93.69	6	6	1	\$113,092	0	0	0	0	0	0	\$113,092		1			
	100	93.74	7	7	11	\$137,668	0	0	0	0	0	0	\$137,668					
	Reg	93.61	6	6	1	\$109,634	0	0	0	0	0	0	\$109,634		1			

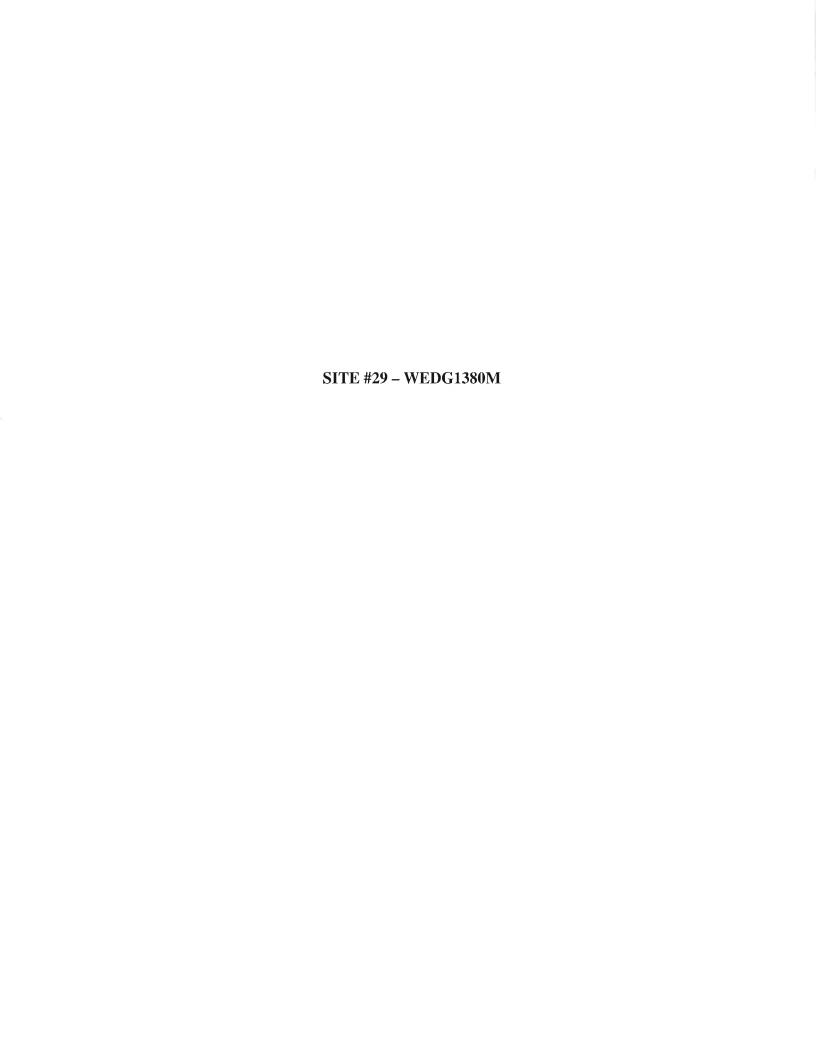
- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not
- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
- 4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
  5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

\$109,634					
Total Indirect Damage Value	Average Annual Damages 2007 Indirect Damages	Present Worth ( 50 Year, 5%) Indirect Damages	Measure Weight	Category Importance/ Significance	Product
(\$)	(\$)	(\$)	(1-10)	(1-10)	
\$7,424					
\$4,777					
\$7,851					
\$11,309	\$3,697	\$67,488	4	4	16
\$16,964					
\$20,650					
\$16,445					

_	I er e e												
Building	Finished Floor	Basement Floor	Lowest	Downstream	2-100/	Upstream 2-100/ Reg		Distance	Interpolated Property	2			
No.	Elevation	Elevation	Opening	Reg	Flood	Flood Elevations (m)	Section Distance	Distance from Downstream Section	100/ Reg Floo	d Building Flood	Damage Costs (\$)	Basement Flooding	First Floor Floodin
	(m)	(m)	(m)	Elevations	(m)	1 lood Elevations (III)		Downstream Section	Elevations (m)	Depth (m)	- "	(Yes/ No)	(Yes/ No)
1347 Devo	91,2	88.8	90,6		90.01	90.78	60	30	90.	40 -100.00	\$0,00	0	
1347 Devo	91.2	88.8	90.6		90.09	90,86	60	30	90,			o o	l
1347 Devo	91.2 91.2	88.8 88.8	90.6		89.78	90.51	60	30	90.			0	<b> </b>
1347 Deve	91.2	88.8	90.6 90.6		90.13 89.64	90.91	60	30	90.		1		
1347 Devo	91.2	88.8	90.6		90	90 36 90 76	60 60	30 30	90.		1 (2)		[
1347 Devo	91.2	88.8	90,6		89.48	90.22	60	30	90. 89.			0	
1351 Deva	90.7	88.3	90,1		90,09	90.9	50	10	90.			1	
1351 Devo	90.7	88,3	90.1		90.13	90.94	50	10	90.		\$16,761.03	1	
1351 Devo	90 7	88.3	90.1		90	90.78	50	10	90.		\$15,156,92	1	
1351 Devo	90.7 90.7	88.3 88.3	90.1 90.1		89.85 89.65	90.61	50	10	90.	207	\$0.00	0	
1351 Devo	90.7	88.3	90.1		89.45	90.36 90.19	50 50	10 10	89.	923 T		0	l,
1351 Devo	90.7	88.3	90.1		89.32	90.01	50	10	89. 89.		\$0.00 \$0.00	0	
1355 Devo	90,2	87.8	89.6		90.09	90.9	50	25	90.		\$28,192.77	1	
1355 Devo	90.2	87.8	89.6		90,13	90.94	50	25	90.		\$29,039.40	ì	
1355 Devo	90.2 90.2	87.8	89.6		90	90,78	50	25	90.		\$26,085.95	1	
1355 Devo	90.2	87.8 87.8	89.6 89.6		89.85 89.65	90,61	50	25	90.		\$23,174,33	1	
1355 Devo	90.2	87.8	89.6		89.45	90.36 90.19	50 50	25 25	90.0		\$19,621.24	1	
1355 Devo	90.2	87.8	89.6		89.32	90.01	50	25	89.0 89.0		\$17,111.80 \$15,258.16	1	
1372 Devo	91.4	89.0	90.8		90.09	90.9	50	31	90.8		\$0.00	- 0	
1372 Devo	91,4	89.0	90.8		90.13	90.94	50	31	90.6		\$0.00	ő	
1372 Devo	91.4 91.4	89.0	90.8		90	90.78	50	31	90.4		\$0.00	0	
1372 Devo	91.4	89. <b>0</b> 89. <b>0</b>	90.8		89.85 89.65	90.61	50	31	90.3		\$0.00	0	
1372 Devo	91.4	89.0	90.8		89.45	90,36 90,19	50 50	31 31	90.0	28	\$0.00	0	
1372 Devo	91.4	89.0	90.8		89.32	90.01	50	31	89.5		\$0,00 \$0.00	0	
396 Ash R	91.5	89,1	90.9		90.9	91,18	30	12	91.0		\$15,797.95	0	
396 Ash R	91.5	89.1	90.9		90.94	91.43	30	12	91.1		\$17,315.52	i	
396 Ash R	91.5 91.5	89,1	90.9		90.78	91.36	30	12	91.0		\$15,797.95	i	
396 Ash R	91.5	89_1 89_1	90.9		90.61 90.36	91.26	30	12	90.8	30	\$0.00	0	
396 Ash R	91.5	89.1	90.9		90.19	91.08 90.85	30 30	12	90.6	0.0	\$0.00	0	
396 Ash R	91.5	89.1	90.9		90.01	90.7	30	12	90.4		\$0.00 \$0.00	0	
402 Ash R	91.5	89,1	90.9		91.18	91.18	1	1	91.1		\$17,888.36	1	
402 Ash Fi	91.5	89.1	90.9		91.43	91.43	1	1	91.4		\$21,521.99	1	
402 Ash R	91.5 91.5	89.1 89.1	90.9		91.36	91,36		1	91.3		\$20,435.96	1	
402 Ash Fi	91.5	89.1	90.9		91.26 91.08	91.26 91.08	1	]	91.2	334	\$18,978.87	1	
402 Ash R	91.5	89.1	90.9		90.85	90.85	1	- 1	91.0		\$16,612,91	1	
402 Ash R	91.5	89,1	90.9		90.7	90.7	i	1	90.7		\$0.00 \$0.00	0	
1356 Amb	92	89.6	91.4		91.18	91,18	1	1	91.1		\$0.00	0	
1356 Amb	92	89.6	91.4		91.43	91.43	1	1	91.4		\$14,868.20	1	
1356 Amb	92 92	89.6 89.6	91.4		91.36 91.26	91,36		3	91.3		\$0.00	0	
1356 Amb	92	89.6	91.4		91.08	91.26 91.08	- 3	]	91.2		\$0.00	0	
1356 Amb	92	89.6	91.4		90.85	90.85	ᆒ		91.0 90.8		\$0.00 \$0.00	0	
1356 Amb	92	89.6	91.4		90,7	90.7		i	90.7		\$0.00	0	
1357 Amb	93.3	90.9	92.7		92,88	92.95	30	4	92.8	9 0.20	\$16,728.00	1	
1357 Amb	93.3 93.3	90,9	92.7		93.13	93.23	30	4	93,1	0.45	\$20,185.56	1	
1357 Ambi	93.3	90.9	92.7 92.7		93.04 92.95	93.13 93.03	30 30	4	93.0		\$18,866.89	1	
1357 Amb	93.3	90.9	92.7		92.83	92.89	30	4	92.9 92.8	81	\$17,634.36		
1357 Amb	93.3	90.9	92,7		92,71	92.77	30	4	92.7		\$16,104.72 \$14,736.81	1	
1357 Amb	93.3	90.9	92.7		93,01	93.03	30	4	93.0		\$18,325.87		
1365 Amb	93.5	91.1	92.9		92.88	92,95	30	17	92.9	0.03	\$14,754.99	1	
1365 Amb	93.5 93.5	91.1 91.1	92.9 92.9		93.13	93.23	30	17	93.1		\$17,976.79	1	
1365 Amb	93.5	91.1	92.9		93.04 92.95	93.13 93.03	30 30	17 17	93.0	27 7.8	\$16,748.63	1	
1365 Amb	93.5	91.1	92.9		92.83	92.89	30	17	93.0 92.8		\$15,604.39	1	
1365 Amb	93.5	91.1	92.9		92.71	92.77	30	17	92.7		\$0.00 \$0.00	0	
1365 Amb	93.5	91.1	92.9		93.01	93.03	30	17	93.0		\$15,907.40	1	
											Reg	6	
											100	7	
											50	6	
											25 10	4 3	
											5	2	
											2	3	

Frequency	Summarized Damage Costs (\$)
Reg	\$109,634.43
100	\$137,668.49
50	\$113,092.31
25	\$75,391,93
10	\$52,338.87
5	\$31,848_61
2	\$49,491.43

- Determine flooding elevations for all storm events at buildings that potentially flood
  Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/Determine basement floor elevation by substracting 2.44m from the first floor elevation
  Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential lar
  Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
  Determine flooding damages for each return period based on the flooding depths and damage curve equations

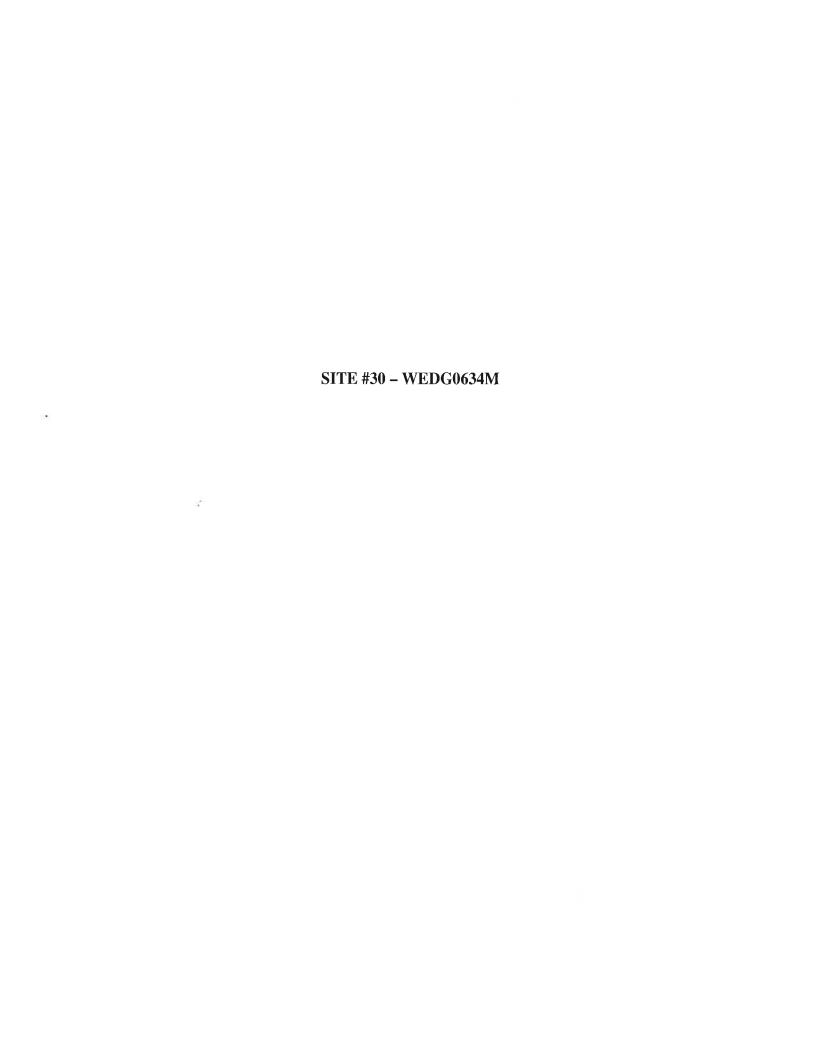


REGULATORY FLOODLINE

TOWNWIDE FLOODING STUDY TOWN OF OAKVILLE SITE # 29 - WEDG1380M WEDGEWOOD CREEK

	Р
	D
HILIPS	S
NGINEERING	F

106026 Project No. January 2008 Date 1:750 Scale Figure No. 29





SITE # 30 - WEDG0634M WEDGEWOOD CREEK

REGULATORY FLOODLINE

Figure No.

Date

Scale

January 2008

1:1,000

30

## Site #30 (WEDG0634M) Implementation Program

## Recommended Management Approach/Project Scope:

Flood proofing of homes not flooded on all sides

### Appropriate Lead for Undertaking:

• Timing and phasing as per Town of Oakville Capital Works Program based on priority ranking established herein.

### Governing Protocol Legislation:

- Town of Oakville's Policies and protocols
- Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
- Ministry of Natural Resources Lakes and Rivers Act

## Approval Requirements:

- Town of Oakville
- Conservation Halton Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Permit

## Need for, and Scope of Follow-Up Assessment/Analysis:

- Detailed topographic survey of area
- Hydraulic modeling refinement
- Approval process with private land owners

### Suggested Timing, Need for Phasing:

 Timing of project dependant on Capital Works Program budget and priority of project within the Program.

### Possible Implementation Issues:

Private land owners consent to proposed flood proofing

## Possible Monitoring Requirements:

• N/A

## Need for Maintenance:

N/A

# Potential Interface with Other Town/Agency Programs:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Potential opportunities with Town's Creek Erosion Study and road work
- Potential projects already identified by Conservation Halton

## Other Funding Opportunities:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Others

# Site #30 (WEDG0634M) Specific Flood Management Alternative Assessment

## Data/Information:

## Flooding mechanisms:

- Wedgewood Drive crossing 4.0 m by 1.7 m arch
- Floodplain capacity is less than the 5 year storm @ 7.70 m<sup>3</sup>/s. Regional is 47.90 m<sup>3</sup>/s

### Screened Alternatives:

- Crossing upgrades based on land availability do not result in significant hydraulic improvements
- Floodplain/channel upgrades not practical due to private property issues and natural vegetation
- Flood-proofing practical for 3 out of 5 homes
- Acquisition 4 homes (costly)
- Regulate

# Preferred Management Approach:

- Flood-proof for homes not flooded on all sides; topographic survey required to verify building elevations and flood proofing possible.
- Regulate

# Potential Linkage to Adjacent Sites:

• Site 31

					ible 7 Evaluation Resul	ts				
			Cate	gory Evaluation Pro	oducts					
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products
30	0.2	4.0	1.3	0.1	2.8	1.3	40.0	64.0	32.0	145.6

			-								F	Road F	Floodi	_	able 4 ood Cr		Evalu	ation																	
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation		1	Flood	Elevat	ions (n	1)	ı —		Ro	ad Flo	oding D	epth (m	1)			FI	ow Vel	ocities	s (m/s)			Sto	rm Eve	nt Freq	uency l	Modifie	rs	Storm Event Flooding Starts/ or Criteria Not Met	Storm Event Frequency Modifier Selected	Evaluation Scale Category Importance/ Significance	Product (Measure Weighting * Storm
		(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5	10	25	50	100 I	Reg	2	5	10	25	50	100 F	Reg	2	5 1	0 25	50	100	Reg	(2-100, Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significance
30	Design Flood Criteria	Arterial	10	82.40	82.6	82,7	82.8	82,8	82,9	82,9	83,0	0,0	0.3	0.4	0.4	0.5	0.5	0.6	0.0	0.7	0.8	0.9	1.0	1.0	1.1	1 0	4 0	2 0.0	8 0.04	0.02	0.01	Arterial / 1:100 - Reg	0.01	2	0.16
30	Private Vehicle	EMS Route	10	82.40						1									- 1				1.0		- 1	- 1							0.1	5	4
30	Emergency Vehicle	EMS Route	10	82.40	82.6	82.7	82.8	82.8	82.9	82.9	83.0	0.0	0.3	0.4	0_4	0.5	0,5	0,6	0.0	0.7	0,8	0.9	1.0	1.0	1.1	1   c	,4 0	2 0,0	8 0.04	0.02	0.01	None	0.0	6	0
30	Private Vehicle Acess to Facilities	Partial	5	82,40									1						- 1				1.0									Arterial / 1:100 - Reg	0.01	3	0.12
30	Emergency Vehicle Access to Facilities	No	5	82,40	82,6	82.7	82.8	82.8	82.9	82.9	83.0	0.0	0.3	0.4	0.4	0.5	0.5	0.6	0.0	0.7	0.8	0.9	1.0	1.0	1.1	1 0	.4 0.	2 0.0	8 0.04	0.02	0.01	25-yr	0.1	7	2.8
30	Private Vehicle Driveway Access (Multiuser)	Low Vehicle Usage	4						1						0.4				- 1			0.9	- 10	1.0	1:1	1 0	.4 0		B 0.04	1		_	0,1	4	1.28

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

																		Threa	t to Life F	Table 5 lood Criteri	a Evaluatio	n																					
.  -			Site Downs	ream Flood E	levations (m)					Reside	ntial Units Fig	oded (#)				Industr	al Area (ha)			Comm	erclal Area (	ne)		Inst	litulional (h	a)	t,ar		sities (pers/ h unit)	1A Of	Pe	ople Enden	ngered		Stor	m Event	Frequency	Modifiers				Composite	T
ilte No	2	- 5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5 10	25 5	50 100	Reg 2	5 10	25 50	100 Reg	g 2	5 10	25	50 100	Reg Re	as Ind	Com Ins	1H 2	5	0 25	50 1	00 Reg	2 5	10	25 5	0 100	Pec	ormalized No. of opic Using Storm luitipliers	Evaluation Scale Measure Weighting (1- 10)	Calegory Importance/ Significance (1-10 (7 - Day Usage) (10 - Day and Nigl Usage)	D) Pr
30	82,57	82.63	82 66	82 76	62 92	83 03	B3 11	t	2	3	345	6	6	7	0	0 0	D	0 0	0 0	0 0	0 0	0 0	0	0 0	0	0 0	0 3	125	90 40	3	6	12	18	8 21	50 20	10	4 :	t (	0.4	470.4	í	10	+

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)

  2 Determine flooding conditions that results in life endangerment (separate spreadsheet direct damages). Note that for residential units, life endagerment has been included if the basement has been predicted to flood.

  3 Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)

  4 Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered

  5 Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm

  6 Apply adjustment factor (Value of Step 5 divided by 10)

- 7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

r												
1	Finished	Basement		Downstream	Upstream 2		Distance	Interpolated				
	Floor	Floor	Lowest	2-100/ Reg	100/ Reg	Section	from	Property 2- 100/ Reg	Building	Damage	Basement	First Floor
Building No.	Elevation	Elevation	Opening	Flood	Flood	Distance	Downstream	Flood	Flood Depth	Costs	Flooding	Flooding
	(m)	(m)	(m)	Elevations	Elevations	Distance	Section	Elevations	(m)	(\$)	(Yes/ No)	(Yes/ No)
	(,	(,		(m)	(m)		Section	(m)				
200 Wedgewo	83.4	81.0	82,8	83,11	83.69	50	6		0.39	\$19,256.03	1	
200 Wedgewo	83.4	81.0	82.8	83,03	83,61	50	6	83,10	0.31	\$18,149.59	1	
200 Wedgewo	83.4	81.0	82.8	82,92	83,49	50	6	82.99	0.20	\$16,716.45	1	
200 Wedgewd	83.4	81.0	82.8	82.76	83,35	50	6	82,83	0.04	\$14,877.01	1	
200 Wedgewo	83.4	81.0	82,8	82.66	83.11	50	6	82,71	-100.00	\$0.00	0	
200 Wedgewd	83.4	81.0	82,8	82,63	82.96	50	6	82,67	-100.00	\$0.00	0	
200 Wedgewo	83.4	81.0	82.8	82.57	82.81	.50	6	82.60	-100.00	\$0.00	0	
208 Wedgewo	83.3	80.9	82.7	83.11	83.69	50	5	83.17	0.48	\$20,557.25	1	
208 Wedgewd	83.3	80.9	82.7	83.03	83,61	50	5	83.09	0.40	\$19,376.05	1	
208 Wedgewd	83.3	80.9	82.7	82.92	83.49	50	5	82.98	0.29	\$17,848.70	1	
208 Wedgewd	83.3	80.9	82.7	82.76	83,35	50	5	82.82	0.13	\$15,879,97	1	
208 Wedgewd	83.3	80.9	82.7	82,66	83.11	50	5	82.71	0.01	\$14,595.78	4	
208 Wedgewd	83.3	80.9	82.7	82.63	82,96	50	5	82.66	-100.00	\$0,00	0	
208 Wedgewd	83.3	80.9	82.7	82.57	82,81	50	5	82.59	-100.00	\$0.00	0	9
216 Wedgewo	84.3	81,9	83.7	83.69	83.76	50	8	83.70	0.01	\$14,554.81	1	
216 Wedgewd	84.3	81,9	83.7	83.61	83,68	50	8	83.62	-100.00	\$0.00	0	
216 Wedgewo 216 Wedgewo	84.3	81.9	83.7	83.49	83.56	50	8	83.50	-100.00	\$0.00	0	1
216 Wedgewo	84.3	81.9	83.7	83.35	83.43	50	8	83.36	-100.00	\$0.00	0	
216 Wedgewo	84.3 84.3	81.9 81.9	83.7	83.11	83.2	50	8	83.12	-100.00	\$0,00	0	
216 Wedgewo	84.3	81.9	83.7 83.7	82.96 82.81	83.05 82.9	50	8	82.97	-100.00	\$0.00	0	1
230 Alscot Dr	83.2	80.8	82.6	83.76	83.76	50	8	82.82	-100.00	\$0.00	0	1
230 Alscot Dr	83.2	8.08	82.6	83.68	83.68	1		83.76 83.68	1,17	\$34,297.96	1	
230 Alscot Dr	83.2	80.8	82.6	83.56	83.56	1		83.56	1.09 0.97	\$32,327.23 \$29,581.41		1
230 Alscot Dr	83.2	80.8	82.6	83.43	83.43	1	,	83.43	0.97	\$26,869.32		1
230 Alscot Dr	83.2	80.8	82.6	83.2	83.2	1	1	83.20	0.61	\$22,665.73	4	
230 Alscot Dr	83.2	80.8	82.6	83.05	83.05	1	1	83.05	0.46	\$20,285.35	4	
230 Alscot Dr	83.2	80.8	82.6	82.9	82.9	1	l i	82.90	0.31	\$18,154.96	4	
236 Alscot Dr	84.1	81.7	83.5	83.7	83.7	1	1	83.70	0.21	\$16,860.51	54	
236 Alscot Dr	84.1	81.7	83.5	83.62	83.62	1	1	83.62	0.13	\$15,891,72	- 4	
236 Alscot Dr	84.1	81.7	83.5	83,51	83.51	1	1	83.51	0.02	\$14,649.86	- 1	1
236 Alscot Dr	84.1	81.7	83.5	83.38	83,38	1	1	83.38	-100.00	\$0.00	0	
236 Alscot Dr	84.1	81.7	83.5	83.15	83.15	1	1	83.15	-100.00	\$0.00	O	
236 Alscot Dr	84.1	81.7	83.5	83.02	83.02	1	1	83.02	-100.00	\$0,00	0	
236 Alscot Dr	84_1	81.7	83.5	82.86	82.86	1	1	82.86	-100.00	\$0.00	0	
244 Alscot Dr	84.3	81.9	83.7	84.36	84.36	1	1	84,36	0.67	\$23,694.34	1	
244 Alscot Dr	84.3	81.9	83.7	84.35	84.35	1	1	84.35	0.66	\$23,519.71	1	
244 Alscot Dr	84.3	81.9	83.7	84.22	84.22	1	1	84.22	0.53	\$21,363.37	1	3
244 Alscot Dr 244 Alscot Dr	84.3	81.9	83.7	84.1	84.1	1	1	84.10	0.41	\$19,548.80	1	
244 Alscot Dr	84.3	81.9	83.7	83.94	83.94	1	1	83.94	0.25	\$17,366,83	1	
244 Alscot Dr	84.3 84.3	81.9 81.9	83.7	83.82	83.82	1	1	83.82	0.13	\$15,891.72	1	
241 Trelawn A	85.3	82.9	83.7 84.7	83.67	83.67	1	1	83.67	-100.00	\$0.00	0	
241 Trelawn A	85.3	82.9	84.7	84.93 84.84	84.93 84.84	3	]	84.93	0,24	\$17,238.84	1	
241 Trelawn A	85.3	82.9	84.7	84.74	84.74		1	84.84	0.15	\$16,128.57	31	1
241 Trelawn A	85.3	82.9	84.7	84.62	84.62	4		84.74 84.62	0.05 -100.00	\$14,978.59	1	
241 Trelawn A	85.3	82.9	84.7	84.44	84.44	12	l i	84.44	-100.00	\$0.00 \$0.00	0	
241 Trelawn A	85.3	82.9	84.7	84.3	84.3		1	84.30	-100.00	\$0.00	0	
241 Trelawn A	85.3	82.9	84.7	84 14	84.14	4	1	84.14	-100.00	\$0.00	0	
1					01114			54.14	100.00	Reg	7	
										100	6	1
										50	6	
										25	4	
										10	3	

requency	Summarized Damage
	Costs (\$)
Reg	\$146,459,73
100	\$125,392.87
50	\$115,138,39
25	\$77,175.09
10	\$54,628.34
5	\$36,177.07
2	\$18,154,96
TAL=	\$573,126.46

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangered.

## Table 6 Flooding Damages Evaluation Scale Category: Site Assessment

Site	Event		Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth ( 50 Year, 5%) Direct Damages	Measure Weight	Category Importance/ Significance	
	(Yr)	(m)	(No.)	(No.)	(No.)	(\$)	(ha)	(\$)	(ha)	(S)	(ha)	(S)	(S)	(\$)	(S)	(1-10)	(1-10)	
	2	92.69	7	7		583,228	0	0	0	0	0	0	583,226					
	- 5	93.00	7	7	2	\$120,582	.0	0	o	p	0	0	\$120,582					
	10	93.51	7	7	2	\$130,498	0	0	ő	0	0	0	\$130,496					
30	25	93.64	7	2	2	\$164,761	0	0	0	0	0	0	\$164,761	\$59,457	\$1,085,451	a	8	64
	50	93.69	- 6	6	- 4	\$182,122	. 0	0	0	0	o	0	5182,122		1			
	100	93.74	6	6	6	\$198,409	0	0	0	0	0	o	5198,409					
	Reg	93.61	4	4	6	\$208,890	0	0	0	0	0	0	\$208,890					
													Total Indirect Damage Value	Average Annual Damages 2007 Indirect Damages	Present Worth (50 Year, 5%) Indirect	Measure Weight	Category Importance/ Significance	

#### **Evaluation Process**

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not

- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
  4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
  5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

Building	Finished Floor	Basement Floor	Lowest Opening	Downstream Reg	2-100/ Flood	Upstream 2-100/ Reg	0	Dislance Irom	Interpolated Pro		Building Flood		Basement Flooding	First Floor Floodin
No	Elevation (m)	Elevation (m)	(m)	Elevations	(m)	Flood Elevations (m)	Section Distance	Downstream Section	100/ Reg Elevations	Flood (m)	Depth (m)	Damage Costs (S)	(Yes/ No)	(Yes/ No)
00 Wedg	62.92	80.5	82,3		83 11	63,69	50	(6		83.1B	0.87	\$27,464.11	1	
00 Wedg	82 92 82 92	80.5			83 03	83,61	50	6		83.10	0.79	\$25,886.05	i	
pbeW 00 pbeW 00	82 92	80.5 80.5			82 92	83 49	50	6		82.99	0.68	\$23,842.02	1	
00 Wedg	82 92	80.5	82 3 82 3		82 70	83,35	50	6		82.83	0.52	\$21,218.49	1	
00 Wedg	82 92	80.5			82 66 82 63	83 11 82 96	50 50	6	1	82.71	0.40	519,462 23		
00 Wedg	82.92	80.5	82.3		82 57	82 81	50	6		82.67	0.36	\$18,833 42	1	
08 Wedg	82.82	80.4	82.2		83.11	83 69	50	6		82 60 83 17	0.29	\$17,872.48	1	
08 Wedi	82.82	80.4	82.2		83.03	83.61	50	5		83.09	0.96 0.88	\$29,319 99 \$27,635 29		
08 Wedg	82.82	80 4	82 2		82.92	83 49	50	5		82.98	0.77	\$27,635.29	3	
08 Wedgi	82.82	80.4	82 2		82.76	83 35	50	5		82.82	0.61	\$22,648.97		
08 Wedg	82.82	80.4	82 2		82 66	83,11	50	5		82.71	0.49	\$20,817.39		
08 Wedge	82.82	80.4	82 2		82 63	82,96	50	- 5		82.66	0.45	\$20,180.59	1	
08 Wedge	82.82	80.4	82.2		82.57	82.81	50			82.59	0.38	\$19,176.43		
16 Wedge	83 82	81.4	83.2		83 69	83.76	50	8		83.70	0,49	\$20,758.95	1	
16 Wedge 16 Wedge	83.82 83.82	81.4 81.4	83.2 83.2		83 61 83 49	83.68	50		1	83 62	0.41	\$19,566 16		
16 Wedg	83 82	81.4	83.2		83 35	83.56 83.43	50	8		83.50	0.29	\$17,904.24	1	
16 Wedg	83 82	81.4	83.2		83.11	83.43	50 50	8		83.36	0_15	\$16,162.01	1	
16 Wedg	83 82	81.4	83.2		82 96	83.05	50		1	83.12	-100 00	S0,00	0	
16 Wedg	83.82	81.4	83.2		82.81	82.9	50		1	82.97 82.82	-100 00 -100 00	\$0.00	0	
30 Aiscol	82.72	80.3	82.1		83.76	83.76	1	- 1		83.76	1.65	\$0.00 \$48,917.83		
30 Alscot	82 72	80.3	82.1		83.68	83.68	i	i		83.68	1.57	\$46,107.06		
30 Alscol	82.72	80.3	82.1		83.56	83.56	1	1		83.56	1.45	\$42,190 79	1	
30 Alscol	82.72	80.3	82 1		83.43	83.43	1	1		83 43	1.32	\$38,322.65	i	
30 Alscot	82.72	80.3	82.1		83.2	83.2	1	1		83 20	1 09	\$32,327.23	1	
30 Alscot	82 72	80.3	82.1		83.05	83.05	1	1		83.05	0,94	\$28,932.20	1	
30 Alscot	82.72	80.3	82 1		82.9	82.9	1	1		82.90	0.79	\$25,893.71	t	ľ.
36 Alscot	83.62	81.2	83.0		83.7 83.62	83.7 83.62	- 1	1		83.70	0.69	\$24,047 47	1	
36 Alscot	83.62	81.2	83.0		83.51	83.51				83.62	0,61	\$22,665 73	1	
36 Alscot	83 62	81.2	83.0		83.38	83.38	- 1	1		83.51 83.38	0.50	\$20,894.52		
36 Alscot	83.62	81.2	83.0		83.15	83,15				63.15	0.37	S18,978 87 S16,009.70	1	
36 Alscot	83.62	81.2	83.0		83.02	83.02	1	1		83.02	0.01	\$14,541.90		
36 Alscot	83.62	81.2	83.0		82,86	82.88	1	1		82.86	-100 00	\$0.00	à	
44 Alscot	83 82	81.4	83.2		84,35	84 38	- 1	1		84.36	1 15	\$33,794.29	1	
44 Alscol	83 82	81.4	83.2		84 35	84.35	31	1		84.35	1.14	\$33,545.24	31	
44 Alscot	83.82	81.4	83.2		84 22	84 22	(3)	1		84.22	1,01	\$30,469.74	1	
44 Alscol	83 82 83 82	61.4 61.4	83.2 83.2		84 1	84.1	3	í		84 10	D.89	\$27,881.68	i i	
44 Alsco	83.82	81.4	83.2		83.94 83.82	83.94	31	- 3		83 94	0,73	\$24,769.62	1	
44 Alscol	83.82	81.4	83.2		83.67	83 82 83 67	3	1		63.82	0.61	\$22,665 73	1	
41 Trelaw	84.82	82.4	842		84.93	84.93	- 1			83 67	0.46	\$20,285,35	1	
11 Trelaw	84.82	82.4	84.2		84.84	84.84	i il	1		84 B4	0.72 0.63	\$24,587.08	1	
11 Trelaw	84.82	82.4	84.2		84.74	84.74	i	1		84.74	0.53	\$23,003.54 \$21,363.37	11	
11 Trelaw	84.82	82.4	84.2		84.62	84.62	i	i		84.62	0.41	\$21,363.37	1	
11 Trelay	84.82	82.4	84 2		84.44	84.44	1	i		84 44	0 23	S17,111 80		
41 Trelaw	84.82	82.4	84.2		84.3	84.3	3	1		84.30	0.09	S15,428 40	1	
41 Trelaw	84.82	82.4	84.2		84 14	84.14	1	1		84 14	-100 00	\$0.00	o	
												Reg	7	
												100	7	
												50	7	
												25	7	
												10	6	
												5	6	

\$12,484				
\$18,087			1	
\$19,575				
\$24,714	\$8,919	\$162,818	8	34
\$27,318				
\$29,761			1	
\$31,333				

Damages

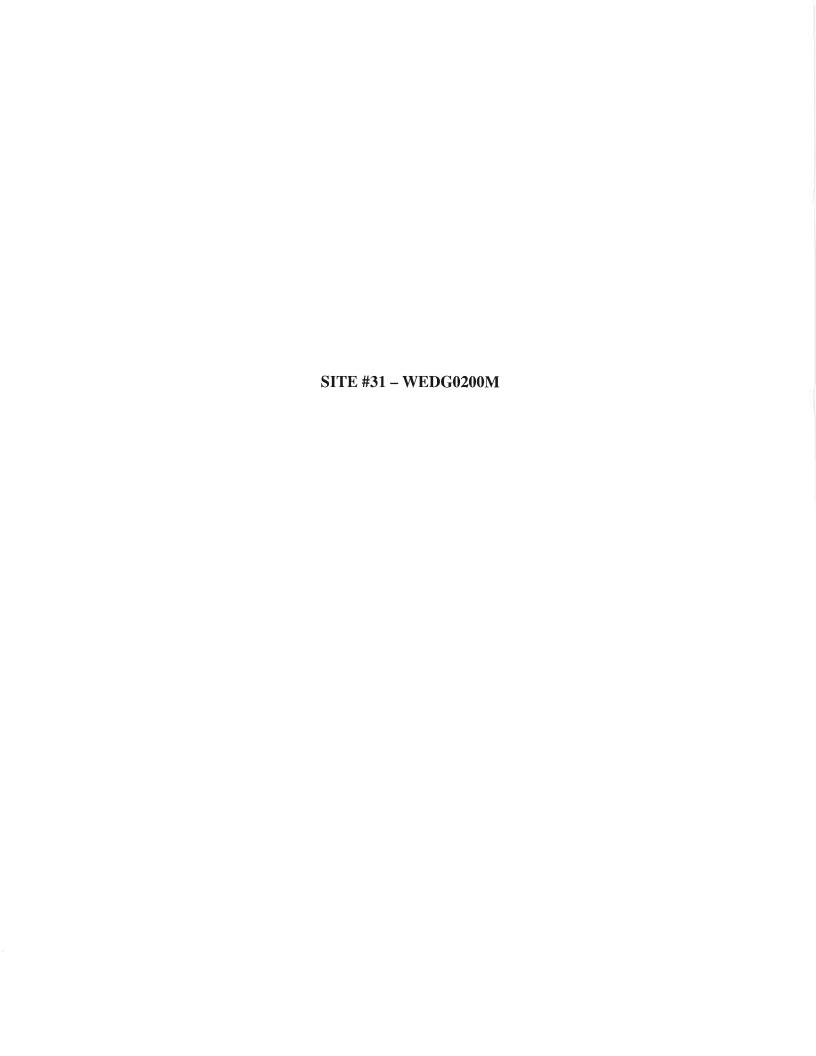
(\$)

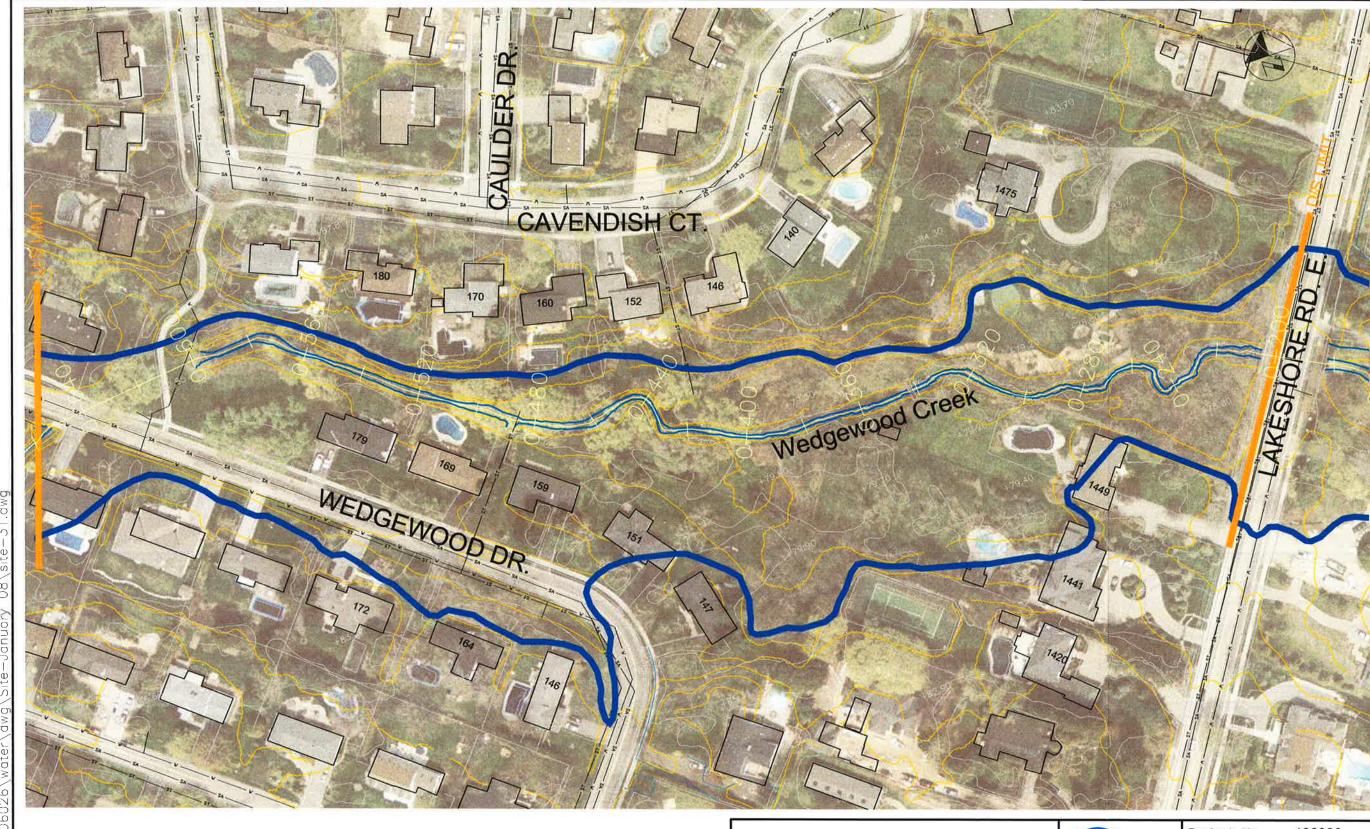
(1-10)

**(S)** 

Frequency	Damage Costs (\$)
Reg	\$208,889.74
100	\$198,409.06
50	\$182,121.59
25	\$164,761 46
10	\$130,497 97
5	\$120,582.23
	\$83,227 97
TOTAL=	\$1,088,490 02

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine flooding damages for each return period based on the flooding depths and damage curve equations





LEGEND:

REGULATORY FLOODLINE

TOWNWIDE FLOODING STUDY TOWN OF OAKVILLE SITE # 31 - WEDG0200M WEDGEWOOD CREEK

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	r
HILIPS	ŀ
ENGINEERING	l

Project No.	106026
Date	January 2008
Scale	1:1,250
Figure No.	31

	Site #31 (WEDG0200M) Implementation Program
Reco	mmended Management Approach/Project Scope:
• ]	Regulate – maintain existing conditions
•	
Appı	opriate Lead for Undertaking:
•	N/A
Gove	rning Protocol Legislation:
•	Town of Oakville's Policies and protocols
•	Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
•	Ministry of Natural Resources Lakes and Rivers Act
•	Department of Fisheries and Oceans Fisheries Act
Appr	oval Requirements:
•	N/A
Need	for, and Scope of Follow-Up Assessment/Analysis:
•	N/A
Sugg	ested Timing, Need for Phasing:
•	N/A
Poss	ble Implementation Issues:
•	N/A
Poss	ble Monitoring Requirements:
•	N/A
Need	for Maintenance:
•	Typical creek and crossing maintenance
Pote	ntial Interface with Other Town/Agency Programs:
•	N/A
Othe	r Funding Opportunities:

N/A

## Site #31 (WEDG0200M) Specific Flood Management Alternative Assessment

### Data/Information:

### Flooding mechanisms:

- Lakeshore Road East crossing 3.9 m by 1.2 m box culvert
- Channel capacity at Lakeshore Road both upstream and downstream
- Channel floodplain capacity near Wedgewood Drive
- Encroachment
- Spill from Wedgewood Drive crossing (Site 30)

#### Screened Alternatives:

- Upgrades to Lakeshore Road East crossing no affect on flooding of homes located on Wedgewood Drive
- Site 30 potential improvements
- Channel/floodplain improvements not practical due to private property, existing vegetation and limited hydraulic improvements.
- Flood-proofing not practical as homes are flooded on all sides
- Acquisition 4 homes (costly)
- Regulate

### Preferred Management Approach:

Regulate

# Potential Linkage to Adjacent Sites:

• Site 30

					ble 7 Evaluation Resul	ts				
			Cater	gory Evaluation Pro	oducts					
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products
31	0.2	1.0	0.5	0.3	1.4	0.5	40.0	16.0	8.0	67.8

														_	able 4																					
											B	oad F	loodi	ng Flo	od Cı	riteria	Evalu	uation																	E.	
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation			Flood	l Eleva	ions (n	1)			Roa	ad Floo	ding D	epth (n	n)			Fle	ow Velo	ocitie	s (m/s)			Sto	rm Ev	ent Fre	quenc	y Mod	ifiers	Floo	Storm Event oding Starts/ or iteria Not Met	Storm Event Frequency Modifier Selected	Evaluation Scale Category Importance/ Significance	Product (Measure Weighting * Storm
		(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5	10	25	50	100 F	Reg	2	5	10 2	25	50	100 F	Reg	(2-100, Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significance
31	Design Flood Criteria	Arlerial	10	79,90	78.4	79.2	80.1	80.2	80.3	80.3	80.4	0,0	0.0	0.2	0,3	0.4	0,4	0.5	0.0	0,5	0.7	0.8	0.8	0.9	0.9	1 (	0.4	0.2 0	08 0	.04	0.02	0.01 Arte	rial / 1:100 - Reg	0.01	2	0.2
31	Private Vehicle	EMS Route	10	79,90	78,4	79,2	80.1	80,2	80,3	80,3	80.4	0.0	0.0	0.2	0,3	0,4	0.4	0,5	0.0	0,5	0.7	8,0	8,0	0.9	0.9	1 (	0.4	0,2 0	.08 0	,04	0.02	0.01	100-yr	0.02	5	1
31	Emergency Vehicle	EMS Route	10	79.90	78.4	79.2	80.1	80,2	80,3	80,3	80.4	0.0	0,0	0.2	0,3	0,4	0,4	0,5	0.0	0,5	0.7	0.8	0.8	0.9	0.9	1 0	.4	0.2	.08 0	.04	0.02	0.01	None	0.0	6	0
31	Private Vehicle Acess to Facilities	Yes	10	79.90	78,4	79,2	80.1	80,2	80.3	80,3	80.4	0.0	0,0	0.2	0.3	0.4	0.4	0.5	0,0	0,5	0.7	0.8	8.0	0.9	0.9	1 0	.4 C	0.2	.08 0	.04	0.02	0.01 Arte	rial / 1:100 - Reg	0.01	3	0.3
31	Emergency Vehicle Access to Facilities	Yes	10	79.90	78,4	79.2	80_1	80.2	80,3	80,3	80.4	0,0	0.0	0.2	0.3	0.4	0.4	0,5	0.0	0.5	0.7	0.8	0.8	0.9	0.9	1 0	.4 0	0.2	.08 0	.04	0.02	0.01	100-yr	0.02	7	1.4
31	Private Vehicle Driveway Access (Multiuser)	Medium Vehicle Usage	6	79.90	78.4	79.2	80.1	80.2	80.3	80.3	80.4	0.0	0.0	0.2	0.3	0.4	0.4	0.5	0.0	0.5	0.7	0.8	0.8	0.9	0.9	1 0	.4 0	0.2 0.	.08 0	.04	0.02	0.01	100-yr	0.02	4	0.5

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

								·										Threat		Table 5 lood Crite	eria Evalu	uation																					
			Site Downs	ream Flood E	evations (m)					Reside	ntial Units Fig	oded (#)				Industrial	Area (ha)			Con	mmercial A	rea (ha)			Instituti	onal (ha)		Land Us	se Densitie /unit	s (pers/ ha c	ж	Peop	le Endang	gered		Storm Ev	ent Frequ	ncy Modifier	6			Composite	T
e No	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5 10	25 5	0 100 F	Reg 2	5 1	10 25	50 100	) Reg	2 5	10 :	25 50	100 Re	g Res	Ind Co	om Instit	2	5 10	25	50 10	0 Reg	2 5	10 25	50 100	Reg Pe	iormalized No. of aople Using Storm Multipliers	Evaluation Scale Measure Weighting (1- 10)	Category Importance/ Significance (1-10 (7 - Day Usage) (10 - Day and Nigi Usage)	10) P
1	79 15	79 62	80 14	80 28	80,35	80 41	60 45	0	0	2	2	2	3	3	0	0 0	0 0	0	0 0	0 1	0 0	0 0	0	0 0	0	0 0	0 0	3	125 9	0 40	0	0 6	6	6 9	9 .	50 20	10 4	2 1	0,4	108 6	4	10	+

- Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)

  Determine flooding conditions that results in life endangerment (separate spreadsheet direct damages). Note that for residential units, life endagerment has been included if the basement has been predicted to flood.

  Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)

  Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered

- 5 Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm
- 6 Apply adjustment factor (Value of Step 5 divided by 10)
- 7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

Building No.	Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream 2-100/ Reg Flood Elevations (m)	Upstream 2 100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floo Flooding (Yes/ No
180 Lakeshor	81.2	78.8	80.6	80,45	80.45	1	1	80.45	-100.00	\$0.00	0	
180 Lakeshor	81.2	78,8	80.6	80.41	80,41	1	1	80.41	-100.00	\$0.00	ő	
180 Lakeshor	81.2	78.8	80.6	80.35	80.35	1	1	80.35	-100.00	\$0.00	o	
180 Lakeshor	81.2	78.8	80.6	80.28	80.28	1	1	80,28	-100.00	\$0.00	o	
180 Lakeshor	81.2	78.8	80.6	80.14	80_14	1	1	80.14	-100.00	\$0.00	0	1
180 Lakeshor	81,2	78.8	80.6	79.62	79.62	1	1	79.62	-100.00	\$0.00	o	
180 Lakeshor	81.2	78.8	80.6	79.15	79.15	1	. 1	79.15	-100.00	\$0.00	0	
180 Lakeshor	81.3	78.9	80.7	80.45	80.5	40	10	80.46	-100.00	\$0.00	0	
180 Lakeshor	81.3	78.9	80.7	80_41	80.46	40	10	80,42	-100.00	\$0.00	o	
180 Lakeshor	81.3	78.9	80.7	80.35	80.4	40	10	80.36	-100.00	\$0.00	0	
180 Lakeshor	81.3	78.9	80.7	80.28	80.32	40	10	80.29	-100.00	\$0.00	0	
180 Lakeshor	81.3	78.9	80.7	80.14	80,17	40	10	80.15	-100.00	\$0.00	0	
180 Lakeshor	81.3	78.9	80.7	79,62	79.67	40	10	79.63	-100.00	\$0.00	0	
180 Lakeshor	81.3	78.9	80.7	79.15	79.38	40	10	79,21	-100.00	\$0.00	0	
47 Wedgewo	82.5	80.1	81.9	80.5	80.61	50	8	80.52	-100.00	\$0.00	0	
47 Wedgewo	82.5	80.1	81.9	80.46	80.57	50	8	80.48	-100.00	\$0.00	o	
47 Wedgewo	82.5	80.1	81.9	80.39	80.5	50	8	80.41	-100.00	\$0.00	o	
47 Wedgewo	82.5	80.1	81.9	80.31	80.43	50	8	80.33	-100.00	\$0.00	o	
47 Wedgewo	82.5	80.1	81.9	80.16	80.3	50	8	80.18	-100.00	\$0.00	o	
47 Wedgewd	82.5	80.1	81.9	79.72	80.22	50	8	79.80	-100.00	\$0.00	0	
47 Wedgewo	82.5	80.1	81_9	79.64	80.12	50	8	79.72	-100.00	\$0.00	0	
51 Wedgewd	82.4	80.0	81.8	80.61	81.4	40	7	80.75	-100.00	\$0.00	0	
51 Wedgewo	82.4	80.0	81.8	80.57	81.35	40	7	80.71	-100.00	\$0.00	0	
51 Wedgewo	82.4	80.0	81.8	80.5	81.29	40	7	80.64	-100.00	\$0.00	o	
51 Wedgewo	82.4	80.0	81.8	80.43	81.23	40	7	80.57	-100.00	\$0.00	0	
51 Wedgewd	82.4	80.0	81.8	80.3	81.12	40	7	80.44	-100.00	\$0.00	o	
51 Wedgewd	82.4	80.0	81.8	80.22	81.04	40	7	80.36	-100.00	\$0.00	o	
51 Wedgewo	82.4	80.0	81.8	80,12	80.95	40	7	80.27	-100.00	\$0.00	o o	
59 Wedgewo	81.9	79.5	81.3	81.4	81.4	1	1	81.40	0.11	\$15,658.34	1	
59 Wedgewo	81.9	79.5	81.3	81.35	81.35	- 1	1	81.35	0.06	\$15,089.80	1	
59 Wedgewo	81.9	79.5	81.3	81.29	81.29	- 14	1	81.29	-100.00	\$0.00	ó	
59 Wedgewd	81.9	79.5	81.3	81.23	81.23	4	il	81.23	-100.00	\$0.00	0	
59 Wedgewo	81.9	79.5	81.3	81.12	81.12	- 1	il	81.12	-100.00	\$0.00	0	
59 Wedgewd	81.9	79.5	81.3	81.04	81.04	1	4	81.04	-100.00	\$0.00	0	
59 Wedgewo	81.9	79.5	81.3	80.95	80.95	i	î	80.95	-100.00	\$0.00	o	
69 Wedgewo	82.2	79.8	81.6	81.4	82.18	50	40	82.02	0.43	\$19,898.95	1	
69 Wedgewo	82.2	79.8	81.6	81.35	82.12	50	40	81.97	0.38	\$19,063.28	il	
69 Wedgewd	82.2	79.8	81.6	81.29	82.04	50	40	81.89	0.30	\$18,021.17	1	
69 Wedgewd	82.2	79.8	81.6	81.23	81.95	50	40	81.81	0.22	\$16,935.50		
69 Wedgewo	82.2	79.8	81.6	81.12	81-83	50	40	81.69	0.10	\$15,519.97	4	
69 Wedgewd	82.2	79.8	81.6	81.04	81.72	50	40	81.58	-100.00	\$0.00	0	
69 Wedgewd	82.2	79.8	81.6	80.95	81.6	50	40	81.47	-100.00	\$0.00	0	
79 Wedgewo	82.4	80.0	81.8	82.18	82.18	1	1	82.18	0.39	\$19,261.73	1	
79 Wedgewd	82.4	80.0	81.8	82 12	82.12	1	il	82.12	0.33	\$18,425.54	1	
79 Wedgewo	82.4	80.0	81.8	82 04	82.04	1	il	82.04	0.33	\$17,366.83	- 1	
79 Wedgewd	82.4	80.0	81.8	81.95	81.95	41	il	81.95	0.25	\$16,248.31		
79 Wedgewo	82.4	80.0	81.8	81.83	81.83	- 1	il	81.83	0.16	\$14,868.20		
79 Wedgewo	82.4	80.0	81.8	81.72	81.72	i il	1	81.72	-100.00		0	
79 Wedgewo	82.4	80.0	81.8	81-6	81-6	41	1	81.60	-100.00	\$0.00	0	
										Reg	3	

Frequency	Summarized Damage Costs (\$)
Reg	\$54,819,02
100	\$52,578.63
50	\$35,388.00
25	\$33,183,81
10	\$30,388.17
5	\$0.00
2	\$0,00
TOTAL=	\$206,357.63

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangered.

Table 6
Flooding Damages Evaluation Scale Category: Site Assessment

Site	Event	WSEL	Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth (50 Year, 5%) Direct Damages	Measure Weight	Category Importance/ Significance	
	(Yr)	(m)	(No.)	(No.)	(No.)	(\$)	(ha)	(\$)	(ha)	(\$)	(ha)	(\$)	(\$)	(\$)	(\$)	(1-10)	(1-10)	1
	2	92,69	0	0	0	\$0	0	0	0	0	0	0	\$0					
	5	93.00	0	0	.0	\$0	0	0	0	0	0	0	\$0		1			
	10	93.51	2	2	0	\$30,388	0	0	0	0	0	0	\$30,388					
31	25	93.64	2	2	0	\$33,184	0	0	0	0	0	0	\$33,184	\$5,097	\$93,046	2	8	16
l l	50	93.69	2	2	0	\$35,388	0	0	0	0	0	0	\$35,388					
	100	93.74	3	3	0	\$52,579	0	0	0	0	0	0	\$52,579					
	Reg	93.61	3	3	0	\$54,819	0	0	0	0	0	0	\$54,819					

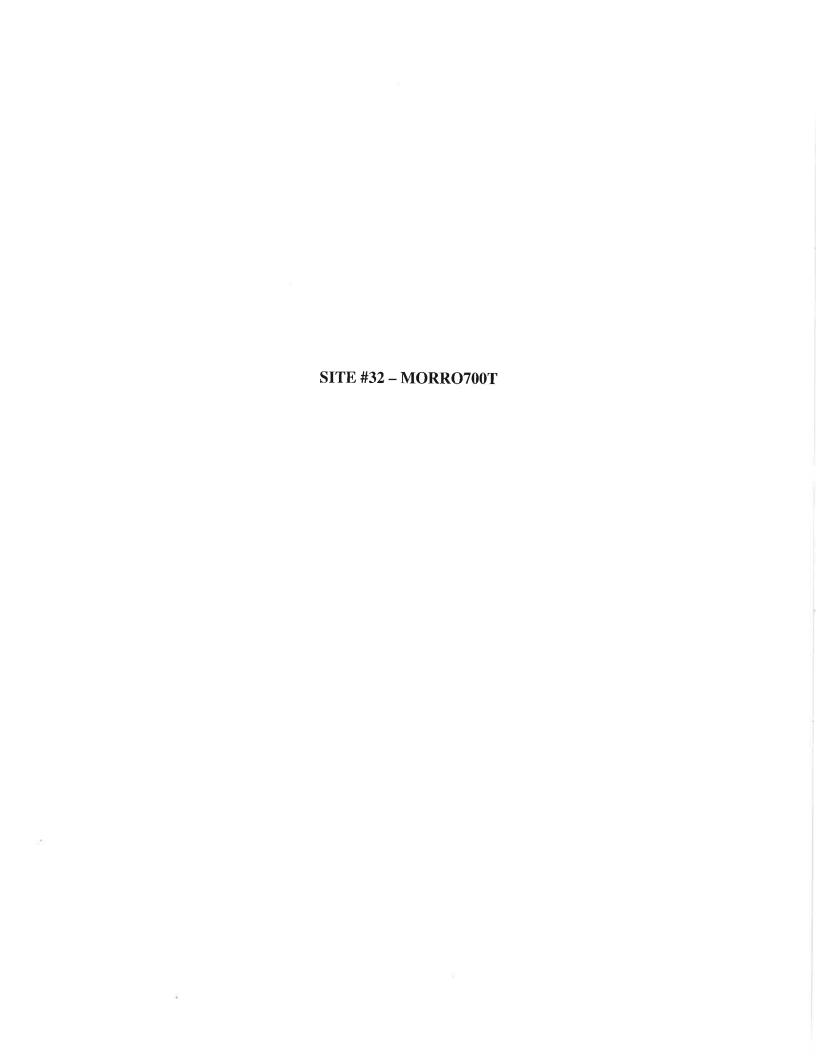
- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not
- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
- 4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
  5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

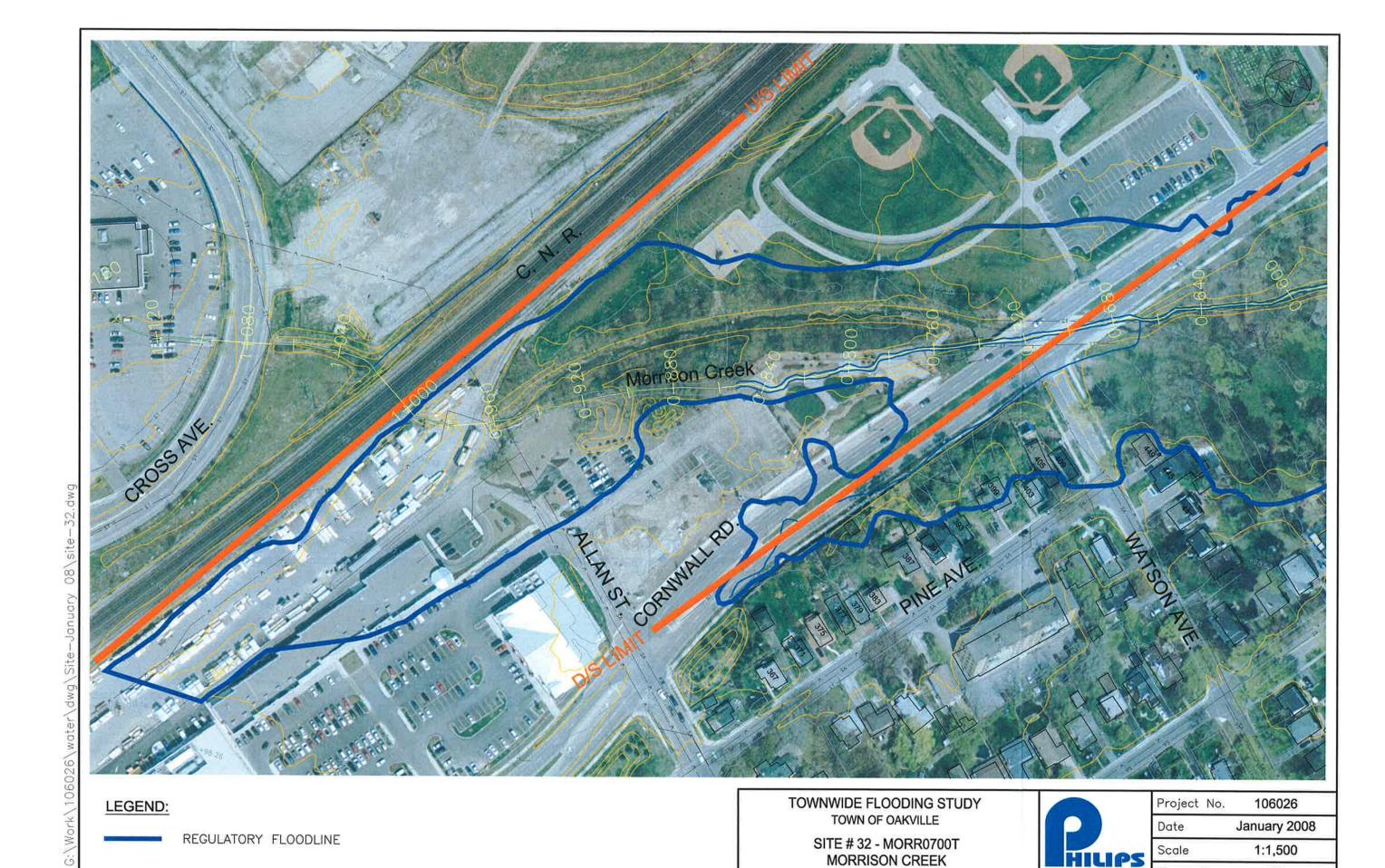
\$54,819					
Total Indirect Damage Value	Average Annual Damages 2007 Indirect Damages	Present Worth ( 50 Year, 5%) Indirect Damages	Measure Weight	Category Importance/ Significance	Product
(\$)	(\$)	(\$)	(1-10)	(1-10)	
\$0					
\$0					
\$4,558					
\$4,978	\$765	\$13,957	2	4	8
\$5,308					
\$7,887					
\$8,223					

	Finished	Basement	Lowest	Dournatroom 0 100/									
Building	Floor	Floor		Downstream 2-100/	Upstream 2-100/ Reg		Distance from	Interpolated Prope	erty 2	Building Flood		D 151 #	
No.	Elevation	Elevation	Opening	Reg Flood	Flood Elevations (m)	Section Distance		100/ Reg	Flood	Building Flood	Damage Costs (\$)	Basement Flooding	First Floor Flooding
	(m)	(m)	(m)	Elevations (m)	Flood Elevations (m)		Downstream Section		(m)	Depth (m)	Jamage Costs (4)	(Yes/ No)	(Yes/ No)
180 Lakesi								Liovations	(0.0				
	81,2	78.8	80.6	80.45	80.45	1	1		80.45	-100.00	\$0.00	0	
180 Lakes	81.2	78.8	80.6	80.41	80.41	11	1		80.41	-100.00	\$0.00	l s	
180 Lakes	81.2	78.8	80.6	80.35	80.35	-1	4		80.35			1	1
180 Lakes	81.2	78.8	80.6	80.28	80.28	1				-100.00	\$0.00	0	
180 Lakes	81.2	78.8	80.6				1		80.28	-100.00	\$0.00	0	
				80.14	80.14	1	1		80.14	-100.00	\$0.00	1 0	
180 Lakes	81.2	78.8	80.6	79.62	79.62	1	1		79.62	-100.00	\$0.00	1	1
180 Lakes	81.2	78.8	80.6	79.15	79.15		1		79.15	-100.00	\$0.00	l š	
180 Lakes	81.3	78.9	80.7	80.45	80.5	40	10		80.46			0	
180 Lakes	81.3	78.9	80.7	80.41	80.46	40	10			-100.00	\$0.00	0	1
180 Lakes	81.3	78.9	80.7						80.42	-100.00	\$0.00	0	0
180 Lakes	2000			80.35	80.4	40	10		80.36	-100.00	\$0,00	0	l
	81.3	78.9	80.7	80.28	80.32	40	10		80.29	-100.00	\$0.00	0	l
180 Lakes	81.3	78.9	80.7	80.14	80.17	40	10		80.15	-100.00	\$0.00	م م	l ä
180 Lakes	81.3	78.9	80.7	79.62	79.67	40	10		79.63	-100.00			1
180 Lakes	81.3	78.9	80.7	79.15	79.38	40	10			10.71	\$0.00	U	l
147 Wedge	82.5	80.1	81.9	80.5					79.21	-100.00	\$0.00		
147 Wedge	82.5	80.1	81.9	0111	80.61	50	8		80.52	-100.00	\$0.00	0	0
147 Wod-			45 10 10 10 10	80.46	80.57	50	8		80.48	-100.00	\$0.00	0	n
147 Wedge	82.5	80.1	81.9	80.39	80.5	50	8		80.41	-100.00	\$0.00	n	0
147 Wedge	82.5	80.1	81.9	80.31	80.43	50	8		80.33	-100.00	\$0.00	Ĭ	,
147 Wedge	82.5	80.1	81.9	80.16	80.3	50	0		80.18			U	O
147 Wedge	82.5	80.1	81.9	79,72	80.22	50	0			-100.00	\$0.00	O	0
147 Weda	82.5	80.1	81.9	79.64			8		79.80	-100.00	\$0.00	0	0
151 Wedge	82.4	80.0			80.12	50	8		79.72	-100.00	\$0.00	0	0
			81.8	80.61	81.4	40	7		80.75	-100.00	\$0.00	0	0
151 Wedge	82.4	80.0	81.8	80.57	81.35	40	7		80.71	-100.00	\$0.00	ام	0
151 Wedge	82.4	80.0	81.8	80.5	81.29	40	7		80.64	-100.00	\$0.00	Ĭ	0
151 Wedge	82.4	80.0	81.8	80.43	81.23	40	7		80.57			0	U
151 Weda	82.4	80.0	81.8	80.3	81.12	40	4			-100.00	\$0.00	O	0
151 Wedge	82.4	80.0	81.8	80.22			<u>′</u> 1		80.44	-100.00	\$0.00	0	0
151 Wedge	82.4	80.0			81.04	40	7		80.36	-100.00	\$0.00	0	0
			81.8	80.12	80.95	40	7		80.27	-100.00	\$0.00	0	0
159 Wedge	81.9	79.5	81.3	81.4	81.4	1	1		81.40	0.11	\$15,658.34	1	0
159 Wedg	81.9	79.5	81.3	81.35	81.35	11	1		81.35	0.06	\$15,089.80	41	0
159 Wedge	81.9	79.5	81.3	81.29	81.29	1	41		81.29				U
159 Wedge	81.9	79.5	81.3	81.23	81.23	41	- 1			-100.00	\$0.00	O	0
159 Wedge	81.9	79.5	81.3	81.12		:1	!!		81.23	-100.00	\$0.00	0	0
159 Wedge	81.9		(L) = (C) (L) (B)		81.12	1	1		81.12	-100.00	\$0.00	0	0
I ~ I		79.5	81.3	81.04	81.04	1	1		81.04	-100.00	\$0.00	n	n
159 Wedg	81.9	79.5	81.3	80.95	80.95	1	1		80.95	-100.00	\$0.00	n	0
169 Wedge	82.2	79.8	81.6	81.4	82.18	50	40		82.02	0.43	\$19,898.95	- 0	U
169 Wedge	82.2	79.8	81.6	81.35	82.12	50	40		81.97			. !	Ü
169 Wedge	82,2	79.8	81.6	81.29	82.04	50				0.38	\$19,063.28	1	0
169 Wedge	82.2	79.8	81.6				40		81.89	0.30	\$18,021.17	1	0
169 Wedge	82.2		1000	81.23	81,95	50	40		81.81	0.22	\$16,935.50	-1	0
1 ~1		79.8	81.6	81.12	81.83	50	40		81.69	0.10	\$15,519.97	I	0
169 Wedg	82.2	79.8	81.6	81.04	81.72	50	40		81.58	-100.00	\$0.00	0	0
169 Wedg	82.2	79.8	81.6	80.95	81.6	50	40		81.47	-100.00	\$0.00	0	Ü
179 Wedge	82.4	80.0	81.8	82.18	82.18	1	40		82.18			0	0
179 Wedge	82.4	80.0	81.8	82.12	82.12	11	3		1 CA STORY A TO	0.39	\$19,261.73	1	0
179 Wedge	82.4	80.0	81.8		551	1	21		82.12	0.33	\$18,425.54	1	0
· · · · · ·		- 1	E	82.04	82.04	1]	1	8	82.04	0.25	\$17,366.83	1	0
179 Wedge	82.4	80.0	81.8	81.95	81.95	1	1	3	81.95	0.16	\$16,248.31	1	0
179 Wedge	82.4	80.0	81,8	81.83	81.83	1	1		81.83	0.04	\$14,868.20	4	0
179 Wedg	82.4	80.0	81.8	81.72	81.72	1	4		81.72				U
179 Wedge	82.4	80.0	81.8	81.6	81.6	<u> </u>	31		1.549 FALST-CE	-100.00	\$0.00	0	0
×1.			3	01.0	01.0		1		81.60	-100.00	\$0.00	0	0
											Rea	3	

	Frequency	Summarize Costs	d Damage (\$)
	Reg	3 5	54,819.02
	100	) (	52,578.63
	50	) {	35,388.00
	25	5 \$	33,183.81
	10	) {	30,388.17
	5	5	\$0.00
	2	2	\$0.00
TOTAL =		\$2	06 357 63

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine flooding damages for each return period based on the flooding depths and damage curve equations





Feb 11/08 - avogt

Figure No.

32

Site #32 (MORR0700T) Implementation Program	
Recommended Management Approach/Project Scope:	
No management approach recommended due to	
Appropriate Lead for Undertaking:	
N/A	
Governing Protocol Legislation:	
N/A	
Approval Requirements:	
N/A	
Need for, and Scope of Follow-Up Assessment/Analysis:	
NA/	
Suggested Timing, Need for Phasing:	
N/A	
Possible Implementation Issues:	
N/A	
Possible Monitoring Requirements:	
N/A	
Need for Maintenance:	
N/A	
Potential Interface with Other Town/Agency Programs:	
N/A	
Other Funding Opportunities:	
N/A	

# Site #32 (MORR0700T) Specific Flood Management Alternative Assessment

# Data/Information:

Flooding mechanisms:

• Based on discussions with Conservation Halton there would be no Threat to Life due to a reduction in flood levels upstream of Cornwall Road to the CNR track. Based on information provided by Conservation Halton Cornwall Road would not be overtopped during the Regional storm event.

### Screened Alternatives:

• N/A

# Preferred Management Approach:

N/A

# Potential Linkage to Adjacent Sites:

• At Site 33

					ible 7 Evaluation Resul	ts				
			Cate	rgory Evaluation Pro	oducts					
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products
32	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0

The combined product of 34 is conservative, as based on discussions with Conservation Halton, actual flood depths would not result in Threat to Life or Flood Damages

	Table 4 Road Flooding Flood Criteria Evaluation																																		
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation			Flood	Elevat	ions (n	n)	T					epth (m				Flow	Velocit	les (m/s	s)		s	torm E	Event F	requen	icy Mc	difier	s	Storm Event Flooding Starts/ or Criteria Not Met	Storm Event Frequency Modifier Selected	Evaluation Scale Category Importance/ Significance	Product (Measure Welghting * Storm
		(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5	10	25	50 1	00 R	eg 2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	(2-100, Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significance
32	Design Flood Criteria	Arterial	10	96,46	95.6	95,7	95,9	96,2	96,3	96.3	95.9	-0,9	-0.7	-0.6	-0,3	-0.2	0.6 -0	6 0.0	0.5	0,7	7 0.8	0.8	0,9	0.9	1	0,4	0,2	0.08	0.04	0.02	0.01	Arterial / 1:100 - Reg	0.00	2	0.0
32	Private Vehicle	Level 1 Road/ 100-Regional	10		1	1	1	1	1	I.									- 1		0.8					- 1	0,2						0.00	5	0
32	Emergency Vehicle	Level 1 Road/ 100-Regional	10	96,46	95.6	95.7	95.9	96,2	96,3	96.3	95.9	-0.9	-0.7	-0.6	-0.3	-0,2	0.6 -0	6 0.0	0,5	0.7	0.8	0.8	0.9	0,9	1	0.4	0.2	0.08	0.04	0.02	0.01	None	0.0	6	0
32	Private Vehicle Acess to Facilities	Partial	5		1		1										- 1	- 1	- 1	1	0.8				1	0.4	0,2	0.08	0,04	0.02	0.01	Arterial / 1:100 - Reg	0,00	3	0
32	Emergency Vehicle Access to Facilities	Partial	5	96.46	95.6	95.7	95.9	96.2	96.3	96.3	95.9	-0.9	-0.7	-0.6	-0.3	-0.2	0,6 -0	6 0.0	0.5	0.7	0.8	0.8	0.9	0,9	4	0.4	0,2	0.08	0.04	0.02	0.01	25-yr	0.00	7	0
32	Private Vehicle Driveway Access (Multiuser)	High-Med Vehicle Usage	8									1 1									0.8				1		0.2					, , , , , , , , , , , , , , , , , , ,	0.00	4	0.0

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

																		Threa		Table 5 lood Crit	eria Evalu	ation																					
-			Site Down	tream Flood E	levations (m)					Reside	ntlei Units Fic	oded (#)		,		Indu	strial Area (ha)			Cor	mmercial Ar	ea (ha)			Institution	nal (ha)		Land Use	Densitles /unit)	pers/ha or	<u> </u>	People	Endangere	d		Storm E	Event Freq	ency Modifi	lers			Composite	Т
la l	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5	10 25 5	0 100	Reg 2	5	10 25	50 100	Reg	5	10 25	50 1	100 Reg	Res	nd Com	Instit	2 5	10	25 50	100	Reg 2	5	10 25	50 10		Normalized No. of People Using Storm Multipliers	Evaluation Scale Measure Weighting (1	Category Importance/ Significance (1- (7 - Day Usage (10 - Day and Ni Usage)	-10) e) ight
T	95.89	96 33	96 29	96 21	95 87	95.78	95 71	0	0	0	0	0	0	0	0	0	0 0 0	0 0	0 0	0	0 0	0 0	0 (	0	0 0	0	0 0	3 1	25 90	40	0 0	0	0 0	0	0 50	20	10 4	2 1	0.4	0	0	10	-

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)
  2 Determine flooding conditions that results in life endangerment (separate spreadsheet direct damages). Note that for residential units, life endagerment has been included if the basement has been predicted to flood.
  3 Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)
- 4 Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered
- 5 Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm
- 6 Apply adjustment factor (Value of Step 5 divided by 10)
- 7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

Finished Floor Elevation (m)	Lowest Opening (m)	Downstream 2-100/ Reg Flood Elevations (m)	Upstream 2 100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)/m2	Damage Costs (\$)	First Floor Flooding (Yes/ No)	Floor Area (m2)
97_87	97.9	97.4	97.39	50	10		-100.00	\$0.00	\$0.00	0	0
97.87	97.9	97.81	97.78	10	10	97.78	-100.00	7-2 30	\$0.00		1,800
97.87	97.9	97.69	97.66	10	97.78	97.40		1970	\$0.00		1,000
97.87	97.9	97.55	97.53	97.78	97.39666	97.53	-100.00		\$0.00		0
97.87	97.9	97.34	97.34	97.39666	97.53007841	97.34	-100.00		\$0.00		0
97,87	97.9	97.17	97.2	97.53007841	97:34	97.20	-100.00		\$0.00		0
97.87	97.9	96.96	97.01	97.34	97.19994153	97.01	-100.00	\$0.00	\$0.00		0

Frequency	Summarized Damage Costs (\$)
Reg	\$0.00
100	\$0.00
50	\$0.00
25	\$0.00
10	\$0.00
5	\$0.00
2	\$0,00

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use) 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangered.

Table 6
Flooding Damages Evaluation Scale Category: Site Assessment

Site	Event	WSEL	Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth ( 50 Year, 5%) Direct Damages	Measure	Category Importance/ Significance	
	(Yr)	(m)	(No.)	(No.)	(No.)	(\$)	(ha)	(\$)	(ha)	(\$)	(ha)	(\$)	(\$)	(\$)	(\$)	(1-10)	(1-10)	1
	2	92,69	0	0	0	\$0	0	0	0	0	0	0	\$0					
	5	93.00	0	0	0	\$0	0	0	0	0	0	0	\$0					
	10	93,51	0	0	0	\$0	0	0	0	0	0	0	\$0					
32	25	93,64	0	0	0	\$0	0	0	0	0	0	0	\$0	\$0	\$0	0	8	0
	50	93,69	0	0	0	\$0	0	0	0	0	0	0	\$0					
	100	93,74	0	0	11	\$0	0	0	0	0	0	0	\$0					
	Reg	93,61	0	0	0	\$0	0	0	0	0	0	0	\$0					

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not
- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
- 4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
- 5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

Finished Floor Elevation (m)	Lowest Opening (m)	Downstrea m 2-100/ Reg Flood Elevations (m)	2-100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2-100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)/m2	Damage Costs (\$)	First Floor Flooding (Yes/ No)	Floor Area (m2)
97.87	97.9	- 1.3191	97.39	50	10	97.40	-100.00	\$0.00	\$0.00	0	0
97.87	97.9	97.81	97.78	10	10	97.78	-100.00	\$0.00		0	0
97.87	97.9	97.69	97.66	10	97.78	97.40	-100.00	\$0.00		o.	0
97.87	97.9	97.55	97.53	97.78	97.39666	97.53	-100.00	\$0.00	\$0.00	o o	0
97.87	97.9	97.34	97.34	97.39666	97.53007841	97.34	-100.00	\$0.00		o o	0
97.87	97.9	97.17	97.2	97.53007841	97.34	97.20	-100.00	\$0.00		ŏ	0
97.87	97.9	96.96	97.01	97.34	97.19994153		-100.00		\$0.00	ő	0

Summarized Damage Costs (\$)
\$0.00
\$0.00
\$0.00
\$0.00
\$0.00
\$0.00
\$0.00

Total

Indirect Damage

Value

(\$)

\$0

\$0

\$0

\$0

\$0

\$0

Present Worth

( 50 Year, 5%)

Indirect

**Damages** 

(\$)

\$0

Category

Importance/

Significance

(1-10)

**Product** 

Measure

Weight

(1-10)

0

**Average Annual** 

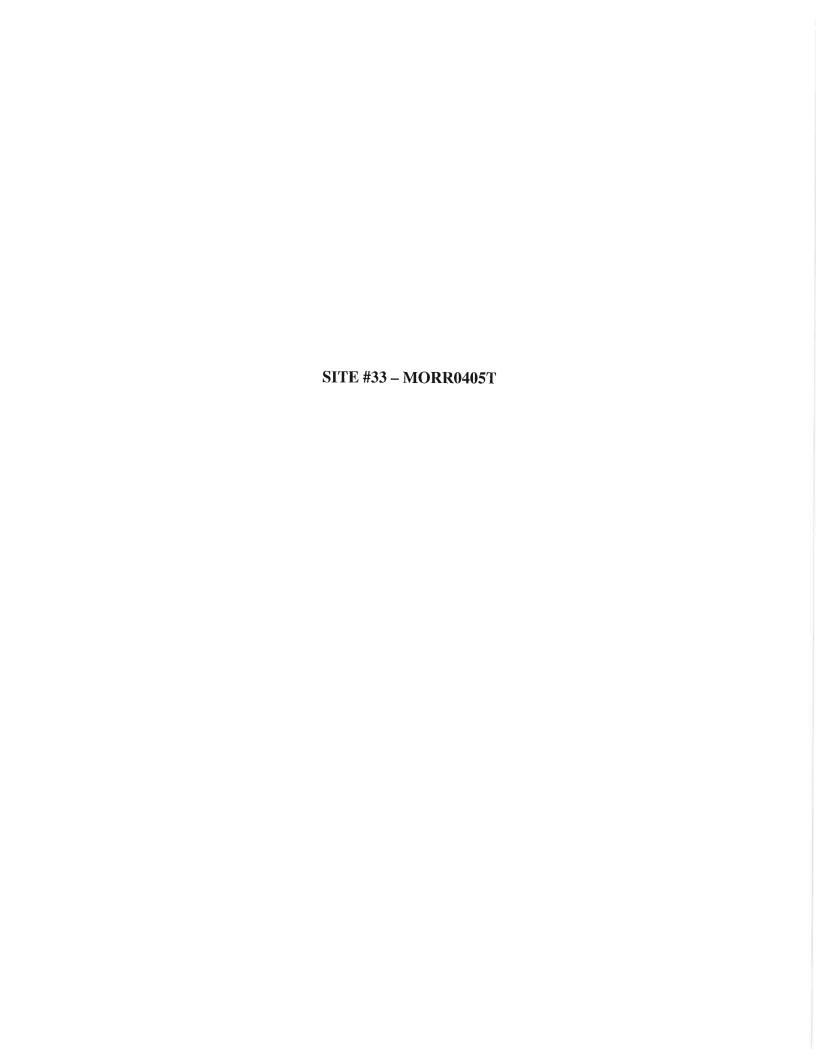
Damages 2007

**Indirect Damages** 

(\$)

SO

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine flooding damages for each return period based on the flooding depths and damage curve equations



LEGEND:

REGULATORY FLOODLINE

TOWNWIDE FLOODING STUDY
TOWN OF OAKVILLE
SITE # 33 - MORR0405T
MORRISON CREEK

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HILLOS	ľ
ENGINEERING	r

Project No.	106026
Date	January 2008
Scale	1:1,500
Figure No.	33

### Site #33 (MORR0405T) Implementation Program

### Recommended Management Approach/Project Scope:

- Upstream flood storage required to reduce flows, potentially located upstream of Maple Avenue within open space lands
- Flood proofing of homes not flooded on all sides

### Appropriate Lead for Undertaking:

• Timing and phasing as per Town of Oakville Capital Works Program based on priority ranking established herein. This project would require an Environmental Assessment to determine the feasibility of a flood storage area upstream.

#### Governing Protocol Legislation:

- Town of Oakville's Policies and protocols
- Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
- Regional Municipality of Halton (EEAC) if flood control located within an ESA
- Ministry of Natural Resources Lakes and Rivers Act
- Department of Fisheries and Oceans Fisheries Act
- Ministry of Environment Certification of Approval
- Others

# Approval Requirements: (Would require both Class EA approval and detail design approval)

- Town of Oakville
- Conservation Halton Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Permit
- Regional Municipality of Halton potentially EEAC
- Regional Municipality for potential water and wastewater servicing alterations
- Ministry of Environment approval of flood control facility design
- Ministry of Environment Permit to Take Water (should dam and pumping for creek diversion or dewatering be required)
- Potentially Department of Fisheries and Oceans (i.e. should a Harmful Alteration Disruption or Destruction (HADD) be identified to occur based on the proposed works)
- Input from Utility companies for utility locations
- Private ownership approval for flood proofing

#### Need for, and Scope of Follow-Up Assessment/Analysis:

- Class Environmental Assessment for assessing feasibility of upstream flood control controls
- As part of the EA
  - o Hydrologic modeling refinement
  - o Hydraulic modeling refinement
  - o Vegetation assessment
  - o Fisheries assessment
  - o Natural channel design assessment
- Approval process with private land owners
- Detail design of flood control facility based on Class EA
- Revision to hydraulic modeling at Site 33 and assessment of reduced flows on flood impacts
- Assessment of homes still flooded with revised hydraulics, topographic survey of homes; flood proofing to follow assessment

#### Suggested Timing, Need for Phasing:

• Timing of project dependant on Capital Works Program budget and priority of project within the Program.

### Possible Implementation Issues:

- Lack of feasibility to implement upstream flood controls, or flood controls not effective in reducing downstream flows as required
- Land ownership
- Fisheries constraints
- Approval from home owner(s) for flood proofing

#### Possible Monitoring Requirements:

Potentially Department of Fisheries and Oceans monitoring requirements\

Site #33 (MORR0405T) I	mplementation Program
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### Need for Maintenance:

Would have to be determined within the Class EA

# Potential Interface with Other Town/Agency Programs:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Potential opportunities with Town's Creek Erosion Study
- Potential projects already identified by Conservation Halton

### Other Funding Opportunities:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Others

# Site #33 (MORR0405T) Specific Flood Management Alternative Assessment

### Data/Information:

### Flooding mechanisms:

- Maple Avenue crossing 161 m by 3.1 m by 1.22 m box culvert
- Encroachment

#### Screened Alternatives:

- Culvert upgrades 2 (2.4 m by 1.2 m box culverts) would be expensive due to 161 m length of culvert and location of culvert within private property.
- Flood storage at site and north of Cornwall Road
- Floodplain and channel improvements would not provide flood protection as the Maple Avenue crossing is the hydraulic constraint.
- Flood-proofing
- Acquisition
- Regulate

### Preferred Management Approach:

- Flood storage at site and potentially north of Cornwall road, details to be determined.
- Flood-proof to extent possible of homes not flooded on all sides.
- Regulate

### Potential Linkage to Adjacent Sites:

• Site 32 and 35

					able 7 Evaluation Resul	ts				
			Cate	gory Evaluation Pr						
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products
33	0.6	0.4	0.5	0.6	0.7	0.5	40.0	32.0	16.0	91.3

	T		-41								F	Road F	loodi		able 4 od Cr		Evalu	ation																	
Site No	Evaluation Scale Criteria	Evaluation Scale Measure  (Road Classification/ Storm	Measure Weight	Road/ Driveway Elevation			Flood	Elevati	ions (m	1)	ľ					Depth (i				Flo	w Velo	cities (	(m/s)	T		Storn	ı Event	Freque	ency M	odifiers		Storm Event Flooding Starts/ or Criteria Not Met	Storm Event Frequency Modifier Selected	Evaluation Scale Category Importance/ Significance	Product (Measure Weighting * Storm Frequency
		frequency)	(4.6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5	_10	25	50	100	Reg	2	5 1	10 2	25 5	50 100	Reg	g 2	5	10	25	50	100	Reg	(2-100, Reg)	(0.4-50)	(1-10)	Modifier * Category Significance
33	Design Flood Criteria	Collector	8	95,40	94.8	95.6	95.6	95.7	95.7	95,8	95_7	0.0	0.2	0,2	0.3	0.3	0.4	0.3	0.0	5 0	0,6 0	7 0	0.8	0.7	1	0.4	0.2	0.08	0.04	0.02	0.01	Collector / 1:50	0.04	2	0.6
33	Private Vehicle	Level 4 Road/ 100-Regional	4	95,40			1						I I										0.8						0.04			100-yr	0.02	5	0.4
33	Emergency Vehicle	Level 4 Road/ 100-Regional	4	95.40	94.8	95.6	95,6	95.7	95.7	95.8	95.7	0.0	0.2	0.2	0.3	0.3	0.4	0.3	0.0	0.5 0	0.6 0	.7 0	8 0.8	0.7	١,	0.4	0.2	0.08	0.04	0.02	0.01	None	0.0	6	
33	Private Vehicle Acess to Facilities	Partial	5	95.40																			.8 0.8						0.04				0.04	3	0.6
33	Emergency Vehicle Access to Facilities	Partial	5	95.40			1								- 1			- 1	- 1				8 0.8						0.04					7	
33	Private Vehicle Driveway Access (Multiuser)	Medium Vehicle Usage	6		11	1				1 11					- 1			- 1					8 0.8						0.04		1.0.	,	0,02	4	0.7

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

								,										1	hreat to	Ta Life Floo	able 5 od Criter	ia Evalua	ıtion																							
			Site Downs	ream Flood E	levations (m	)				Resid	ential Units Flo	oded (#)				Indu	strial Area	(ha)			Comm	ercial Are	a (ha)			Institut	tlonal (ha	)	(Lan	d Use Dens /u		/ ha or		People E	Endangere	ed		Storm	Event Fre	quency	Modifiers				Composite	T
ile Na	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5	10 25	50	100 Re	2	5. 10	25	50 100	Reg	2 5	10	25 50	100	Reg Re	s Ind	Com I	nstit	2 5	10	25 50	100	Reg :	2 5	10	25 50	100	Reg Mul	People	Evaluation Scale Measure Weighting (1- 10)	Calegory Importance/ Significance (1-10 (7 - Day Usage) (10 - Day and Nigh Usage)	10) ;) ght
3	94 79	95 56	95.63	95 67	69,68	95.8	95 67	0	2	3	7	12	12	3	0	0	0 0	0	0 0	0	0 0	0	0 0	0 (	0 0	0	0 0	0	0 3	125	90	40	0 6	9	21 36	36	9 5	0 20	10	4 2	1	04 4	05.6	4	10	$\exists$

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)
  2 Determine flooding conditions that results in life endangerment (separate spreadsheet direct damages). Note that for residential units, life endagerment has been included if the basement has been predicted to flood.
  3 Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)
  4 Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered

- 5 Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm
- 6 Apply adjustment factor (Value of Step 5 divided by 10)
- 7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

_Building No	Finished Floor Elevalion (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream 2-100/ Reg Flood Elevations (m)	Upstream 2 100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Properly 2- 100/ Reg Flood Elevations	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floo Flooding (Yes/ No
477 Maple Av	95.9	93.5	95,3	95 19	95 19	-	1	(m) 95.19	-100 00	\$0.00	0	
477 Maple Av	95 9	93.5	95 3		95,67	3	1	95 67	0.38	\$19,119.77	1	
477 Maple Av 477 Maple Av	95 9 95 9	93.5	95 3		95.56	- 1	1	95 56	0.27	\$17,625.66	1	
477 Maple Av	95 0	93.5 93.5	95 <b>3</b> 95 <b>3</b>		95.34 94.89		1 1	95 34	0 05	\$14,978.59	1	
477 Maple Av	95 9	93.5	95.3	94.4	94.4	9	1	94 69 94 40	100.00 100.00	\$0.00 \$0.00	0	
477 Maple Av	95.9	93.5	95 3		94.28		l i	94 28	-100.00	\$0.00	9	
473 Maple Av	95.9	93.5	95.3		95 19	1	1	95.19	-100.00	\$0.00	0	
473 Maple Av	95.9	93 5	95.3	95,67	95 67	3	3	95 67	0.38	\$19,119.77	1	
473 Maple Av	95.9	93.5	95.3	95 56	95 56		1	95.56	0.27	\$17,625.66	1	
473 Maple Av 473 Maple Av	95.9	93.5	95.3	95,34	95,34	13	1	95 34	0.05	\$14,978 59	1	
473 Maple Av	95 9 95 9	93 <b>5</b> 93 <b>5</b>	95.3	94.69	94.89	1		94 89	-100,00	\$0.00	0	
473 Maple Av	95.9	93.5	95.3 95.3	94 4 94 28	94.4		1 3	94 40	-100.00	\$0.00	0	1
469 Maple Av	95.9	93.5	95.3	95 19	95.19		-	94.28 95.19	-100.00	\$0,00	0	
469 Maple Av	95.9	93 5	95 3	95.67	95.67	i	1	95 67	0.38	\$19,11977	1	
469 Maple Av	95.9	93 5	95 3	95.56	95.56	1	3	95 56	0.27	\$17,625.66	19	
469 Maple Av	95.9	93.5	95 3	95 34	95.34	1	1	95.34	0.05	\$14,978.59		
469 Maple Av	95 9	93.5	95 3	94 89	94.89	1	1	94.89	-100.00	\$0.00	-0	
469 Maple Av	95 9 95 9	93.5 93.5	95 3	94 4	94.4	1	1 3	94 40	-100 00	\$0.00	0	
465 Maple Av	96	93.6	95 3 95 4	94.28 95.19	94 28 95 19	1	1	94 28	-100.00	\$0.00	. 0	
465 Maple Av	96	93.6	95 4	95.67	95.67	1	1	95.19 95.67	100 00	\$0,00 \$17,756.52	0	
465 Maple Aw	96	93 6	95 4	95.56	95.56	i	i	95.56	0 17	\$16,368.95	- 1	
465 Maple Av	96	93.6	95,4	95,34	95.34	1	1	95 34	-100 00	\$0.00	0	
465 Maple Av	96	93.6	95 4	94 89	94.89	- 3	1 3	94 89	-100.00	\$0.00	0	
465 Maple Av	96	93.6	95 4	94 4	94 4	1	1	94.40	-100 00	\$0.00	0	
465 Maple Av	96 98.1	93.6	95.4	94.28	94.28	1	1	94.28	-100.00	\$0.00	0	
461 Maple Av 461 Maple Av	96.1 96.1	93.7 93.7	95 5 95 5	95 19 95 67	95 19 95.67	1	!	95 19	100.00	\$0.00	0	
461 Maple Av	96.1	93.7	95.5	95.56	95.56	1		95 67 95 56	0 18	\$16,490,48 \$15,201.83	13	
461 Maple Av	96.1	93.7	95.5	95.34	95.34	1	l. il	95 34	-100.00	\$0.00	0	
461 Maple Av	96.1	93.7	95.5	94 89	94.89	1	1 3	94 89	+100.00	\$0.00	o	
461 Maple Aw	96_1	93.7	95.5	94.4	94.4	1	- 1	94 40	-100 00	\$0.00	0	
461 Maple Av	96.1	93.7	95.5	94 28	94.28	1	1	94 28	-100.00	\$0.00	٥	
485 Bohemia 485 Bohemia	96 96	93.6	95.4	95 19	95.19	1	1	95 19	-100 00	\$0.00	0	
485 Bohemia	96	93.6 93.6	95.4 95.4	95.67 95.56	95.67 95.56	1	1	95 67	0.28	\$17,756 52	1	
485 Bohemia	96	93.6	95 4	95 34	95.34	1	1 0	95.56 95.34	0 17	\$16,368 95	1	
485 Bohemia	96	93.6	95 4	94 89	94.89	1	1	94 89	-100 00 -100 00	\$0.00 \$0.00	0	
485 Bohemia	96	93.6	95.4	94.4	94.4	1	1	94 40	-100.00	\$0.00	0	
485 Bohemia	96	93.6	95.4	94 28	94.28		1	94 28	-100.00	\$0.00	10	
487 Bohemia	96	93 6	95 4	95 19	95.19	1	1	95,19	-100,00	\$0.00	0	
487 Bohemia 487 Bohemia	96 96	93 6 93 6	95 4 95 4	95,67 95,56	95.67	1	1	95.67	0.28	\$17,756,52	3	
487 Bohemia	96	93.6	95.4	95.34	95.56 95.34	1	11 11	95 56 95 34	0.17	\$16,368.95	1	
487 Bohemia	96	93 6	95.4	94.89	94.89	1		94.89	-100 00 -100 00	\$0.00 \$0.00	0	
487 Bohemia	96	93.6	95.4	94.4	94.4	1	ll îl	94.40	-100.00	\$0.00	o	
487 Bohemia	96	93.6	95.4	94.28	94.28	1	1	94.28	-100.00	\$0.00	0	
489 Bohemla	96	93.0	95.4	95 19	95.19	ī	- 1	95 19	-100.00	\$0.00	0	
489 Bohemia 489 Bohemia	96 96	93.0	95.4	95,67	95.67	1	1	95.67	0.28	\$17,756.52	1	
489 Bohemia	96	93.6 93.6	95.4 95.4	95 56 95 34	95.56 95.34	1		95.56	0 17	\$16,368.95	1	
489 Bohemia	96	93.6	96.4	94.89	94.89	- 1		95 34 94 89	-100 00 -100 00	\$0.00 \$0.00	0	
489 Bohemia	96	93.6	35.4	94.4	94.4	- 1	1 1	94.40	-100 00	\$0.00	o	
489 Bohemia	. 96	93.6	95.4	94 28	94.28	1	1	94 28	100.00	\$0.00	o	
445 Watson A	96.9	94.5	96.3	95_35	95.35	1	- 1	95.35	-100.00	\$0.00	0	
445 Walson A	96.9 96.9	94.5	96.3	95.78	95.78	1	1	95.78	-100.00	\$0.00	0	
445 Watson A	96.9	94.5	96.3 96.3	95 69 95 53	95.69	2	1 11	95,69	-100,00	\$0.00	0	
445 Walson A	96.9	94.5	96.3	95 28	95.53 95.2 <b>6</b>			95.53	-100 00	\$0.00	0	
445 Walson A	96.9	94.5	96.3	95.16	95.16	1	1 4	95.28 95.16	-100,00 -100,00	\$0.00	0	
445 Watson A	96.9	94.5	96.3	94 97	94.97	i	4	94.97	-100.00	\$0.00	ő	
409 Pine Ave	96	93.6	95.4	95 69	95.69	1	7	95.69	0.30	\$18,021.17	1	
409 Pine Ave	96	93 6	95.4	95 9	95.9	. 1	1	95.90	0.51	\$21,049 65	1	
409 Pine Ave 409 Pine Ave	96	93.6 93.6	95.4 95.4	95 84	95.84	1	1	95.64	0 45	\$20,135.85	3	
409 Pine Ave	96	93.6	95.4	95.76 95.66	95.76 95.66	1	1	95.76	0,37	\$18,978.87	. 1	
409 Pine Ave	96	93.6	95.4	95 55	95.55	- 1		95.66 95.55	0.27	\$17,625,66 \$16,248,31	1	
409 Pine Ave	96	93.6	95.4	95 39	95.39	- 1		95.39	-100.00	\$0.00	0	
405 Pine Ave	96.1	93,7	95.5	95 69	95.69	1	i	95.69	0.20	\$16,736.25	1	
405 Pine Ave	96.1	93.7	95.5	95 9	95.9	1	11	95.90	0 41	\$19,548 80	1	
105 Pine Ave	96 1	93 7	95.5	95.84	95.84	1		95.84	0.35	\$18,700.16	1	
405 Pine Ave 405 Pine Ave	96 1	93,7	95.5	95.76	95.76	- 1	1	95.76	0.27	\$17,625,66	1	
105 Pine Ave	96.1 96.1	93.7 93.7	95.5 95.5	95 66 95 55	95.66		1	95.86	0 17	\$16,368.95	1	
405 Pine Ave	96.1	93.7	95.5	95.55	95.55 95.39	3		95.55 95.39	-100.00	\$15,089 80	1 0	
403 Pine Ave	96.2	93.8	95.6	95_69	95.69	-	- 1	95.69	0.10	\$15,542.95	- 0	
403 Pine Ave	96.2	93.8	95.6	95 9	95 9	- 1		95.90	0.31	\$18,154.96	1	
403 Pine Ave	96.2	93 8	95.6	95 84	95.84	1	1	95.84	0.25	\$17,366 83	il	
403 Pine Ave	96.2	93.8	95.6	95.76	95.76	5.1	1	95.78	0.17	\$16,368,95	1	
403 Pine Ave 403 Pine Ave	96.2 96.2	93.8	95.6	95.66	95.66	- 1	1	95.66	0.07	\$15,201.83		
403 Pine Ave	96.2	93.8	95.6 95.6	95.55 95.39	95.55	. 1	1	95.55	-100,00	\$0.00	0	
399 Pine Ave	96.3	93.9	95.7	95,39	95.39 95.69	- 1		95 39 95 69	-100.00	\$0.00	0	
399 Pine Ave	96.3	93.9	95.7	95.9	95,9	1	- 4	95.90	0.21	\$16,860.51		
399 Pine Ave	96.3	93.9	95.7	95.84	95.84	- 1	의	95.84	0.15	\$16,128.57	3	
399 Pine Ave	96.3	93.9	95.7	95 76	95.76	1	3.6	95.76	0.07	\$15,201.83	i	
399 Pine Ave	96 3	93.9	95.7	95 66	95.66	1	1	95 66	-100.00	\$0.00	0	
399 Pine Ave	96.3	93.9	95.7	95.55	95.55		1.5	95.55	-100,00	\$0.00	0	
399 Pine Ave	96.3	93.9	95.7	95 39	95.39	1	1	95.39	-100,00	\$0.00	0	
										Reg	3	
										100 50	12 12	
										25	7	
										10	3	
										5	2	

Frequency	Summarized Damage Costs (\$)
Reg	\$50,300.36
100	\$220,489.81
50	\$205,886.01
25	\$113,111.08
10	\$49,196 44
5	\$31,338 11
2	\$0.00

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
  2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
  4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
  5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
  6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangerme

Table 6
Flooding Damages Evaluation Scale Category: Site Assessment

Site	Event	WSEL	Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth (50 Year, 5%) Direct Damages	Measure	Category Importance/ Significance	
	(Yr)	(m)	(No.)	(No.)	(No.)	(\$)	(ha)	(\$)	(ha)	(\$)	(ha)	(\$)	(\$)	(\$)	(\$)	(1-10)	(1-10)	
	2	92.69	0	0	0	\$0	0	0	0	0	0	0	\$0	***				
	5	93,00	2	2	0	\$31,338	0	0	0	0	0	0	\$31,338					
	10	93,51	3	3	0	\$49,196	0	0	0	0	0	0	\$49,196					
33	25	93,64	7	7	0	\$113,111	0	0	0	0_	0	0	\$113,111	\$20,297	\$370,536	4	8	32
	50	93.69	12	12	0	\$205,886	0	0	0	0	0	0	\$205,886					
	100	93.74	12	12	0	\$220,490	0	0	0	0	0	0	\$220,490					
	Reg	93,61	3	3	0	\$50,300	0	0	0	0	0	0	\$50,300					

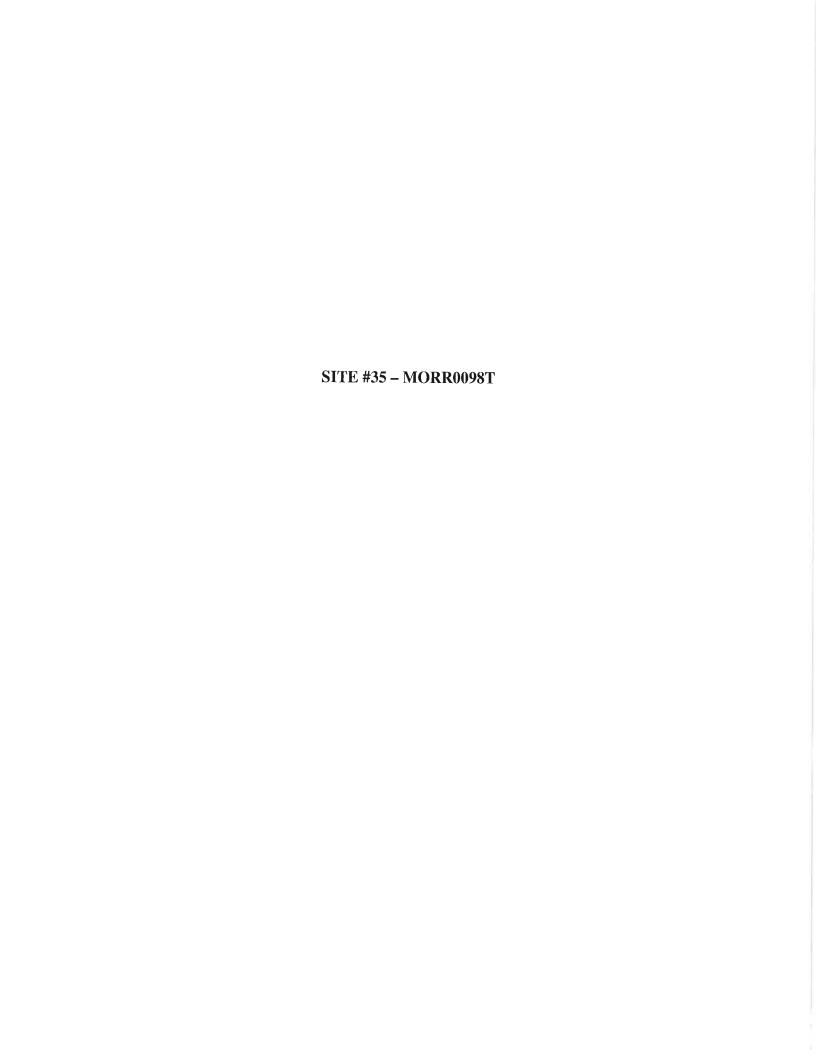
- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not
- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
- 4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
  5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

\$50,300					
Total Indirect Damage Value	Average Annual Damages 2007 Indirect Damages	Present Worth ( 50 Year, 5%) Indirect Damages	Measure Weight	Category Importance/ Significance	Product
(\$)	(\$)	(\$)	(1-10)	(1-10)	
\$0					
\$4,701					
\$7,379					
\$16,967	\$3,045	\$55,580	4	4	16
\$30,883					
\$33,073					
\$7,545					

wnstream Reg levations	2-100/ Flood (m)	Upstream 2-100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Prop 100/ Reg Elevations	Flood (m)	Building Flood Depth (m)	Damage Costs (S)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
	95 19 95 67	95 19 95 67	1			95.19 95.67	-100 00 0.38	\$0.00 \$19,119.77	0	
	95 56 95 34	95 <b>56</b> 95 <b>34</b>	1	i		95.56	0.27	\$17,625.86	i	
	94 89	94.89	1	1		95.34 94.89	0.05 -100.00	\$14,978.59 \$0.00	1 0	
	94 4 94 28	94.4	1	1		94.40 94.28	-100.00 -100.00	\$0.00 \$0.00	0	
	95 19 95 67	95 19 95 67				95 19	-100.00	\$0.00	ő	
	95.56	95.58	i	-		95.67 95.56	0:38 0.27	\$19,119.77 \$17,625.66	1	
	95.34 94.89	95 34 94 89	1	1		95 34 94 89	0.05 -100.00	\$14,978,59 \$0.00	1	
	94.4 94.28	94 4 94 28	1	1		94 40	-100.00	\$0.00	0	
	95 19	95.19	1	1		94.28 95.19	-100.00 -100.00	\$0.00 \$0.00	0	
	95 67 95 56	95 <b>67</b> 95 <b>56</b>	1	1		95 67 95 56	0.38 0.27	\$19,119 <b>77</b> \$17,625 <b>66</b>	1	
	95 34 94 89	95 34 94 89	1	1		95.34	0.05	\$14,978 59	4	
	94 4	94.4	1	1		94.89	-100.00 -100.00	\$0.00 \$0.00	0	
	94 28 95 19	94 28 95 19	1	1		94.28 95.19	-100.00 -100.00	\$0.00	0	
	95 67 95 56	95.67	1	1		95.67	0.28	\$0.00 \$17,756.52	0	
	95 34	95 <b>56</b> 95 <b>34</b>	ì	3		95.56 95.34	0 17 -100.00	\$16,368.95 \$0.00	1	
	94.89	94.89	1	1		94 89 94 40	-100.00 -100.00	\$0.00	0	
	94.28 95.19	94.28				94 28	-100.00	\$0.00 \$0.00	0	
	95,67	95.19 95.67	1	3		95 19 95 67	-100.00 0.18	\$0.00 \$16,490.48	0	
	95.56 95.34	95 56 95.34	1	1		95.56 95.34	0.07	\$15,201.83	i	
	94.89 94.4	94.89	1	i		94.89	-100.00 -100.00	\$0.00 \$0.00	0	
	94 28	94.4 94.28	- 1	1		94.40	-100.00 -100.00	\$0.00 \$0.00	0	
	95 19 95 67	95.19 95.67	3	1		95.19 95.67	-100.00	\$0.00	.0	
	95 56 95 34	95 56	- 1	i		95.56	0.28	\$17,756.52 \$16,368.05	1	
	94 89	95 34 94 89	1	1		95.34 94.89	-100.00 -100.00	\$0.00 \$0.00	0	
	94.4 94.28	94.4 94.28	1	1		94.40 94.26	-100.00 -100.00	\$0.00	0	
	95 19 95 67	95 19	1	i		95.19	-100,00	\$0.00 \$0.00	0	
	95.56	95.67 95.56	1	1		95.67 95.58	0.28	\$17,756.52 \$16,368.95	1	
	95,34 94.89	95.34 94.89	1	1		95.34 94.89	-100.00	\$0.00	0	
	94 4 94 28	94.4	1	1		94.40	-100,00 -100,00	\$0.00 \$0.00	0	
	95 19	94 28 95 19	- 1	1		94 28 95 19	-100.00 -100.00	\$0.00 \$0.00	0	
	95 67 95 56	95 <b>67</b> 95 <b>56</b>	1	1		95.67 95.56	0.28	\$17,756.52	1	
	95.34	95.34	1	i		95.34	-100.00	\$16,368.95 \$0.00	0	
	94 89 94 4	94. <b>89</b> 94.4	3	1		94 89	100.00	\$0.00 \$0.00	0	
	94.28 95.35	94 28 95 35	- 1	- !		94.28 95.35	-100.00	\$0.00	. 0	
	95 78	95.78	il.	i		95.78	-100,00 -100,00	\$0,00 \$0.00	0	
	95 69 95 53	95.69 95.53	1	1		95.69 95.53	-100.00 -100.00	\$0.00 \$0.00	0	9
	95.28 95.16	95.28 95.16	1	3		95.28 95.16	-100.00 -100.00	\$0.00	0	
	94.97	94.90	- 1	i		94 97	-100.00	\$0.00 \$0.00	0	
	95 69 95 9	95.69 95.9	3	1		95 69 95 90	0.30	\$18,021.17 \$21,049.65	1	
	95.84 95.76	95.84 95.76	1	1		95.84 95.76	0.45 0.37	\$20,135.85	1	
	95.66	95.68	i	i		95.66	0.27	\$18,978.97 \$17,625.66	3	
	95 55 95 39	95.5 <b>5</b> 95.3 <b>9</b>				95.55 95.39	-100.00	\$16,248.31 \$0.00	1	
	95 69 95 9	95.6 <b>9</b> 95. <b>9</b>	1	1		95 69 95 90	0.20	\$16,736.25		(
	95 84 95 76	95,84	1	i		95,84	0.35	\$19,548.80 \$18,700.16	1	
	95.66	95.76 95.66	i			95.76 95.68	0.27	\$17,625.66 \$16,368.95	1	
	95.55 95.39	95. <b>55</b> 95. <b>39</b>	1	1		95.55 95.39	0.06 -100.00	\$15,089.80	1	
	95 69	95.69	1	i		95.69	0.10	\$0,00 \$15,542.95	0	
	95.9 95.84	95. <b>9</b> 95. <b>84</b>	1	3		95.90 95.84	0.31	\$18,154.96 \$17,366.83	1	0
	95 76 95 66	95.76 95.66	1	1		95.76 95.66	0.17	\$16,368.95	1	
	95.55	95.55	ĵ.	il		95.55	-100.00	\$15,201 83 \$0.00	0	(
	95.39 95.69	95 39 95 69	1	1		95.39 95.69	-100.00 -100.00	\$0.00	0	
	95.9 95.84	95 9 95 84	1	1		95.90	0.21	\$16,860,51	1	
	95.76	95.78	i	- i		95.84 95.76	0.15	\$16,128.57 \$15,201.83	1	6
	95 66 95 55	95,66 95.55	3	1		95.66 95.55	-100.00 -100.00	\$0.00 \$0.00	0	6
	95.39	95.39	i	i		95.39	-100.00	\$0.00	0	0
								Reg 100	3 12	0
								50 25	12 7	0
								10	3	0
								5	2	0

g elevations for all storm events at buildings that potentially flood or elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/ent floor elevation by substracting 2.44m from the first floor elevation
ent window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land us g depths based on lowest opening elevation and flooding elevations for all storms
g damages for each return period based on the flooding depths and damage curve equations

Frequency		Summarized Damage Costs (\$)
	Reg	\$50,300.36
	100	\$220,489 81
	50	\$205,886.01
	25	\$113,111,08
	10	\$49,196 44
	5	\$31,338.11
	2	\$0.00





LEGEND:

REGULATORY FLOODLINE

TOWNWIDE FLOODING STUDY TOWN OF OAKVILLE SITE # 35 - MORR0098T MORRISON CREEK

HILLOS	ľ
ENGINEERING	ľ

110		
	Project No.	106026
	Date	January 2008
	Scale	1:1,000
	Figure No.	35

#### Site #35 (MORR0098T) Implementation Program

# Recommended Management Approach/Project Scope:

- Flood control upstream of site (See Site 33)
- Upgrade Chartwell Road crossing by adding 3 m by 1.6 m box culvert to existing 3 m by 1.6 m box culvert

### Appropriate Lead for Undertaking:

• Timing and phasing as per Town of Oakville Capital Works Program based on priority ranking established herein. This project would require an Environmental Assessment to determine the feasibility of a flood storage area upstream. The additional culvert could be considered following possible reduction of flows from flood protection upstream

#### Governing Protocol Legislation:

- Town of Oakville's Policies and protocols
- Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
- Ministry of Natural Resources Lakes and Rivers Act
- Department of Fisheries and Oceans Fisheries Act
- Ministry of Environment Certification of Approval
- Others

# Approval Requirements: (Would require both Class EA approval and detail design approval)

- Town of Oakville
- Conservation Halton Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Permit
- Regional Municipality for potential water and wastewater servicing alterations
- Ministry of Environment approval of flood control facility design
- Ministry of Environment Permit to Take Water (should dam and pumping for creek diversion or dewatering be required)
- Potentially Department of Fisheries and Oceans (i.e. should a Harmful Alteration Disruption or Destruction (HADD) be identified to occur based on the proposed works)
- Input from Utility companies for utility locations

### Need for, and Scope of Follow-Up Assessment/Analysis:

- Class Environmental Assessment for assessing feasibility of upstream flood control controls
- As part of the EA
  - o Hydrologic modeling refinement
  - o Hydraulic modeling refinement
  - o Vegetation assessment
  - o Fisheries assessment
  - Natural channel design assessment
- Approval process with private land owners
- Detail design of flood control facility based on Class EA
- Revision to hydraulic modeling at Site 35 and assessment of reduced flows on flood impacts
- Topographic survey of crossing and creek to facilitate hydraulic modeling and detail design
- Hydraulic modeling of Site with proposed culvert addition once potential flood control in place

#### Suggested Timing, Need for Phasing:

Timing of project dependant on Capital Works Program budget and priority of project within the Program.

#### Possible Implementation Issues:

- Lack of feasibility to implement upstream flood controls, or flood controls not effective in reducing downstream flows as required
- Land ownership
- Fisheries constraints

#### Possible Monitoring Requirements:

Potentially Department of Fisheries and Oceans monitoring requirements

#### Need for Maintenance:

Would have to be determined within the Class EA

#### Potential Interface with Other Town/Agency Programs:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Potential opportunities with Town's Creek Erosion Study
- Potential projects already identified by Conservation Halton

# Site #35 (MORR0098T) Implementation Program

# Other Funding Opportunities:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Others

# Site #35 (MORR0098T) Specific Flood Management Alternative Assessment

# Data/Information:

# Flooding mechanisms:

- Chartwell Road crossing 3 m by 1.6 m resulting in overflow (spill across road to Site 37)
- Spill across Maple Road resulting from 3.1 m by 1.22 m box culvert (Site 33)

### Screened Alternatives:

- Culvert/crossing upgrades for Chartwell Road crossing by adding a 3 m by 1.6 m box (or equivalent)
- Culvert/crossing upgrades for Maple Avenue crossing in combination with other alternatives for Site 33

## Preferred Management Approach:

- Upgrade Chartwell Road crossing
- See Site 33

### Potential Linkage to Adjacent Sites:

• Site 33

					able 7 Evaluation Resul	ts				
			Cater	gory Evaluation Pr	oducts					
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products
35	1.6	0.0	0.0	0.0	0.0	0.0	30.0	16.0	8.0	55.6

											Ro	oad Fi	oodin		able 4 od Cr		Evalu	uation	1																	
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation			lood I	Elevatio	ons (m	)			Road	d Floo	ding D	epth (m	1).			F	low Ve	locitie	es (m/s)			S	torm E	vent Fr	equen	cy Mod	ifiers		Storm Event Flooding Starts/ or Criteria Not Met	Storm Event Frequency Modifier Selected	Evaluation Scale Category Importance/ Significance	Product (Measure Weighting * Storm
OKC NO	Evaluation Scale Citiena	(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Rea	2	5	10	25	50	100 I	Rea	2	5	10	25	50	100	Rea	(2-100, Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significance
35	Design Flood Criteria	Arterial	10	93,47	92.7	93,0	93,5	93.6	93.7	93.7	93.6	0.0												0,7									Arterial / 1:100 - Reg	0.08	2	2
35	Private Vehicle	EMS Route	10	93,47																				0,7		- 1				0.04	.		None	0,00	5	0
35	Emergency Vehicle	EMS Route	10	93,47	92.7	93.0	93.5	93.6	93.7	93.7	93.6	0.0	0.0	0.0	0.2	0.2	0.3	0.1	0.0	0.0	0,0	0,7	0.7	0.7	0.6	1	0.4	0.2	80,0	0.04	0.02	0.01	None	0.0	6	0
35	Private Vehicle Acess to Facilities	Partial	0	93,47	92,7	93,0	93,5	93.6	93.7	93.7	93,6	0.0	0.0	0:0	0.2	0,2	0.3	0.1	0.0	0.0	0.0	0.7	0.7	0.7	0.6	1	0.4	0.2	80,0	0.04	0.02	0.01	Arterial / 1:100 - Reg	0.08	3	0
35	Emergency Vehicle Access to Facilities	Partial	0	93,47	92.7	93.0	93.5	93.6	93.7	93.7	93,6	0.0	0.0	0.0	0.2	0,2	0.3	0.1	0.0	0.0	0.0	0.7	0.7	0.7	0.6	ř	0.4	0.2	0.08	0.04	0.02	0.01	None	0.00	7	0
35	Private Vehicle Driveway Access (Multiuser)	Medium Vehicle Usage	0	93,47	92.7	93.0	93.5	93.6	93.7	93.7	93.6	00	0.0	0.0	0.2	0,2	0.3	0.1	0.0	0.0	0.0	0.7	0.7	0,7	0,6	1	0.4	0.2	0.08	0.04	0.02	0.01	None	0.00	4	0

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

	1																	Th	reat to L	Tabl ife Flood.	le 5 Criteria	Evaluatio	n																					
			Site Down	stream Flood E	levations (m)	)				Reside	ntial Units Flo	ooded (#)				Indust	rial Area (h	na)			Commer	rcial Area (h	a)		ln	stitutional (ha		Lan	d Use Dens /u	The state of the s	s/ha or		People	Endangere	ď		Slorm E	vent Fred	uency Mod	liters			Composite	
Site No	2	S	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5 1	0 25	50 100	) Reg	2 5	10	25 50	100 Re	eg 2	5 10	25 50	100	Reg Re	s Ind	Com (	Instit	2 5	10	25 50	100	Reg 2	5	10 25	5 50	100 Re	Normalized No eif People Using Storm Multipliers	Evaluation Scale Measure Weighting (1- 10)	Category Importance/ Significance (1-10 (7 - Day Usage) (10 - Day and Nigh Usage)	) Produc
35	92 69	93	93 51	93 64	93 69	93 74	93.61	0	0	3.	818	1:	2	30	0	0	0 0	0 0	0	0 0	0	0 0	0 0	0	0 0	0 0	0	0 3	125	90	40	0 0	3	3 3	6	3 50	20	10 4	2	1 0	55 2	3	10	30

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)
  2 Determine flooding conditions that results in life endangerment (separate spreadsheet direct damages). Note that for residential units, life endagerment has been included if the basement has been predicted to flood.
  3 Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)
  4 Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered
  5 Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm

- 6 Apply adjustment factor (Value of Step 5 divided by 10)
- 7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

Building No.	Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream 2-100/ Reg Flood Elevations (m)	Upstream 2- 100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
482 Maple Av		93.8	95.6	94.62	95,67	10	10	95.67	80.0	\$15,314.70	1	0
482 Maple Av		93.8	95.6	94_91	95.8	10	10	95.80	0.21	\$16,860,51	1	0
482 Maple Av	- 101	93.8	95.6	94,79	95,68	10	10	95.68	0.09	\$15,428.40	1	0
482 Maple Av	96.2	93.8	95.6	94.67	95.67	10	10	95,67	0.08	\$15,314.70	1	0
482 Maple Av		93.8	95.6	94.5	95.63	10	10	95,63	0.04	\$14,868.20	1	0
482 Maple Av		93.8	95.6	94.34	95.56	10 10 10	10	95.56	-100,00	\$0.00	0	0
482 Maple Av		93.8	95.6	93,93	94.79	10	10	94.79	-100.00	\$0.00	0	0
486 Maple Av		93.9	95.7	94.62	95.67	10	10	95.67	-100.00	\$0.00	0	0
486 Maple Av		93,9	95.7	94.91	95.8	10		95.80	0_11	\$15,658.34	1	0
486 Maple Av		93.9	95.7	94.79	95.68	10	10	95.68	-100.00	\$0.00	0	0
486 Maple Av		93.9	95.7	94.67	95.67	10	10	95.67	-100.00	\$0.00	0	0
486 Maple Av		93.9	95.7	94.5	95.63	10	10	95.63	-100.00	\$0.00	0	0
486 Maple Av		93.9	95.7	94.34	95.56	10	10	95.56	-100.00	\$0.00	0	0
486 Maple Av	96.3	93.9	95.7	93.93	94.79	10	10	94.79	-100.00	\$0.00	0	0
										Reg	1	0

Frequency	Summarized Damage Costs (\$)
Reg	\$15,314.70
100	\$32,518.85
50	\$15,428.40
25	\$15,314.70
10	\$14,868.20
5	\$0.00
2	\$0.00

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangered.

Table 6
Flooding Damages Evaluation Scale Category: Site Assessment

Site	Event			Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth (50 Year, 5%) Direct Damages	Measure Weight	Category Importance/ Significance	
	(Yr)	(m)	(No.)	(No.)	(No.)	(\$)	(ha)	(\$)	(ha)	(\$)	(ha)	(\$)	(\$)	(\$)	(\$)	(1-10)	(1-10)	
	2	92.69	0	0	0	\$0	0	0	0	0	0	0	so					
	- 5	93.00	0	0	Ö	so	0	0	0	0	0	0	\$0	[				
	10	93.51	1	Ĭ	Ö	\$14,868	0	0	0	0	0	0	\$14,868					
35	25	93.64	1	1	0	\$15,315	0	0	ő	0	0	0	\$15,315	\$2,439	\$44,524	2	8	16
	50	93.69	1	1	0	\$15,428	0	0	0	0	0	0	\$15,428					
	100	93.74	2	2	Ö	\$32,519	0	0	0	0	0	0	\$32,519					
	Reg	93.61	1	111	0	\$15,315	0	0	0	0	0	0	\$15,315					

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not
- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
- 4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
- 5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

Building No.	Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream 2-100/ Reg Flood Elevations (m)	Upstream 2-100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
482 Maple	96.2	93.8	95.6	94.62	95.67	10	10	95.67	0.08	\$15,314.70	1	
482 Maple	96.2	93.8	95.6	94.91	95.8	10	10	95.80	0.21	\$16,860.51	ľ	
482 Maple	96.2	93.8	95.6	94.79	95.68	10	10	95.68	0.09	\$15,428.40	i i	
482 Maple	96.2	93.8	95.6	94.67	95.67	10	10	95.67	0.08	\$15,314.70	i	
482 Maple	96.2	93.8	95.6	94.5	95.63	10	10	95.63	0.04	\$14,868.20	i	
482 Maple	96.2	93.8	95.6	94.34	95.56	10	10	95.56	-100,00	\$0.00	o.	
482 Maple	96.2	93.8	95.6	93.93	94.79	10	10	94.79	-100.00	\$0.00	ŏ	
486 Maple	96.3	93.9	95.7	94.62	95.67	10	10	95.67	-100.00	\$0.00	0	
486 Maple	96.3	93.9	95.7	94.91	95.8	10	10	95.80	0.11	\$15,658.34	Ĭ i	
486 Maple	96.3	93.9	95.7	94.79	95.68	10	10	95.68	-100.00	\$0.00	0	
486 Maple	96.3	93.9	95.7	94.67	95.67	10	10	95.67	-100.00	\$0.00	0	
486 Maple	96.3	93.9	95.7	94.5	95.63	10	10	95.63	-100.00	\$0.00	ő	
486 Maple	96.3	93.9	95.7	94,34	95.56	10	10	95.56	-100.00	\$0.00	ő	
486 Maple	96.3	93.9	95.7	93.93	94.79	10	10	94.79	-100.00	\$0.00	0	
								/ <del></del>		Reg	1	
										100	2	
										50	1	
										25	1	
										10	1	
										5	0	
										0		

\$4,878	
\$2,297	
	Summarized Direct Damage
	Costs (\$)
	\$15,314.70
	\$32,518,85
	\$15,428.40
	¢15 014 70

Average Annual

Damages 2007

**Indirect Damages** 

\$366

Total

Indirect Damage

Value

(\$)

\$0

\$0

\$2,230

\$2,297

\$2,314

Present Worth

(50 Year, 5%)

Indirect

Damages

(\$)

\$6,679

Category

Importance/

Significance

(1-10)

Product

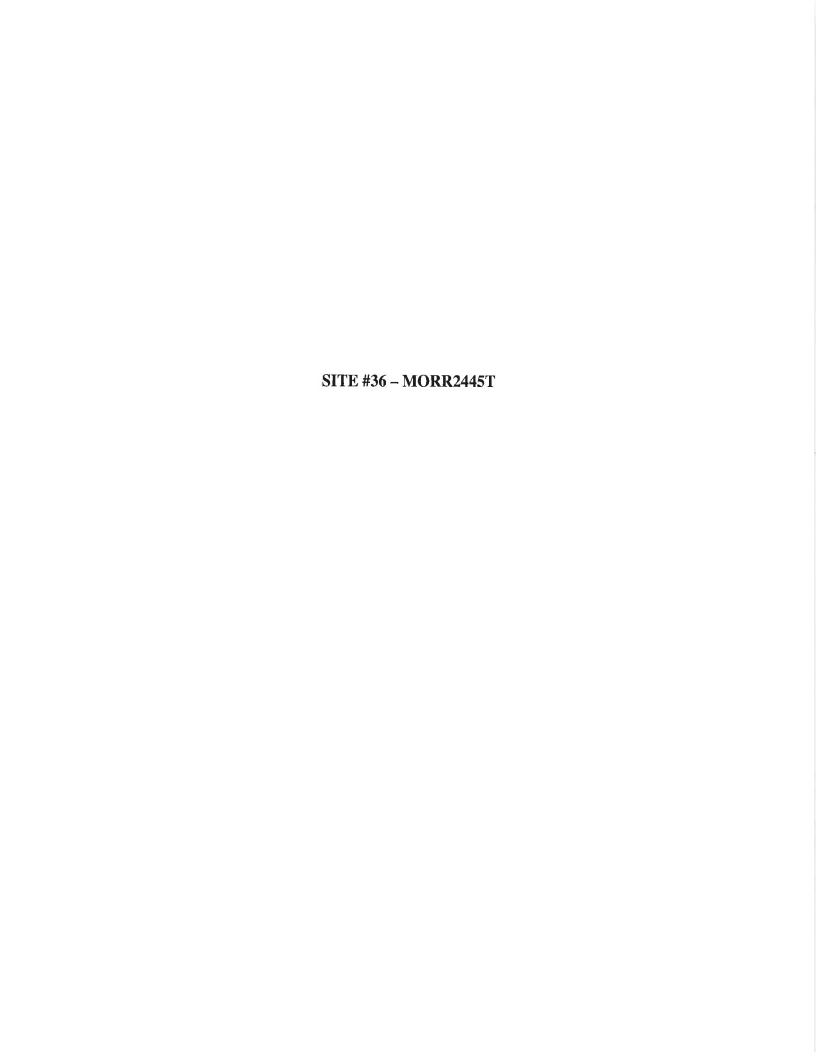
Measure

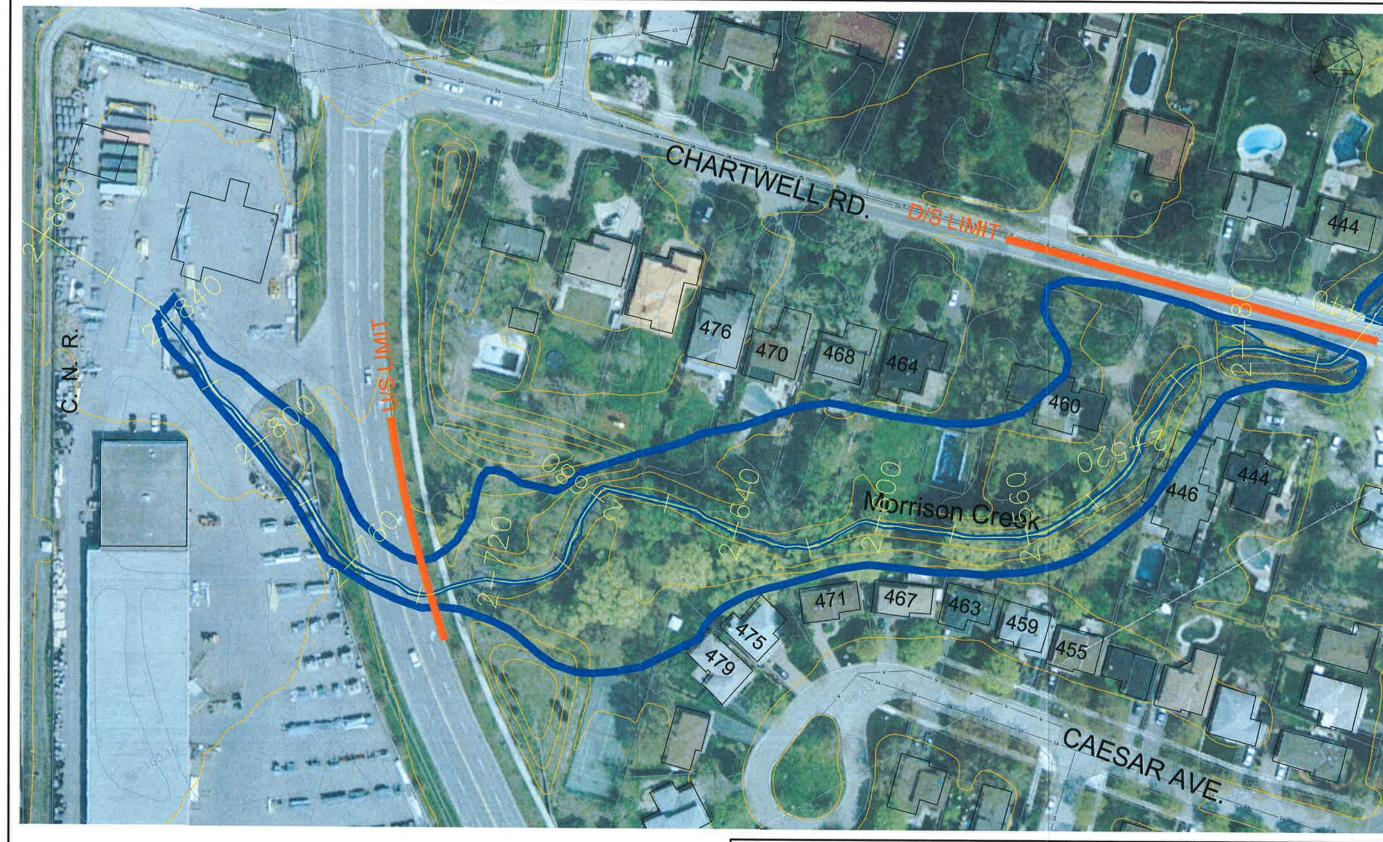
Weight

(1-10)

2

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine flooding damages for each return period based on the flooding depths and damage curve equations





LEGEND:

REGULATORY FLOODLINE

TOWNWIDE FLOODING STUDY

TOWN OF OAKVILLE

SITE # 36 - MORR2445T

MORRISON CREEK

	F
	ι
HILLOS	0/
ENGINEERING	F

	Project No.	106026
	Date	January 2008
-	Scale	1:1,000
G	Figure No.	36

# Site #36 (MORR2445T) Implementation Program

## Recommended Management Approach/Project Scope:

- Upgrade driveway crossing at 446 Chartwell Road, from 2.4 by 1.8 Elliptical CSP to 1.8 by 1.6 m+ box culvert or equivalent
- Flood proofing of 446, 460 Chartwell Road and 479 Caesar Avenue

## Appropriate Lead for Undertaking:

 Timing and phasing as per Town of Oakville Capital Works Program based on priority ranking established herein.

#### Governing Protocol Legislation:

- Town of Oakville's Policies and protocols
- Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
- Ministry of Natural Resources Lakes and Rivers Act
- Department of Fisheries and Oceans Fisheries Act
- Ministry of Environment Water Taking (required for damming and pumping operations)

#### Approval Requirements:

- Town of Oakville
- Conservation Halton Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Permit
- Regional Municipality of Halton for water and wastewater servicing alterations
- Ministry of Environment Permit to Take Water (should dam and pumping for creek diversion or dewatering be required)
- Potentially Department of Fisheries and Oceans (i.e. should a Harmful Alteration Disruption or Destruction (HADD) be identified to occur based on the proposed works)
- Input from Utility companies for utility locations

# Need for, and Scope of Follow-Up Assessment/Analysis:

- Detailed topographic survey of area
- Vegetation assessment
- Natural channel design assessment
- Hydraulic modeling refinement
- Approval process with private land owners

#### Suggested Timing, Need for Phasing:

 Timing of project dependant on Capital Works Program budget and priority of project within the Program.

#### Possible Implementation Issues:

- Private land owners consent to proposed grading
- Town of Oakville potential easement requirements
- Vegetation loss, requiring mitigation

# Possible Monitoring Requirements:

Potentially Department of Fisheries and Oceans monitoring requirements

#### Need for Maintenance:

- Potential vegetation replacement and seeding
- Potential creek stabilization resulting from local grading impacts
- Crossing maintenance

## Potential Interface with Other Town/Agency Programs:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Potential opportunities with Town's Creek Erosion Study and road work
- Potential projects already identified by Conservation Halton

#### Other Funding Opportunities:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Canada/ Ontario Municipal Renewal Infrastructure Fund
- Others

# Site #36 (MORR2445T) Specific Flood Management Alternative Assessment

# Data/Information:

# Flooding mechanisms:

- Driveway crossing for 446 Chartwell Road (2.4 m by 1.8 m Elliptical CSP)
- Floodplain capacity
- Encroachment

#### Screened Alternatives:

- Culvert upgrade for 446 Chartwell Road put in 1.8 m by 1.6 m+ box culvert
- Flood proofing of 446, 460 Chartwell Road and 479 Caesar Ave.
- Floodplain improvements are impractical due to private property and existing vegetation.

# Preferred Management Approach:

- Culvert upgrade
- Flood-proofing of 479 Caesar Avenue approximately 0.01 m. Topographic survey required to verify building elevation and flood proofing required.

## Potential Linkage to Adjacent Sites:

No linkage

Table 7	
Summary of Site Evaluation Results	
gory Evaluation Products	W

			Cater	gory Evaluation Pr	oducts					
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products
36	0.0	0.0	0.0	0.0	0.0	0.0	40.0	16.0	8.0	64

											Roa	d Floo		Table Flood (	-	ia Eva	luatio	n																
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation		F	lood El	evation	ns (m)			F	Road FI	ooding	Depth	(m)				Flow V	elocitie	es (m/s)			S	torm Ev	ent Fre	equency	Modifi	ers	Storm Event Flooding Starts/ or Criteria Not Met	Storm Event Frequency Modifier Selected	Evaluation Scale Category Importance/ Significance	Product (Measure Weighting * Storm
		(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50 1	100 R	eg 2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5	10 2	25 5	0 10	0 Reg	(2-100, Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significance
36	Design Flood Criteria	Arterial	10	94.66	93,8	93.9	94.0	94.1	94.2 9	14.3 94	1.0 0.0	0.0																		0,01		0.0	2	0
36	Private Vehicle	EMS Route	10	94,66	93.8	93.9	94.0	94.1	94.2	4.3 94	1.0 0.0	0.0	0.0	0,0	0.0	0,0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1	0.4	0.2 0.	.08 0.	0.0	0.01	None	0.0	5	0
36	Emergency Vehicle	EMS Route	10	94.66	93.8	93.9	94.0	94.1	94,2 9	4.3 94	0.0	0.0	0.0	0.0	0,0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1	0.4	0.2 0.	.08 0.	0.0	0.01	None	0.0	6	0
36	Private Vehicle Acess to Facilities	No	0	94.66	93.8	93,9	94.0	94.1	94.2 9	4.3 94	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0	0,0	0.0	0.0	0.0	1	0.4	0.2 0.	.08 0.	0.0	0.01	None	0.0	3	0
36	Emergency Vehicle Access to Facilities	No	0	94.66	93.8	93.9	94.0	94.1	94.2 9	4.3 94	0.0	0.0	0.0	0.0	0,0	0.0	0.0	0.0	0.0	0.0	0.0	0,0	0.0	0.0	1	0.4	0.2 0.	.08 0.0	0.0	0.01	None	0.0	7	0
36	Private Vehicle Driveway Access (Multiuser)	NA	0	94.66	93.8	93.9	94.0	94-1 9	94.2 9	4.3 94	-0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1	0.4	0.2 0.	.08 0.0	0.0	0.01	NA	0.0	4	

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

																		Threat	o Life F	Table 5 lood Criter	ia Evaluati	on																				
1			Site Downs	treem Flood E	levations (m)					Reside	ntial Units Flo	oded (#)				Industri	Area (ha)			Comr	norcial Area	(ha)		Pite	stitutional (h	1)	Lane	/u		or	Pec	ople Endar	pered		Store	m Event F	equency !	Modifiers			Composite	
ite No	2	5	10	25	50	160	Reg	2	5	10	25	50	100	Reg	2	s 10	25 5	100 A	log 2	5 10	25 5	100	Aug 2	5 1	25 5	0 100	Reg Res		Com Insti	t 2	5 1	0 25	50 10	00 Reg	2 5	10	25 50	100 A	No. o People U	weighting		( e/ (1-10) Pr (ge)
6	93.7	93.61	93.89	93.99	94.05	94 11	93.86	(1)	î	ñ	3	3	3	1	0	0 0	0 6	0	0 0	0 0	0 0	0	0 0	0 0	0 1	0	0 5	125	90 40	a	3 0	3 9	9 9	9 3	±0 20	10	4 2	1 0	.4 304.2	4	10	-

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)

  2 Determine flooding conditions that results in life endangerment (separate spreadsheet direct damages). Note that for residential units, life endagerment has been included if the basement has been predicted to flood.

  3 Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)

  4 Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered

  5 Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm

  6 Apply adjustment factor (Value of Step 5 divided by 10)

- 7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

Building No.	Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream 2-100/ Reg Flood Elevations (m)	Upstream 2 100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
446 Chartwell		93.9		95.33	95.9	60	20	95.52	-100.00	\$0.00	0	C
446 Chartwell	0.000	93.9		95.67	96.06	60	20	95.80	0.11	\$15,658.34	1	C
446 Chartwell	96.3	93.9		95.63	96.03	60	20)	95.76	0.07	\$15,239.36		C
446 Chartwell		93.9	95.7	95,56	95,98	60	20	95.70	0.01	\$14,541.90	- 1	C
446 Chartwell	96.3	93.9		95,27	95.92	60	20	95.49	-100.00	\$0.00	0	0
446 Chartwell	96.3	93.9		95.19	95.86	60	20	95.41	-100.00	\$0,00	0	C
446 Chartwell	96.3	93.9		94,88	95.81	60		95.19	-100.00	\$0.00	0	
460 Chartwell	96.5	94.1	95.9		95.9	60	50	95.81	-100.00	\$0.00	0	0
460 Chartwell		94.1	95.9	95,67	96.06	60	50	96.00	0.10	\$15,600.54	1	0
460 Chartwell	1 1 1 1 1 1 1	94.1	95.9		96.03	60	50	95.96	0.07	\$15,239.36	1	C
460 Chartwell	96,5	94.1	95.9		95.98	60	50	95.91	0.02	\$14,649.86	1	0
460 Chartwell	96.5	94.1	95.9	95.27	95.92	60	50	95.81	-100.00	\$0.00	0	0
460 Chartwell	96.5	94.1	95.9	95,19	95.86	60	50	95.75	100.00	\$0.00	0	0
460 Chartwell	96.5	94.1	95.9		95.81	60	50	95.66	-100.00	\$0.00	0	0
479 Caesar A	96.5	94.1	95.9	96.83	96.83	1	1	96.83	0.94	\$28,932.20	1	1
479 Caesar A	96.5	94.1	95.9	96,93	96.93	1	1	96.93	1,04	\$31,153.45	1	1
479 Caesar A	96.5	94.1	95.9	96.9	96.9	. 1	1	96.90	1.01	\$30,469.74	1	1
479 Caesar A	96.5	94.1	95.9	96.87	96.87	1	1	96.87	0.98	\$29,801.03	1	1
479 Caesar A	96.5	94.1	95.9	96.85	96.85	1	1	96.85	0.96	\$29,363.40	1	1
479 Caesar A	96.5	94.1	95.9	96.81	96.81	1	1	96.81	0.92	\$28,507.32	1	1
479 Caesar A	96.5	94-1	95.9	96.77	96.77	1	1	96.77	0.88	\$27,676.20		1

Frequency	Summarized Damage Costs (\$)
Reg	\$28,932.20
100	\$62,412,33
50	\$60,948.46
25	\$58,992.79
10	\$29,363,40
5	\$28,507.32
2	\$27,676,20

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-3 Determine basement floor elevation by substracting 2.44m from the first floor elevation

- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
  5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
  6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangered by flooding: 3 people for residential based the building incurring flooding.

Table 6	
Flooding Damages Evaluation Scale Category: Site Assessment	

Site	Event	WSEL	Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth (50 Year, 5%) Direct Damages	Measure Weight	Category Importance/ Significance	
	(Yr)	(m)	(No.)	(No.)	(No.)	(S)	(ha)	(\$)	(ha)	(\$)	(ha)	(S)	(S)	(S)	(S)	(1-10)	(1-10)	1
	2	92.69	0	0	0	so	0	0	0	0	0	0	80			1131. 111.331		<b></b>
	5	93.00	0	0	0	\$0	0	0	0	0	0	0	\$0		1 1			
	10	93.51	0	0	0	so	0	O	0	0	0	0	SO SO		1 1			
36	25	93 64	2	2	0	\$29,192	0	0	0	o o	0	0	\$29,192	\$2,308	\$42,130	2	a	16
	50	93.69	3	3	0	\$45,021	0	0	0	0	0	0	\$45,021		50.000			2.5
	100	93.74	3	3	0	\$46,127	0	0	0	0	0	0	\$46,127					
	Reg	93.61	0	0	0	S0	0	0	0	0	0	0	S0 S0					
					-								Total Indirect Damage	Average Annual Damages 2007	Present Worth (50 Year, 5%)	Measure	Category Importance/	

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not
- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
- 4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
- 5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

Building No.	Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream Reg Elevations	2-100/ Flood (m)	Upstream 2-100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Prop 100/ Reg Elevations	perty 2- Flood (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
446 Charty	96.3	93.9			95.33	95.9	60	20		95.52	-100 00	\$0.00	0	
446 Charty	96.3	93.9			95.67	96.06	60	20		95.80	0.11	\$15,658.34	ĭ	
446 Charty	96.3	93.9			95.63	96.03	60	20		95.76	0.07	\$15,239.36	1	
446 Charty	96.3	93.9	95.7		95.56	95.98	60	20		95.70	0.01	\$14,541.90	i i	
446 Charly	96.3	93.9			95.27	95.92	60	20		95.49	-100.00	\$0.00	0	
446 Charty	96.3	93.9	95.7		95.19	95.86	60	20		95.41	-100.00	\$0.00	o o	
446 Charty	96.3	93.9	95.7		94.88		60	20		95.19	-100.00	\$0.00	0	
460 Charty	96.5	94.1	95.9		95.33		60	50		95.81	-100,00	\$0.00	0	
160 Charty	96.5	94.1	95.9		95.67	96.06	60	50		96.00	0.10	\$15,600.54	1	
460 Charty 460 Charty	96.5 96.5	94.1	95.9		95.63		60	50		95.96	0.07	\$15,239.36	1	
460 Charty	96.5	94_1	95.9		95.56		60	50		95.91	0.02	\$14,649.86	1	
160 Charty		94.1	95.9		95.27	95.92	60	50		95.81	-100.00	\$0.00	0	
460 Charty	96.5 96.5	94.1	95.9		95 19	95.86	60	50	8	95.75	-100.00	\$0.00	0	
179 Caesa	97.5	94.1 95.1	95,9 96.9		94,88	95.81	60	50		95.66	-100.00	\$0.00	0	
179 Caes	97.5	95.1	96.9		96.83	96.83	1	1		96.83	-100.00	\$0.00	0	
79 Caes	97.5	95.1	96.9		96 93 96 9	96.93		1		96 93	0.04	\$14,868.20	1	
79 Caesa	97.5	95.1	96.9	ll.	96.87	96.9		1		96.90	0.01	\$14,541.90	-1	
79 Caesa	97.5	95.1	96.9		96.85	96.87		1		96.87	-100.00	\$0.00	0	
79 Caes	97.5	95.1	96.9		96.85	96.85	31	1		96.85	-100.00	\$0.00	0	
79 Caesa	97.5	95.1	96.9		96.77	96.81 96.77	3	1		96.81	-100,00	\$0.00	0	
- Daese	31.01	33-1	30.3		50.77	96.77	1	1		96.77	-100.00	\$0.00	0	
												Reg	.0	
												100	3	
												50	3	

Frequency		Summarized Damage Costs (\$)
	Reg	\$0.00
	100	\$46,127.09
	50	\$45,020,62
	25	\$29,191.76
	10	\$0.00
	5	\$0,00
	2	\$0.00

**Indirect Damages** 

(\$)

\$346

Indirect

amages

(\$)

\$6,320

Weight

(1-10)

Product

Significance

(1-10)

Value

**(S)** 

SO.

SO

SO

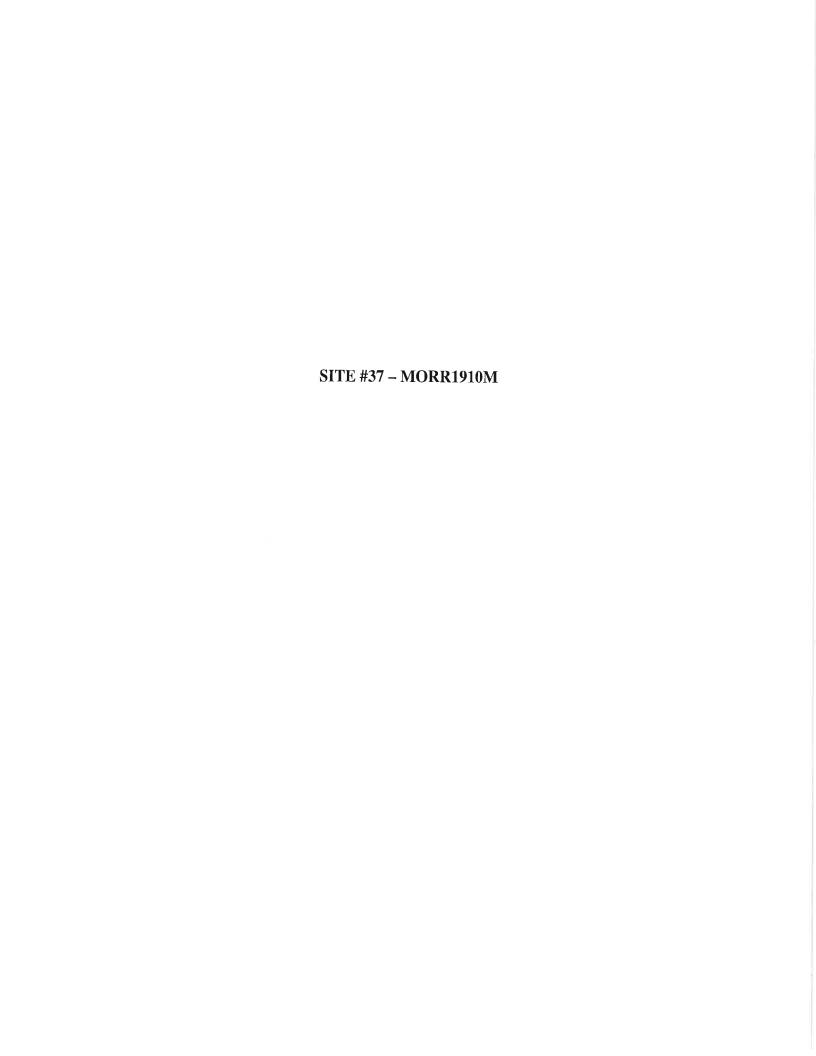
\$4,379

\$6,753

\$6,919

SO

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine flooding damages for each return period based on the flooding depths and damage curve equations





LEGEND:

REGULATORY FLOODLINE

TOWNWIDE FLOODING STUDY TOWN OF OAKVILLE SITE # 37 - MORR1910M MORRISON CREEK

ENGINEERING Figure No.

Project No. 106026 January 2008 Date 1:1,000 Scale 37

# Site #37 (MORR1910M) Implementation Program

# Recommended Management Approach/Project Scope:

- Flood control upstream of site (See Site 33)
- Upgrade Chartwell Road Culvert (Site 35) by adding 3 m by 1.6 m box culvert to existing 3 m by 1.6 m box culvert
- Flood proofing of 1020 Linbrook Road once Chartwell Road culvert upgraded

### Appropriate Lead for Undertaking:

• Timing and phasing as per Town of Oakville Capital Works Program based on priority ranking established herein.

#### Governing Protocol Legislation:

- Town of Oakville's Policies and protocols
- Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
- Ministry of Natural Resources Lakes and Rivers Act
- Department of Fisheries and Oceans Fisheries Act
- Ministry of Environment Water Taking (required for damming and pumping operations)

#### Approval Requirements:

- Town of Oakville
- Conservation Halton Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Permit
- Regional Municipality of Halton for water and wastewater servicing alterations
- Ministry of Environment Permit to Take Water (should dam and pumping for creek diversion or dewatering be required)
- Potentially Department of Fisheries and Oceans (i.e. should a Harmful Alteration Disruption or Destruction (HADD) be identified to occur based on the proposed works)
- Input from Utility companies for utility locations
- Approval from home owner for flood proofing

### Need for, and Scope of Follow-Up Assessment/Analysis:

- Class Environmental Assessment for assessing feasibility of upstream flood control
- As part of the EA
  - Hydrologic modeling refinement
  - o Hydraulic modeling refinement
  - Vegetation assessment
  - o Fisheries assessment
  - Natural channel design assessment
- Approval process with private land owners
- Detail design of flood control facility based on Class EA
- Revision to hydraulic modeling at Site 35 and assessment of reduced flows on flood impacts
- Topographic survey of crossing and creek to facilitate hydraulic modeling and detail design
- Hydraulic modeling of Site with proposed culvert addition once potential flood

#### Suggested Timing, Need for Phasing:

• Timing of project dependant on Capital Works Program budget and priority of project within the Program.

#### Possible Implementation Issues:

- Private land owners consent to proposed grading
- Town of Oakville potential easement requirements
- Vegetation loss, requiring mitigation

### Possible Monitoring Requirements:

Potentially Department of Fisheries and Oceans monitoring requirements

#### Need for Maintenance:

- Potential vegetation replacement and seeding
- Potential creek stabilization resulting from local grading impacts
- Crossing maintenance

# Site #37 (MORR1910M) Implementation Program

# Potential Interface with Other Town/Agency Programs:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Potential opportunities with Town's Creek Erosion Study and road work
- Potential projects already identified by Conservation Halton

# Other Funding Opportunities:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Canada/ Ontario Municipal Renewal Infrastructure Fund
- Others

# Site #37 (MORR1910M) Specific Flood Management Alternative Assessment

# Data/Information:

# Flooding mechanisms:

- Spill from Chartwell Road due to 3 m by 1.6 m box culvert
- Encroachment

#### Screened Alternatives:

- Upstream crossing upgrade (see Site 35)
- Flood proofing properties flooded on all sides, although 1020 Linebrook Road may be possible based on building elevations being verified through topographic survey.
- Acquisition 3 properties (costly)
- Regulate

## Preferred Management Approach:

- Upstream crossing (see Site 35)
- Flood proofing of 1020 Linbrook Road
- Regulate

## Potential Linkage to Adjacent Sites:

• Linkage to Site 35

					able 7					
				Summary of Site	Evaluation Resul	ts				
			Cater	gory Evaluation Pr	oducts					
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products
37	0	0	0	0	0	0	40	16	8	64

	I	<del></del>									R	oad Flo	oding	Tab Floo		eria Ev	aluatio	on																	
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation			Flood I	Elevati	ons (m	)			Road	Floodi	ng Depi	th (m)				Flow V	elocitie	es (m/s)			Sto	orm Ev	ent Fre	quency	y Modif	iers	Floodi	rm Event ng Starts/ or ria Not Met	Storm Event Frequency Modifler Selected	Evaluation Scale Category Importance/ Significance	Product (Measure Weighting Storm
		(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5 1	0 2	5 50	0 100	Reg	2	5	10	25	50	100 F	Reg	2	5	10 2	5 5	50 10	00 Re	eg (2-:	100, Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significanc
37	Design Flood Criteria	Not Applicable	NA	0.00	0.0	0.0	0_0	0.0	0.0	0.0	0.0	0.0	0.0 0.	.0 0.	0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1 0		0.2 0.					Applicable	0.0	2	0
37	Private Vehicle	Not Applicable	NA	0.00											- 1	- 1	1						0.0		- 1		0.2 0.					Applicable	0.0	5	0
37	Emergency Vehicle	Not Applicable	NA	0.00	0.0	0.0	00	0.0	0.0	0.0	0.0	0.0	0.0	0 0.	0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1 0	0,4	0.2 0.1	0.0	04 0.0	0.0	D1 Not	Applicable	0.0	6	0
37	Private Vehicle Acess to Facilities	Not Applicable	NA	0.00		H 111					- 1	- 11	1		- 1	10		1 1			1		0.0	1		0,4	0,2 0.0	0.0	04 0.0	0.0		Applicable	0.0	3	0
37	Emergency Vehicle Access to Facilities	Not Applicable	NA	0,00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0.	0.0	0.0	0.0	0.0	0,0	0.0	0.0	0.0	0.0	0.0	1 0	).4 C	0,2	0.0	04 0.0	0.0	O1 Not	Applicable	0.0	7	0
37	Private Vehicle Driveway Access (Multiuser)	Not Applicable	NA	0.00	11	0.0						- 1	- 1	- 1	- 10						- 11		0.0				0.2		100			Applicable	0.0	4	

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

																		Threat	to Life F	Table 5 lood Cri	teria Eval	uation																					
-			Site Downs	tream Flood E	levations (m)	).	-			Resid	dontial Units F	(8) bebool				Indust	rial Area (ha	)		Co	ommercial .	Area (ha)			Institutio	onat (ha)		Land	Use Densit or /un	ies (pers/ l lt)	na	Peop	le Endang	ered		Storm	Event Fr	requency M	dodillors			Composit	to
No.	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	6 1	0 25	50 100	Reg 2	5	10 25	50 1	OO Reg	2 5	10 25	5 . 50	100 Re	g Ros	Ind Co	om Insti	t 2	5 10	25	50 100	Rog	2 5	10	25 50	100 F	Normaliz No. of Per Using Sto Multiplie	Measure	Category Importance Significance ( (1- (7 - Day Usa (10 - Day and Usage)	e/ (1-10) age) Night
	89.11	89.2	89.28	89 37	89 43	89 48	89.47	0	0	2	2	2	2	0	0	0	0	0 0	0 0	0	0 0	0 0	0 0	0 0	0 0	0	0 0	3	125 9	0 40	0	0 6	6	6 6	0	50 20	10	4 2	1 74	4 102	4	10	_

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)
  2 Determine flooding conditions that results in life endangerment (separate spreadsheet direct damages). Note that for residential units, life endangerment has been included if the basement has been predicted to flood.
  3 Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)
  4 Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered
  5 Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered

- 5 Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm
- 6 Apply adjustment factor (Value of Step 5 divided by 10)
- 7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream 2-100/ Reg Flood Elevations (m)	Upstream 2 100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
93,2	90.8	92.6	92.36	92,55	80	80		-100.00	\$0.00	0	
93.2	90.8	92.6	92.4	92.8	80	80	92.80	0.21	\$16,860.51	1	
93.2	90.8	92.6	92.34	92.76	80	80	92.76	0.17	\$16,368.95	1	
93,2	90_8	92,6	92,27	92.72	80	80	92.72	0.13	\$15,891.72	1	10
93.2	90.8	92,6	92.16	92,65	80	80	92.65	0.06	\$15,089.80	1	((0
93.2	90.8	92,6	92.09	92.59	80	80	92.59	-100,00	\$0.00	0	
93.2	90.8	92,6	91.99		80	80	92.50	-100.00	\$0.00	0	- 10
93.2	90.8	92,6	92,55	92.55	1	1	92.55	-100,00	\$0.00	0	
93.2	90.8	92,6	92.8	92.8	1	1	92.80	0.21	\$16,860.51	Ĩ	(
93.2	90.8	92.6	92.76	92.76	1	1	92.76	0.17	\$16,368.95	1	- 0
93.2	90.8	92.6	92.72	92.72	1	1	92,72	0.13	\$15,891.72	1	
93.2	90.8	92,6	92.65	92,65	1	1	92.65	0.06	\$15,089.80	1	1
93.2	90.8	92.6	92,59	92,59	1	1	92.59	-100.00	\$0.00	0	(
93,2	90_8	92.6	92.5	92.5	1	1	92.50	-100.00	\$0.00	0	
93.9	91.5	93.3	92.55	92.55	1	1	92.55	-100.00	\$0.00	0	
93.9	91.5	93.3	92.8	92.8	1	1	92.80	-100.00	\$0.00	o	
93.9	91.5	93.3	92.76	92.76	1	1	92.76	-100.00	\$0.00	0	
93.9	91.5	93.3	92.72	92.72	1	1	92.72	-100.00	\$0.00	0	
93.9	91.5	93.3	92.65	92.65	1	1	92.65	-100.00	\$0.00	0	(
93.9	91.5	93.3	92.59	92.59	1	1	92.59	-100.00	\$0.00	0	1
93.9	91.5	93.3	92.5	92.5	1	. 1	92.50	-100.00	\$0.00	0	(

Frequency	Summarized Damage Costs (\$)
Reg	\$0.00
100	\$33,721.01
50	\$32,737.89
25	\$31,783.43
10	\$30,179.60
5	\$0.00
2	\$0.00

- 1 Determine flooding elevations for all storm events at buildings that potentially flood 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use) 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangered

Table 6
Flooding Damages Evaluation Scale Category: Site Assessment

Site	Event	100000000000000000000000000000000000000	Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth (50 Year, 5%) Direct Damages	Measure Weight	Category Importance/ Significance	
	(Yr)	(m)	(No.)	(No.)	(No.)	(\$)	(ha)	(\$)	(ha)	(\$)	(ha)	(\$)	(\$)	(\$)	(\$)	(1-10)	(1-10)	
	2	92.69	0	0	0	so	0	0	0	0	0	0	\$0	3,70,70			150	<u> </u>
	5	93.00	0	0	0	\$0	0	0	0	0	0	0	S0					
	10	93.51	2	2	0	\$30,180	0	0	0	0	0	0	\$30,180					
37	25	93.64	2	2	0	\$31,783	0	0	0	0	0	0	\$31,783	\$4,521	\$82,543	2	B	16
	50	93.69	2	2	0	\$32,738	o o	0	0	0	0	0	\$32,738	1				
	100	93.74	2	2	0	\$33,721	0	0	0	0	0	0	\$33,721					
	Reg	93.61	0	0	0	\$0	0	o	0	0	0	0	\$33,721					
											7,		Total	Average Annual	Present Worth		Category	

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not
- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
- 4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
- 5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Flood Elevations (m)	Upstream 2-100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2-100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Floodin (Yes/ No)
93.2	90.8	92.6		92.55	80	80	92.55	-100.00	\$0.00	0	
93.2	90.8	92.6		92.8	80	80	92.80	0.21	\$16,860.51	1	
93.2	90.8	92.6		92.76	80	80	92.76	0.17	\$16,368.95	i	l <sub>II</sub>
93.2	90.8	92.6		92.72	80	80	92.72	0.13	\$15,891.72	i	
93.2	90.8	92.6		92.65	80	80	92.65	0.06	\$15,089.80	i	
93.2	90.8	92.6			80	80	92.59	-100.00	\$0.00	ò	
93.2	90.8	92.6			80	80	92.50	-100.00	\$0.00	o o	1
93.2	90.8	92.6	92.55	92.55	1	1	92.55	-100,00	\$0.00	0	
93.2	90.8	92.6	92.8	92.8	1	1	92.80	0.21	\$16,860.51	Ĩ	ļ.,
93.2	90.8	92.6	92 76	92.76	1	1	92.76	0.17	\$16,368.95	1	
93.2	90.8	92.6	92.72	92.72	1	1	92.72	0.13	\$15,891.72	1	
93.2	90.8	92.6	92.65	92.65	1	1	92.65	0.06	\$15,089.80	1	
93.2	90.8	92.6	92.59	92.59	- 1	1	92.59	-100.00	\$0.00	o	
93.2	90.8	92.6		92.5	1	1	92.50	-100.00	\$0.00	o o	
93.9	91.5	93.3	92,55	92.55	1	- 1	92.55	-100.00	\$0.00	Ó	
93.9	91.5 91.5	93.3 93.3	92.8	92.8	- 1	1	92.80	-100.00	\$0.00	0	
93.9	91.5	93.3	92.76	92 76	1	1	92.76	-100.00	\$0.00	0	
93.9	91.5	93.3	92.72	92 72		1	92.72	-100.00	\$0.00	0	
93.9	91.5	93.3	92.65	92.65		1	92.65	-100.00	\$0.00	0	
93.9	91.5	93.3	92.59	92 59	1	1	92.59	-100.00	\$0.00	0	
93.9	91.51	93.3	92.5	92.5	1	1	92,50	-100.00	\$0.00	0	
									Reg	0	
									100	2	
									50	2	
									25	2	
									10	2	
									5	0	
									2		

Frequency		Summarized Damage Costs (\$)
	Reg	\$0.00
	100	\$33,721.01
	50	\$32,737.89
	25	\$31,783,43
	10	\$30,179,60
	.5	\$0.00
	2	\$0.00

**Indirect Damage** 

Value

(\$)

\$0

\$0

\$4,527

\$4,768

\$4,911

\$5,058

Importance/

Significance

(1-10)

Product

Measure

Weight

(1-10)

( 50 Year, 5%)

Indirect

Damages

(\$)

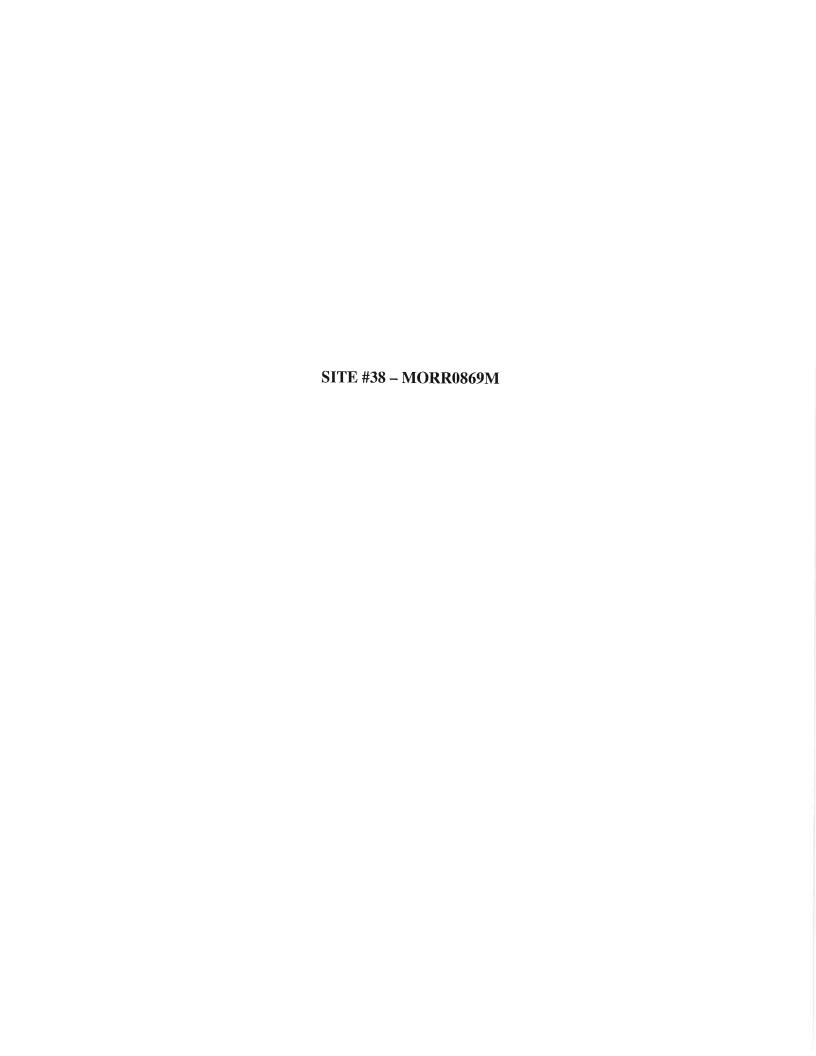
\$12,381

Damages 2007

**Indirect Damages** 

(\$)

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine flooding damages for each return period based on the flooding depths and damage curve equations





**LEGEND**:

REGULATORY FLOODLINE

TOWNWIDE FLOODING STUDY TOWN OF OAKVILLE SITE # 38 - MORR0869M MORRISON CREEK

	ŀ
	[
HILLOS	,
ENGINEERING	ı

	Project No.	106026
	Date	JAnuary 2008
ı	Scale	1:1,000
	Figure No.	38

#### Site #38 (MORR0869M) Implementation Program

# Recommended Management Approach/Project Scope:

- Flood control upstream of site (See Site 33)
- Upgrade Morrison Road crossing by twinning existing 3.6 m by 1.8 m box culvert

#### Appropriate Lead for Undertaking:

• Timing and phasing as per Town of Oakville Capital Works Program based on priority ranking established herein.

#### Governing Protocol Legislation:

- Town of Oakville's Policies and protocols
- Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
- Ministry of Natural Resources Lakes and Rivers Act
- Department of Fisheries and Oceans Fisheries Act
- Ministry of Environment Water Taking (required for damming and pumping operations)

#### Approval Requirements:

- Town of Oakville
- Conservation Halton Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Permit
- Regional Municipality of Halton for water and wastewater servicing alterations
- Ministry of Environment Permit to Take Water (should dam and pumping for creek diversion or dewatering be required)
- Potentially Department of Fisheries and Oceans (i.e. should a Harmful Alteration Disruption or Destruction (HADD) be identified to occur based on the proposed works)
- Input from Utility companies for utility locations

### Need for, and Scope of Follow-Up Assessment/Analysis:

- Class Environmental Assessment for assessing feasibility of upstream flood control controls
- As part of the EA
  - o Hydrologic modeling refinement
  - o Hydraulic modeling refinement
  - o Vegetation assessment
  - Fisheries assessment
  - o Natural channel design assessment
- Approval process with private land owners
- Detail design of flood control facility based on Class EA
- Revision to hydraulic modeling at Site 38 and assessment of reduced flows on flood impacts
- Topographic survey of crossing and creek to facilitate hydraulic modeling and detail design
- Hydraulic modeling of Site with proposed culvert addition once potential flood control upstream determined

#### Suggested Timing, Need for Phasing:

 Timing of project dependant on Capital Works Program budget and priority of project within the Program.

#### Possible Implementation Issues:

- Private land owners consent to proposed grading
- Town of Oakville potential easement requirements
- Vegetation loss, requiring mitigation

#### Possible Monitoring Requirements:

Potentially Department of Fisheries and Oceans monitoring requirements

#### Need for Maintenance:

- Potential vegetation replacement and seeding
- Potential creek stabilization resulting from local grading impacts
- Crossing maintenance

#### Potential Interface with Other Town/Agency Programs:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Potential opportunities with Town's Creek Erosion Study and road work
- Potential projects already identified by Conservation Halton

# Site #38 (MORR0869M) Implementation Program

# Other Funding Opportunities:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Canada/ Ontario Municipal Renewal Infrastructure Fund
- Others

# Site #38 (MORR0869M) Specific Flood Management Alternative Assessment

## Data/Information:

# Flooding mechanisms:

- Morrison Road crossing (3.6 m by 1.8 m concrete box) with Regional storm backwater of 1.05 m
- Floodplain capacity of approximately the 5 year storm (16.5 m<sup>3</sup>/s). Regional storm is 37.9 m<sup>3</sup>/s
- Encroachment

### Screened Alternatives:

- Crossing/culvert upgrades twin existing culvert
- Floodplain/channel improvements not practical due to private property and existing vegetation.
- Flood proofing only possible for 1 out of 2 flooded homes, therefore this does not resolve the flooding problem
- Acquisition would be expensive
- Regulate

# Preferred Management Approach:

• Crossing upgrades by twinning existing 3.6 by 1.8 m concrete box culvert

# Potential Linkage to Adjacent Sites:

 Spill occurs Morrison Road to Site 39 would be eliminated and 177 Morrison Road would be flooded.

			Coto	Summary of Site	able 7 Evaluation Resul	ts		71.		
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	rgory Evaluation Property Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products
38	0.6	0.5	0.2	0.0	0.4	0.2	20.0	16.0	8.0	46.0

											Ro	ad Fic	oding		le 4 d Crite	ria Eva	luatio	n																
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation			lood E	Elevatio	ons (m	)			Road	Floodi	ng Depti	ı (m)			F	low Ve	locitie	es (m/s)			Sto	orm Ev	ent Fred	luency	Modifi	ers	Storm Event Flooding Starts/ or Criteria Not Met	Storm Event Frequency Modifier Selected	Evaluation Scale Category Importance/ Significance	Product (Measure Weighting Storm
		(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5 10	0 2	5 50	100	Reg	2	5	10	25	50	100	Reg	2	5	10 2	5 50	10	0 Rec	(2-100. Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significance
38	Design Flood Criteria	Collector	8	82,44	81.7	82,0	82.2	82.7	82.7	82.8	82,9	0.0	0.0 0.	0 0	2 0.3	0.4	0.4	0.0								24 (	0.2 0.0	08 0.0	14 00	00.	1 Collector / 1:50-yr	0.04	2	0.6
38	Private Vehicle	EMS Route	10	J	1	82.0						- 1							- 1					- 1	1.	- 1		- 1			1	0.04	5	0.5
38	Emergency Vehicle	EMS Route	10	93.47	92.7	93.0	93.5	93.6	93,7	93.7	93,6	0.0	0.0	0 0.	2 0.3	0.4	0.4	0.0	0.0	0.0	0.7	0.7	0.7	0.6	1 (	0.4	0.2 0.0	0.0	4 00	0.0	1 None	0.0	6	
38	Private Vehicle Acess to Facilities	Partial	5	l .		93.0	- 1							- 1			1				- 1						0.2 0.0					0.00	3	0
38	Emergency Vehicle Access to Facilities	Partial	5	93,47	92,7	93.0	93.5	93.6	93.7	93.7	93.6	0.0	0.0	0 0.	2 0.3	0.4	0.4	0.0	0.0	0.0	0.7	0.7	0.7	0.6	1 (	14 (	0.2	18 0 0	4 00	2 001	I Reg	0.01	7	0.05
38	Private Vehicle Driveway Access (Multiuser)	Medium Vehicle Usage	6	1	1	93.0	- 1				- 1	- 1	- 1			110	1	100	- 1		- 1			~			0.2 0.0					0.01	4	0.35

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

																		1	Threat to	Ta Life Floo	ible 5 od Criteri	ia Evalua	tion																					
			Site Downs	ream Flood E	levetions (m)	6	_			Heside	ential Units Flo	oded (#)				Indu	strial Area	(ha)			Comm	nercial Area	(ha)		Jr.	nstitutional	l (ha)		and Use D	ensitles (pe /unit)	ers/ha or		People E	ndanger	ed		Storm E	vent Freq	quency Mod	diflers			Composite	
ite No	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	5	10 25	50	100 Reg	2	5 10	25 6	io 100	Reg 2	5 1	0 25	50 10	00 Fleg	Res Ind	Com	instit	2 5	10	25 50	100	Reg 2	5	10 25	5 50	100 Fis	Normalized (No. of Peop Using Storr Multipliers	Measure	Category Importance/ Significance (1- (7 - Day Usage (10 - Day and Ni Usage)	/ -10) / ie) light
3	82.78	82 75	82 68	82 59	81 53	81 61	81 35	0	0	0	ā	2	2	2	Ō	0	0 0	0	0 0	0	0 0	0	0 0	0 0	0 0	0 0	0 0	0	3 125	90	40	0 0	0	3 6	6	6 50	20	10 4	2	1 0	32.4	2	10	+

- Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)

  Determine flooding conditions that results in life endangerment (separate spreadsheet direct damages). Note that for residential units, life endagerment has been included if the basement has been predicted to flood.

  Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)

  Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered for each respective storm.

  Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm.

- 6 Apply adjustment factor (Value of Step 5 divided by 10)
  7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

Upstream 2 100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
82.87	80		1.7	0.177725	16467.62054	1	
82.84	80	75.0	82.8	0.1471	16098.76803	1	
82.76	80	75,0	82.8	0.0671	15173.74678	1	
82,69	80	75.0	82.7	-100	0	0	
82,38	80	75,0	82.4	-100	0	0	
82.11	80	75,0	82.1	-100	0	0	
81,75	80	75,0	81.8	-100	0	0	
82,83	1	1.0	82.8	0.23	17116.85891	1	
82.78	1	1.0	82.8	0.18	16495 35587	1	
82.68	1	1.0	82.7	80.0	15319.22965	1	
82.62	1	1.0	82.6	0.02	14654 19846	1	
82.53	1	1.0	82.5	-100	0	0	
82.45	1	1.0	82.5	-100	0	0	
82.22	1	1.0	82.2	-100	0	0	
					Reg	2	
					100	2 2	
					50	2	

Frequency	Summarized Damage Costs (\$)
Reg	\$33,584,48
100.00	\$32,594.12
50.00	\$30,492,98
25.00	\$14,654.20
10.00	\$0.00
5.00	\$0.00
2.00	\$0.00

- 1 Determine flooding elevations for all storm events at buildings that potentially flood 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangered.

Table 6
Flooding Damages Evaluation Scale Category: Site Assessment

Site	Event	WSEL	Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth ( 50 Year, 5%) Direct Damages	Measure Weight	Category Importance/ Significance	
	(Yr)	(m)	(No.)	(No.)	(No.)	(\$)	(ha)	(\$)	(ha)	(\$)	(ha)	(\$)	(\$)	(\$)	(\$)	(1-10)	(1-10)	1
	2	92.69	0	0	0	\$0	0	0	0	0	0	0	\$0					
	5	93.00	0	0	0	\$0	0	0	0	0	0	0	\$0	<del> </del>				
	10	93,51	0	0	0	\$0	0	0	0	0	0	0	\$0					
38	25	93,64	1	1	0	\$14,654	0	0	0	0	0	0	\$14,654	\$1,539	\$28,099	2	8	16
	50	93.69	2	2	0	\$30,493	0	0	0	0	0	0	\$30,493	1 mg/c 5000m/m0				
	100	93.74	2	2	0	\$32,594	0	0	0	0	0	0	\$32,594	İ				
	Reg	93,61	2	2	0	\$33,584	0	0	0	0	0	0	\$33,584		1			
												•	Total	Average Appual	Present Worth		Cotocour	

Total

**Indirect Damage** 

Value

(\$)

\$0

\$0

\$0

\$2,198

\$4,574

\$4,889

\$5.038

**Average Annual** 

Damages 2007

Indirect Damages

\$231

(50 Year, 5%)

Indirect

**Damages** 

(\$)

\$4,215

Category

Importance/

Significance

(1-10)

**Product** 

Measure

Weight

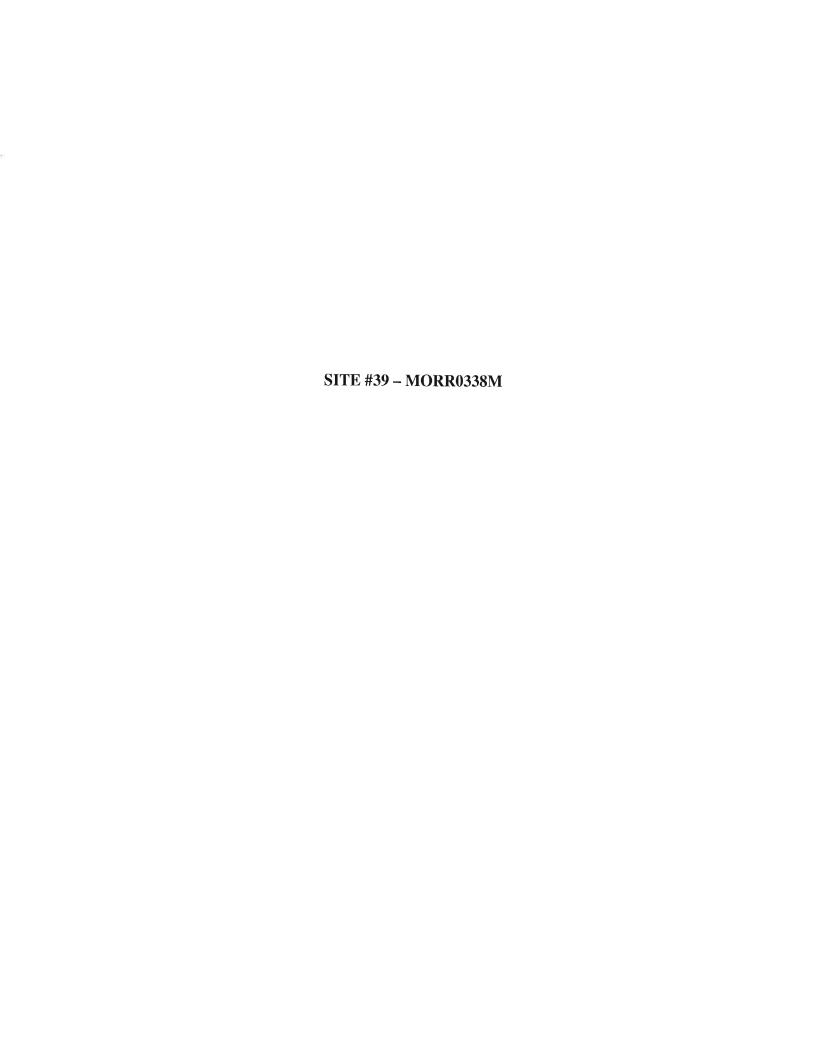
(1-10)

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not
- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
- 4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
- 5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

Upstream 2-100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstrea m Section	Interpolate d Property 2-100/ Reg Flood Elevations (m)		Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
82.87	80	75.0		0,177725	16467 62054	1	
82.84	80	75.0		0.1471	16098.76803	1	Č
82.76	80	75.0		0.0671	15173.74678	1	i i
82.69	80	75.0		-100	0	0	d
82.38	80	- 10		-100	0	0	Ċ
82.11	80	75.0		-100	0	0	(
81.75	80	75.0		-100	0	0	(
82.83	1	1.0		0.23		1	(
82.78	1	1.0	- 955	0.18	16495.35587	1	
82.68	1	1.0		0.08	15319.22965	1	
82.62	1	1.0		0.02	14654,19846	1	
82,53	1	1.0		-100		0	:.0
82.45	1	1.0	82.5	-100	(29)	0	((0
82,22	1	1.0	82.2	-100		0	0
					Reg	2	0
					100	2	d
					50	2	0
					25	1	0
					10	0	- 0
					5	0	0
					2	0	0

Frequency	Summarized Damage Costs (\$)
Reg	\$33,584.48
100.00	\$32,594,12
50.00	\$30,492,98
25.00	\$14,654.20
10.00	\$0.00
5.00	\$0.00
2.00	\$0.00

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine flooding damages for each return period based on the flooding depths and damage curve equations





Feb 11/08 - avogt

39

# Site #39 (MORR0338M) Implementation Program

# Recommended Management Approach/Project Scope:

- Flood control upstream of site (See Site 33)
- Upgrade Morrison Road crossing by twinning existing 3.6 m by 1.8 m box culvert (Site 38)

#### Appropriate Lead for Undertaking:

• Timing and phasing as per Town of Oakville Capital Works Program based on priority ranking established herein.

#### Governing Protocol Legislation:

- Town of Oakville's Policies and protocols
- Conservation Halton's Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Regulations
- Ministry of Natural Resources Lakes and Rivers Act
- Department of Fisheries and Oceans Fisheries Act
- Ministry of Environment Water Taking (required for damming and pumping operations)

#### Approval Requirements:

- Town of Oakville
- Conservation Halton Development; Interference with Wetlands and Alteration to Shorelines and Watercourse Permit
- Regional Municipality of Halton for water and wastewater servicing alterations
- Ministry of Environment Permit to Take Water (should dam and pumping for creek diversion or dewatering be required)
- Potentially Department of Fisheries and Oceans (i.e. should a Harmful Alteration Disruption or Destruction (HADD) be identified to occur based on the proposed works)
- Input from Utility companies for utility locations
- Home owner's approval for flood proofing

## Need for, and Scope of Follow-Up Assessment/Analysis:

- Class Environmental Assessment for assessing feasibility of upstream flood control controls
- As part of the EA
  - o Hydrologic modeling refinement
  - o Hydraulic modeling refinement
  - o Vegetation assessment
  - o Fisheries assessment
  - o Natural channel design assessment
- Approval process with private land owners
- Detail design of flood control facility based on Class EA
- Revision to hydraulic modeling at Site 39and assessment of reduced flows on flood impacts
- Topographic survey of crossing and creek to facilitate hydraulic modeling and detail design
- Hydraulic modeling of Site with proposed culvert addition once potential flood control upstream determined

#### Suggested Timing, Need for Phasing:

• Timing of project dependant on Capital Works Program budget and priority of project within the Program.

#### Possible Implementation Issues:

- Private land owners consent to proposed grading
- Town of Oakville potential easement requirements
- Vegetation loss, requiring mitigation
- Home owner's approval for flood proofing

### Possible Monitoring Requirements:

Potentially Department of Fisheries and Oceans monitoring requirements

### Need for Maintenance:

- Potential vegetation replacement and seeding
- Potential creek stabilization resulting from local grading impacts
- Crossing maintenance

# Site #39 (MORR0338M) Implementation Program

# Potential Interface with Other Town/Agency Programs:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Potential opportunities with Town's Creek Erosion Study and road work
- Potential projects already identified by Conservation Halton

# Other Funding Opportunities:

- To be discussed/ determined with the Town of Oakville and Conservation Halton
- Canada/ Ontario Municipal Renewal Infrastructure Fund
- Others

# Site #39 (MORR0338M) Specific Flood Management Alternative Assessment

# Data/Information:

# Flooding mechanisms:

- Channel/floodplain capacity just under the Regional flow of 20.6 m<sup>3</sup>/s
- Spill across Morrison Road from Site No. 38

#### Screened Alternatives:

- Floodplain/channel improvements system is natural and exhibits good grading improvements would not provide substantial reduction in flooding
- Flood proofing of 177 Morrison Road
- · Spill reduction at Morrison Road

# Preferred Management Approach:

- Flood proofing of 177 Morrison Road, topographic survey required to verify building elevation and flood proofing required following spill reduction/elimination
- Spill reduction see Site No. 38

# Potential Linkage to Adjacent Sites:

Site 38 and 39 are linked due to spill over Morrison Road

Table 7	
<b>Summary of Site Evaluation Results</b>	
ory Evaluation Products	

Catergory Evaluation Products										T
Site	Road Crossings	Private Vehicle Access	Emergency Vehicle Access	Private Vehicle Access to Facilities	Emergency Vehicle Access to Facilities	Private Multi- user Driveway Access	Threat to Life	Direct Damages	Indirect Damages	Combined Products
39	0	0	0	0	0	0	0	0	0	0

												Road	Flood		able 4	-	a Eval	uatior												-						
Site No	Evaluation Scale Criteria	Evaluation Scale Measure	Measure Weight	Road/ Driveway Elevation			Flood	l Eleva	tions (r	m)			Ro	ad Flo	oding C	Depth (	m)			F	low Ve	locitie	es (m/s)			Si	torm E	vent Fre	equency	/ Modif	iers		Storm Event Flooding Starts/ or Criteria Not Met	Storm Event Frequency Modifier Selected	Evaluation Scale Category Importance/ Significance	Product (Measure Welghting * Storm
		(Road Classification/ Storm frequency)	(4,6,8,10)	(m)	2	5	10	25	50	100	Reg	2	5	10	25	50	100	Rea	2	5	10	25	50	100	Rea	2	5	10	25 5	6 1	00 B	nes	(2-100, Reg)	(0.4-50)	(1-10)	Frequency Modifier * Category Significance
39	Design Flood Criteria	Arterial	10	80.08	77.0	77-1	77.3	77.4			77.7													0.0					08 0				None	0.0	2	Significance
39	Private Vehicle	EMS Route	10	80.08	1					7.	77.7	00	1 ° 1	- ^^	A2 1	725										- 1	1		08 0				None	0.0	5	0
39	Emergency Vehicle	EMS Route	10	80.08	77.0	77.1	77.3	77.4	77.5	77.6	77.7	0,0	0,0	0,0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1	0.4	0,2 0	.08 0.	04 0,	02 0,	,01	None	0.0	6	0
39	Private Vehicle Acess to Facilities	None	0	80.08	77.0	77.1	77.3	77.4	77.5	77.6	77.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4	0,4	0.2	.08 0.	04 0.	02 0.	.01	None	0.0	3	0
39	Emergency Vehicle Access to Facilities	None	0	80.08	77.0	77.1	77.3	77.4	77.5	77.6	77.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1	0.4	0.2 0	.08 0.	04 0.	02 0.	.01	None	0.0	7	0
39	Private Vehicle Driveway Access (Multiuser)	NA NA	0	80.08	77.0	77.1	77.3	77.4	77.5	77.6	77.7	00	0.0	00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1	0_4	0.2 0	.08 0.	04 0	02 0	01	None	0.0	4	0

### **Evaluation Process**

- 1 Determine road crossing classification, whether urban local, collector etc. and then determine the appropriate design storm criteria (2-100, Regional)
- 2 Apply appropriate Evaluation Scale Weight (1-10), (ref. Table 1), i.e. Level 1 Roads have a Measure Weight of 10.
- 3 Determine lowest road elevation at crossing
- 4 Determine flood elevations for the 2-100 year storm events and Regional storm Hurricane Hazel
- 5 Calculate road crossing flow depths and flow velocities for all storm events that result in road flooding
- 6 For Evaluation Scale Criteria (Design Flood Criteria), determine for which storm event flooding occurs and the appropriate road design storm criteria
- 7 For the Evaluation Scale Criteira (Design Flood Criteria), determine the appropriate Storm Event Frequency Modifier for the Design Flood Evaluation Scale Criteria (0.4-50)
- 8 For the Design Flood Evaluation Scale Criteria calculate product of the Evaluation Scale Measure Weight, Stom Event Frequency Modifier, and the Evaluation Scale Catergory Significance
- 9 For both Private and Vehicle Passage, determine what storm event flooding conditions commence that prevent vehicle passage for the crossing, and then apply the appropriate Storm Event Frequency Modifier
- 10 For private and emergency vehicle access to government facilities determine if flooding conditions preclude access based on flooding depth and velocities
- 11 For Private vehicle driveway access to muilt-user land uses (schools, malls etc.) determine flooding depths and velocities at driveway entrance to property
- 12 For both Private and Vehicle Passage Evaluation Scale Criterion, calculate the product of the Evaluation Scale Measure Weight, Storm Event Frequency Modifier and the Evaluation Scale Category Significance

																		Thre	at to Life	Table e Flood (	5 Criteria E	valuation	,																					
			Site Downs	tream Flood E	levations (m)	)			1	Resid	ential Units Flo	ooded (#)				Indus	trial Area (I	ia)		09	Commerci	al Area (ha	1		te	stitutional	(ha)		Land Use	Densities ( Aunit)	pers/ha or		Peop	e Endange	red		Storm	Event Fr	equency !	Modifiers			Composit	
No	2	959	10	25	50	100	Reg	2	5	10	25	50	100	Reg	2	s	10 25	50 100	Reg	2 5	10	e5 So	100 86	eg 2	5 1	0 25	50 10	0 Reg	Res Ir	id Com	Instit	2 !	5 10	25 5	50 100	Reg	2 5	10	25 50	100 R	Normaliz No. of Pec Using Sto Multiplie	ed Evaluation Scale Measure Weighting 10)		1-10)
	76.98	77.13	77.26	77.42	77.51	77.6	77 65	0	0	0	0	0	0	0	0	0	0 0	0 0	0	0 0	0	0 0	0 0	0 0	0 0	0	0 0	0	3 1	25 90	40	0 (	0 0	0 (	0 0	0	50 20	10	4 2	1 0	4 0	0	10	-

# **Evaluation Process**

- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet direct damages ref. below)
  2 Determine flooding conditions that results in life endangerment (separate spreadsheet direct damages). Note that for residential units, life endagerment has been included if the basement has been predicted to flood.
  3 Determine number of people endangered based on land use population densities and flooding conditions. For residential -= 3 people/home for Non Residential related to building size (ref. Table 5)
- 4 Determine number of people endangered for each storm event. Apply appropriate Evaluation Scale Measure Weight for that frequency event based on the number of people endangered 5 Determine normalized number of people endangered for all storm events using the Storm Event Frequency Modifiers multiplied by number of endangered people for each respective storm
- 6 Apply adjustment factor (Value of Step 5 divided by 10)
- 7 Determine the product of the Ajusted No. of People times Measure Weight and the Evaluation Scale Category Significance

Building No.	Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Downstream 2-100/ Reg Flood Elevations (m)	Upstream 2 100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2- 100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basement Flooding (Yes/ No)	First Floor Flooding (Yes/ No)	Frequency	Summarized Damage Costs (\$)
1268 Cambrid		78.9	80.7	78.31	78,31	1	1	78.31	-100.00	\$0.00	0	0	Reg	\$0.00
1268 Cambrid		78.9	80.7	78,2	78.2	1	1	78.20	-100.00	\$0.00	0	0	100	
1268 Cambrid	81.3	78.9	80.7	78	78	1	1	78.00	-100.00	\$0.00	0	0	50	
1268 Cambrid	81.3	78.9	80.7	77.72	77,72	1	1	77.72	-100.00	\$0.00	0	0	25	\$0.00
1268 Cambrid	81,3	78,9	80.7	77.49	77.49	1	1	77.49	-100.00	\$0,00	0	0	10	\$0.00
1268 Cambrid	81.3	78.9	80.7	77.32	77.32	1	1	77,32	-100.00	\$0.00	0	0	5	\$0.00
1268 Cambrid	81.3	78,9	80.7	77.13	77.13	1	. 1	77.13	-100.00	\$0.00	0	0	2	\$0.00
1249 Lakesho	82.1	79.7	81.5	79,12	79.64	140	118	79.56	-100.00	\$0.00	0	0		
1249 Lakesho	82.1	79.7	81.5	79.05	79,63	140	118	79.54	-100.00	\$0.00	0	0		
1249 Lakesho	82.1	79.7	81.5	78.87	79.58	140	118	79,47	-100.00	\$0.00	0	0		
1249 Lakesho	82.1	79.7	81.5	78.64	79.56	140	118	79,42	-100.00	\$0.00	0	0		
1249 Lakesho	82.1	79.7	81.5	78,27	79.5	140	118	79,31	-100.00	\$0.00	0	0		
1249 Lakesho	82.1	79.7	81.5	77.84	79.46	140	118	79.21	-100,00	\$0.00	0	0		
1249 Lakesho	82,1	79.7	81.5	77.74	79.43	140	118	79.16	-100.00	\$0.00	0	0		
169 Morrison	83.4	81.0	82.8	81.36	81.82	80	22	81.37	-100.00	\$0.00	0	0		
169 Morrison	83.4	81.0	82.8	81,3	81.75	80		81.31	-100.00	\$0.00	0	0		
169 Morrison	83.4	81.0	82.8	81.19	81.61	80		81.20	-100.00	\$0.00	0	0		
169 Morrison	83.4	81.0	82.8	81.06	81.58	80		81.07	-100.00	\$0.00	0	0		
169 Morrison	83.4	81.0	82.8	80.89	81.4	80		80.90	-100.00	\$0.00	0	0		
169 Morrison	83.4	81.0	82.8	80.75	81.19	80		80.76	-100.00	\$0.00	0			
169 Morrison	83.4	81.0	82.8	80.6	80.99	80		80.60	-100.00	\$0.00	0	0		
177 Morrision	82.5	80.1	81.9	81.36	81.82	80	70	81.76	-100.00		0	0		
177 Morrision	82.5	80.1	81.9	81.3	81.75	80	70	81.69	-100.00	1 10	0	0		
177 Morrision	82,5	80.1	81.9	81.19	81.61	80	70	81.56	-100.00	\$0.00	0	0		
177 Morrision 177 Morrision	82.5	80.1	81.9	81,06	81.58	80	70	81.52	-100.00	\$0.00	0	0		
177 Morrision	82.5	80.1	81.9	80.89	81.4	80	70	81.34	-100.00	\$0.00	0	0		
177 Morrision	82.5 82.5	80.1	81.9	80.75	81.19	80	70	81.14	-100.00	\$0.00	0	0		
185 Morrision	82.5	80.1	81.9	80.6	80.99	80	70	80.94	-100.00	\$0.00	0	0		
185 Morrision	82.9	80.5 80.5	82.3	81.36	81.82	80	70	81.76	-100.00	\$0.00	0	0		
185 Morrision	82.9	80.5	82.3	81.3	81.75	80	70	81.69	-100.00	\$0.00	0	0		
185 Morrision	82.9	80.5	82.3	81,19	81.61	80	70	81.56	-100,00	\$0.00	0	0		
185 Morrision	82.9	80.5	82.3	81.06	81.58	80	70	81.52	-100.00	\$0.00	0	0		
185 Morrision	82.9	CONTROL (CONTROL (CON	82.3	80.89	81.4	80	70	81.34	-100.00	\$0.00	0	0		
185 Morrision	82.9	80.5 80.5	82.3	80.75	81.19	80	70	81:14	-100.00	\$0.00	0	0		
100 MONISION	02.9	60.5	82.3	80,6	80.99	80	70	80.94	-100.00	\$0.00	0	0		
										Reg	0	0		
										\$100.00	0	0		
										\$50.00	0	0		
										\$25.00	0	0		
										\$10.00	0	0		
										\$5.00	0	0		
								I		\$2,00	0	0		

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine the number of people endangered by flooding: 3 people for residential based the building incurring flooding, other land uses require certain flood depths and velocities for life endangered.

# Table 6 Flooding Damages Evaluation Scale Category: Site Assessment

Site	Event		Homes	Basement Flooding	First Floor	Residential Damage Value	Industrial Area	Industrial Damage Value	Commercial Area	Commercial Damage Value	Institutional Area	Institutional Damage Value	Total Direct Damage Value	Average Annual Damages 2007 Direct Damages	Present Worth ( 50 Year, 5%) Direct Damages	Measure Weight	Category Importance/ Significance	Produc
	(Yr)	(m)	(No.)	(No.)	(No.)	(\$)	(ha)	(S)	(ha)	(S)	(ha)	(S)	(S)	(\$)	(\$)	(1-10)	(1-10)	ĺ
ļ	2	92.69	0	0	0	\$0	0	0	0	0	0	0	\$n	0.00		CANCEL SAFE	MC1-1B6	
ļ	5	93.00	.0	0	0	S0	0	0	0	0	0	0	50					
	10	93.51	0	0	2	\$0	0	0	0	0	0	0	\$0		1			
39	25	93.64	0	0	3	SO	0	0	0	0		.0	\$0	80	so	2	2	1 2
	50	93.69	0	0	3	\$0	0	0	,		0	0	\$0	300	30	9		.9
	100	93.74	0	0	В	\$0	0	0		0		0	\$0					
	Reg	93.61	0	0	22	\$0	0	0	0	.0	0	0	\$0					
									9			0	Total	Average Annual	Present Worth		Category	

# **Evaluation Process**

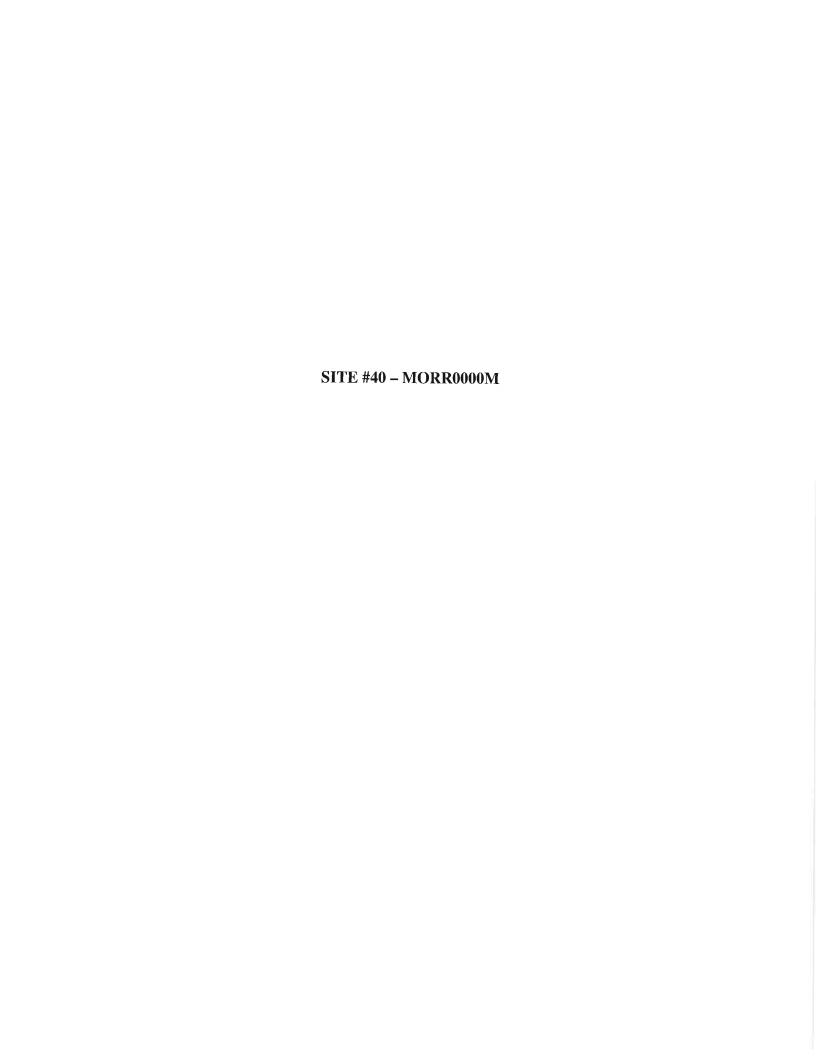
- 1 Determine flooding conditions for all buildings within the site, depth of flooding and velocities (separate speadsheet)
- 2 Determine flooding conditions that results in direct damages (separate spreadsheet direct damages) related to whether building is subjected to flooding or not
- 3 Determine The Total Value for Direct Damages and Indirect Damages (15% of Direct Damages)
- 4 Determine Average Annual Damages (AAD) for Direct and Indirect damages
- 5 Determine Present Value based on AAD and Engineering Lifetime of 50 Years and Discount Rate of 5% for Direct and Indirect Damages (for information purposes only)
- 6 Determine the product of the Measure Weight and the Evaluation Scale Category Significance for Direct and Indirect Damages

			In .								
Finished Floor Elevation (m)	Basement Floor Elevation (m)	Lowest Opening (m)	Flood Elevations (m)	Upstream 2-100/ Reg Flood Elevations (m)	Section Distance	Distance from Downstream Section	Interpolated Property 2-100/ Reg Flood Elevations (m)	Building Flood Depth (m)	Damage Costs (\$)	Basemenl Flooding (Yes/ No)	First Floor Flooding (Yes/ No)
81.3	78,8616	80.7	78.3	78.31	1	1	78.31	-100,00	0.00	PO 00	
81,3	78,8616	80.7	78.2	78.2	1	3	78.2	-100.00	0.00	\$0.00	1
81.3	78.8616	80.7	78.0	78	1	i i	78		0.00	\$0.00 \$0.00	
81,3	78 8616	80.7	77.7	77.72	. 1	l i	77.72	-100.00	0.00	\$0.00	
81,3	78.8616	80.7	77.5	77,49	1	1	77.49	-100.00	0.00	\$0.00	
81.3	78.8610	80.7	77.3	77.32	1	1	77,32	-100.00	0.00	\$0.00	
81.3	78.8616	80.7	77.1	77.13	1	1	77.13	-100.00	0.00	\$0.00	
82.1	79,6616	81.5	79.1	79.54	140	118	79,55828571	-100.00	0.00	\$0.00	
82.1 82.1	79 6616	81.5	79.1	79.63	140	118	79.53885714	-100.00	0.00	\$0.00	
82.1	79.6616	81.5		79.58	140	118	79.48842857	-100 00	0.00	\$0.00	
82,1	79.6616	81.5	78.6	79.56	140	118	79.41542857	-100.00	0.00	\$0.00	
82.1	79.6616 79.6616	81.5		79.5	140	118	79.30671429	-100_00	0.00	\$0.00	
82.1	79.6616	81.5	77.8	79.46	140	118	79.20542857	-100.00	0.00	\$0.00	
83.4	80.9616	81.5	77.7 81.4	79.43	140	118	79.16442857	-100,00	0.00	\$0.00	
83.4	80 9616	82.8	81.3	81.82	80	1	81,36575	-100,00	0.00	\$0.00	
83.4	80 9616	82.8	81.2	81,75	80	1	81.305625	-100.00	0.00	\$0.00	
83.4	80 9616	82.8	81.1	81,61	80	1	81.19525	-100.00	0.00	\$0.00	
83.4	80.9616	82.8	80.9	81.58	80	- 1	81.0665	-100.00	0,00	\$0.00	
83.4	80.9616	82.8	80.8	81.4 81.19	80	1	80.896375	-100.00	0.00	\$0.00	
83.4	80.9616	82.8	80.6	80.99	80	1	80.7555	-100.00	0.00	\$0.00	
82.5	80,0616	81.9	81.4	81.82	80	1	80.604875	-100.00	0.00	\$0.00	
82.5	80.0616	81.9	81.3	81.75	80 80	70	81,7625	-100.00	0.00	\$0.00	
82.5	80,0616	81.9	81.2	81,61	80	70	81.69375	-100.00	0.00	\$0.00	9
82.5	80.0616	81.9	81.1	81.58	80	70 70	81,5575	-100.00	0.00	\$0.00	R)
82.5	80.0616	81.9	80.9	81.4	80	70	81.515	-100.00	0.00	\$0.00	3
82.5	80.0616	81.9	80.8	81.19	80	70	81.33625	-100.00	0.00	\$0.00	
82.5	80,0616	81.9	80.6	80.99	80	70	81.135 80.94125	-100.00	0.00	\$0.00	
82.9	80,4616	82.3	81.4	81.82	80	70	81,7625	-100.00	0.00	\$0.00	
82.9	80,4616	82.3	81.3	81.75	80	70	81.69375	-100.00	0.00	\$0,00	(
82.9	80,4616	62.3	81.2	81.61	80	70	81.5575	-100.00	0.00	\$0.00	
82.9	80,4616	82.3	81.1	81.58	80	70	81.515	-100,00	0,00	\$0.00	
82.9	80.4616	82.3	80.9	81.4	80	70	81.33625	-100.00	0.00	\$0,00	
82.9	80 4616	82.3	80.6	81.19	80	70	81.135	-100.00 -100.00	0.00	\$0.00	(
82.9	80.4616	82 3	80.6	80.99	80	70	80,94125	-100.00	0.00	\$0.00	
							OM:P41EG	-100.00	Reg	\$0.00	
								- 1		\$0.00	
								- 1	100.00 50.00	\$0.00	(
									25.00	\$0.00	9
									10.00	\$0.00 \$0.00	(
									5.00	\$0.00	(
								- 1	2.00	\$0.00	(

Total Indirect Damage Value	Average Annual Damages 2007 Indirect Damages	Present Worth (50 Year, 5%) Indirect Damages	Measure Weight	Category Importance/ Significance	Product
(S)	(S)	(\$)	(1-10)	(1-10)	
So					
\$0					
\$0		1			
\$0	\$0	50	0	- 4	0
so	Î	1			
\$0					
\$0					

	Summarized Damage Costs (\$)
Frequency	
Reg	0
100	0
50	a
25	
10	0
5	0
	0

- 1 Determine flooding elevations for all storm events at buildings that potentially flood
- 2 Determine first floor elevation by reviewing topographic mapping elevations at building footprint and add 0.5m +/-
- 3 Determine basement floor elevation by substracting 2.44m from the first floor elevation
- 4 Determine basement window opening elevation by adding 1.83m to basement floor elevation (lowest opening, except if building has a walkout or is not residential land use)
- 5 Determine flooding depths based on lowest opening elevation and flooding elevations for all storms
- 6 Determine flooding damages for each return period based on the flooding depths and damage curve equations



LEGEND :

REGULATORY FLOODLINE

TOWNWIDE FLOODING STUDY

TOWN OF OAKVILLE

SITE # 40 - MORR0000M

MORRISON CREEK

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Project No.	106026
Date	January 2008
Scale	1:1,000
Figure No.	40

# **Lower Morrison Creek Photo Log (October 2016)**



1: D/S Face of Lakeshore Road 7.9m x 3.2m Conc. Arch Culvert, Station 354.4469



2: U/S Face of Morrison Road 3.7m x 2.05m Conc. Box Culvert, Station 878.3941



3: D/S Face of Linbrook Road 7.3m x 1.1m Conc Arch Culvert, Station 120.4545



4: D/S Face of Chartwell Road Twin Conc. Box 3.0m x 1.9m, Station 176.7459

# Lower Morrison Creek Photo Log (October 2016)



5: D/S Face Maple Avenue 3.0m x 1.2m Box Culvert, Station 2711.132

# **Lower Wedgewood Creek Photo Log (October 2016)**



1: D/S Face Lakeshore Road 3.8m x 1.9m Conc Arch, Station 242.8122



3: D/S Face of Wedgewood Drive 5.5m x 1.5m CSP Arch, Station 675.4334



2: U/S Face of Warren Drive Park 4.2m x 1.5m CSP, Station 644.3186



4: Bridge at Weaver Avenue Pedestrian Bridge 2.3m x 14.1m, Station 1480.446

# **Lower Wedgewood Creek Photo Log (October 2016)**



5: D/S Face Devon Road Twin Conspan Arch 4.3m x 2.0m, Station 1587.402



7: U/S Face Duncan Road culvert CMP Ellipse 2.45m x 1.8m, Station 1844.065



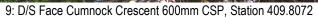
6: U/S Face of Amber Crescent CSP Ellipse 2.6m x 2.1m, Station 1711.164



8: U/S Face Drummond Road CSP Arch 1.15m x 1.7m, Station 263.7177

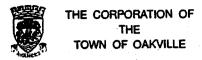
# Lower Wedgewood Creek Photo Log (October 2016)







10: U/S Face of Morrison Road CSPA 1.8 x 1.26, Station 2.465





The Corporation of the Torre of **Calville**Department of Public Viries
2274 Tratalgar Road
Dakville, Ontario L517622
Phone: (905) 338-44231
Fact (905) 330-4159

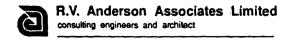


# Lower Morrison/Wedgewood Creeks

# Flood, Erosion and Master Drainage Plan Study

Technical Report

January 1993



# **ERRATUM No. 1**

A study was undertaken to update the sites and priorities for implementation of erosion control works that were identified in the Lower Morrison/Wedgewood Creeks - Flood, Erosion and Master Drainage Plan Study. The Study Update involved an erosion site inventory and development of numerical ratings for each erosion site. This Erratum presents the ratings and the priorities for each erosion site along the Lower Morrison/Wedgewood Creeks.

IT IS RECOMMENDED THAT THE RATINGS DEVELOPED DURING THIS STUDY UPDATE REPLACE THE PRIORITIES ASSIGNED DURING THE MASTER DRAINAGE PLAN STUDY. A HIGH RATING INDICATES THAT EROSION CONTROL WORKS SHOULD BE IMPLEMENTED BEFORE AN EROSION SITE WITH A LOWER RATING.

A procedure was developed to assign a numerical rating or value to each erosion site. The maximum rating for any site is 20 and the minimum value is five (5). The rating procedure developed during this Study is expected to yield more consistent results when evaluating erosion sites than the subjective procedures used in the Master Drainage Plan Study. Ratings for each of the streambank erosion sites are shown in Tables Err.1 and Err.2.

A detailed report of the streambank erosion inventory and analyses undertaken during the Study Update was provided under separate cover to the Corporation of the Town of Oakville.

Site Location	Site Number	Type of Erosion	Extent of Erosion	Consequences of Failure	Remedial Measures	Rating
100 m upstream of Maple Avenue	<b>1</b>	bank	shape undercut length 20 m width 2 m	loss of land.	provide erosion protection.	6
Adjacent to Cedar Grove Boulevard	J	toe	shape bluff length 45 m width 6 m	loss of land.	remove trees, protect toe to promote undergrowth.	14
Balmoral Place	<b>K</b>	bank	shape rect. length 10m width 2m	loss of storm drain outlet.	repair drain outlet and provide erosion protection.	11
160 m upstream of Morrison Road	L	toe	shape bluff length 160 m height 4 m	loss of buildings, loss of land, imminent risk.	construct retaining wall.	13
30 m upstream of Morrison Road	M	bank	shape undercut length 20 m width 2 m	loss of land.	construct retaining wall.	7
Morrison Road	N	bank	shape rect. length 1 m width 1.5 m	loss of erosion protection.	extend protection (a) and key into bank (b).	6
Lakeshore Road East	O	bed	shape rect. length 35 m width 4 m	loss of culvert (footings exposed).	protect footings.	7

Lower Morrison/Wedgewood Creeks - 1993 Update

Table ERR.2 LOWER WEDGEWOOD CREEK EROSION INVENTORY AND REMEDIAL MEASURES

Site Location	Site Number	Type of Erosion	Extent of Erosion	Consequences of Failure	Remedial Measures	Rating
Watercourse realignment, north of QEW	A	sheet/rill under construction.	shape trap. length 200m width 10m	loss of land.	seed and mulch.	Completed
Comwall Road	В	bank/bed existing rip rap displaced.	shape trap. length 50m width 46m	culvert washout.	replace riprap with massive or anchored protection.	Completed
150 m downstream of Cornwall Road	C	bank/toe	shape bluff length 30m height 4m	loss of land.	massive, anchored flexible system also slope protection, removal of trees and stabilize slope.	14
Devon Road	D	frost heaved concrete	shape trap. length 16m width 12m	loss of access road.	monitor erosion, replace retaining wall on south bank & stabilize north bank.	9
60 m downstream of Devon Road	E	toe	shape bluff length 75m		monitor to identify when protection is required.	8
150 m upstream of Wedgewood Drive	F	bank	shape undercut length 30m height 2m	loss of land.	construction of retaining wall (a) & (b).	11
180 m upstream of Lakeshore Road East	G	bank	shape undercut length 30m width 2m	loss of swimming pool.	monitor to determine if and when a retaining wall will be necessary.	10
20 m downstream of Lakeshore Road East	н	deteriorating channel protection.	shape rect. length var. width 2m	loss of land.	recommend examination for integrity and reconstruction.	5

## SUMMARY

Development pressures within the Lower Morrison and Lower Wedgewood Creeks necessitated that flooding and erosion be identified and remedial measures recommended before development could proceed.

The Town of Oakville requested that a Study carry out the following:

- prepare Flood Plain Mapping of the Lower Morrison and Lower Wedgewood Creeks:
- an erosion inventory;
- a hydrologic/hydraulic analyses;
- determine impacts of future development; and
- identify and recommend remedial measures to mitigate potential flooding and erosion.

The Study was carried out under the guidance of a Project Administration Team comprised of individuals from the Town of Oakville, the Halton Region Conservation Authority, Environment Canada and Pro Urban Developments.

The Study was conducted using the Canada/Ontario Flood Damage Reduction Program standards. Funding was provided by the Corporation of the Town of Oakville, Pro Urban Developments Limited and Markborough Properties Incorporated.

R. V. Anderson Associates Limited was retained to carry out the Study with Bennett & Norgrove Limited producing the topographic mapping and Gartner Lee Limited conducting the erosion inventory.

The Flood Plain Mapping identified 26 potentially flooded buildings within the Regulatory Flood Plain along Lower Morrison Creek and potentially 42 buildings along Lower Wedgewood Creek.

The erosion inventory identified only one (1) site which endangered two (2) private residential buildings that should receive immediate attention. Two (2) additional sites should be monitored on a regular basis to determine when remedial measures should be implemented. The remainder of the erosion sites would not require immediate action but would warrant remedial works.

The recommended works to mitigate potential erosion and flooding are shown in Table S.1. Five (5) erosion sites that require quick attention are identified as high priority. The total cost to implement the works is approximately \$4.6 million. The completion of the Plan will involve a considerable time period and monetary effort. The Plan when completed will eliminate potential flood and erosion damages along the Lower Morrison/Wedgewood Creek. Since the time to completion could be considerable, peak runoff rates from all new development sites should be controlled to 50% of predevelopment levels until the plan is completed.

If the above policies are followed then flood and erosion damages within the watershed should not increase as a result of new development.

**SUM - 3** 

Lower Morrison/Wedgewood Creeks Flood, Erosion and MDP

Table S.1 RECOMMENDED FLOOD AND EROSION CONTROL WORKS

Location	Watercourse	<u>Priority</u>	<u>Works</u>	<u>Ownership</u>	Type of Works	1 - [	Costs
Lower Morrison/Wedgewood Creeks	LM/WC	high	SWM Policy				
Morrison Road - 160 m u/s	L. Morrison	high	retaining wall	private	erosion	-3	\$ 480,000
Lakeshore Road East - 180 m u/s	L. Wedgewood	high	monitor	private	erosion		
60 m d/s of Devon Road	L. Wedgewood	high	monitor	private	erosion		· . •
north of QEW	L. Wedgewood	high	seed and mulch	private	erosion		\$ 15,000
Lakeshore Road East	L. Morrison	medium	protect footings	public	erosion		\$ 95,000
Balmoral Place	L. Morrison	medium	repair drain outlet	public	erosion		\$ 20,000
Lakeshore Road East	L. Morrison	low	floodproof 1 building	private	flood		\$ 30,000
Morrison Road	L. Morrison	low	floodproof 5 buildings	private	flood		\$ 150,000
Morrison Road	L. Morrison	low	erosion protection	public	erosion		\$ 5.000
Morrison Road - 30 m upstream	L. Morrison	low	erosion protection	private	erosion		\$ 40,000
Cedar Grove Boulevard	L. Morrison	low	remove trees, protect toe	private	erosion		\$ 30,000
Chartwell-Linbrook Road	L. Morrison	low	floodproof 3 buildings	private	flood		\$ 90,000
Maple Avenue	L. Morrison	low	floodproof 12 buildings	private	flood		\$ 360.00
Maple Avenue - 100 m u/s	L. Morrison	low	erosion protection	private	erosion	16.47	\$ 30,000
CN Railway Spur Line	L. Morrison	low	floodproof 3 buildings	private	flood		\$ 90,000
Chartwell Road - East Branch	L. Morrison	low	floodproof 2 buildings	private	flood		\$ 60,000
Lakeshore Road East	L. Wedgewood	low	floodproof 1 building	private	flood		\$ 30,000
Lakeshore Road East - 20 m d/s	L. Wedgewood	low	structural examination	public	erosion		\$ 5.000
Wedgewood Drive - d/s	L. Wedgewood	low	enlarge park & Wedgewood	public	flood		\$ 1,030,00
Wedgewood Drive - u/s	L. Wedgewood	low	floodproof 4 buildings	private	flood		\$ 120,000
Wedgewood Drive - 150 m u/s	L. Wedgewood	low	retaining wall	private	erosion		\$ 150,00
Devon Road	L. Wedgewood	low	enlarge Devon Rd. culvert & floodproof 3 buildings	public & private	flood		\$ 340,000
Amber Crescent	L. Wedgewood	low	enlarge Amber culvert	public	flood		\$ 100,000
Cornwall Road - 150 m d/s	L. Wedgewood	low	erosion protection	private	erosion		\$ 350,00
Cornwall Road	L. Wedgewood	low	replace rip rap	public	erosion		\$ 40,000
Duncan Road	L. Wedgewood	low	enlarge Duncan Rd. culvert & floodproof 1 building	public & private	flood		\$ 270,000
Duncan Road - u/s	L. Wedgewood	low	floodproof 1 building	private	flood	e de la compansión de l	\$ 30,000
Canadian Road	L. Wedgewood	low	floodproof 1 building	private	flood		\$ 30,000
Drummond Road	L. Wedgewood	low	enlarge Drummond Rd. cul. & floodproof 4 building	public & private	flood		\$ 470,000
Morrison Road	L. Wedgewood	low	floodproof 5 buildings	private	flood		\$ 150,000
			그렇게 하고 있는 것 이 없는 것?	and the second s	TOTAL		\$4,610,000

L. Morrison - Lower Morrison
L. Wedgewood - Lower Wedgewood

# **HYDROLOGIC ANALYSIS**

**Chapter 3** 

# 3.0

# **HYDROLOGIC ANALYSIS**

## 3.1 General

A hydrologic analysis of the watersheds is required to determine peak flow rates at points of interest within the basin. These flow rates are needed in the subsequent hydraulic analysis for determining water levels. Methods used to estimate peak flow rates include:

- frequency analysis of a station's recorded flood flows;
- regional flood frequency analysis; and
- rainfall/runoff simulation.

The most accurate and preferred method of generating peak flow rates would be a frequency analysis of a station's recorded flood flow rates. Stations with a sufficient period of record would have to be located at the points of interest and the upstream land use would have remained constant over the period of record. The single station frequency analysis cannot be used because no stations are located within the Lower Morrison/Wedgewood Creeks' watersheds.

The second most appropriate method would be a regional flood frequency analysis. Three (3) methods have been developed to determine peak flow rates from mostly rural/undeveloped watersheds. However, the Lower Morrison/Wedgewood basins are mostly developed. Regional flood frequency analysis cannot consider land uses different from the basin from which the procedures were developed. Also regional flood frequency analysis cannot consider changing land use within the study basin.

The rainfall/runoff simulation method was chosen to calculate peak flow rates from the Lower Morrison/Wedgewood basins. The three (3) regional flood frequency analysis methods developed by Environment Canada (Index Flood Method and Regression Analysis) and the Ministry of Natural Resources (Regression Analysis) were used to check the peak flow rates developed from the rainfall/runoff simulation.

# 3.2 Methodology

The process used to calculate peak flow rates for the Lower Morrison/Wedgewood Creeks included the following steps:

- select a rainfall/runoff simulation model appropriate for the study area;
- collect data and build model input files;
- calibrate the model;
- use the 100 year design storm to perform a sensitivity analysis of appropriate model input parameters;
- calculate peak flow rates for the Regional, 100 year, 50 year, 20 year, 10 year, 5 year and 2 year return period storms for existing and future land use conditions; and
- check peak flow rates using Environment Canada's Index Flood Method, Regression Analysis and the Ministry of Natural Resources' Regression Analysis Method.

## 3.3 Simulation Model

The rainfall/runoff simulation model OTTHYMO was used for determining peak flow rates. OTTHYMO is basically the hydrologic model, HYMO, with the following capabilities implemented by the University of Ottawa:

- urban basin runoff calculation;
- rural basin runoff calculation using the Nash method;
- variable initial abstraction; and
- closed conduit runoff routing of runoff.

The urban runoff calculation method was developed at the University of Ottawa and uses a two parallel linear reservoir model. The Nash method, published in 1957, calculates runoff from natural/rural basins. The original HYMO natural/rural runoff calculation method of J.R. Williams, which uses a two (2) parameter gamma distribution and recession constant, is included in OTTHYMO.

The University of Ottawa (OTTHYMO) urban runoff calculation method (URBHYD), which is the only urban hydrograph method, was applied to the areas of the Lower Morrison/Wedgewood Creeks.

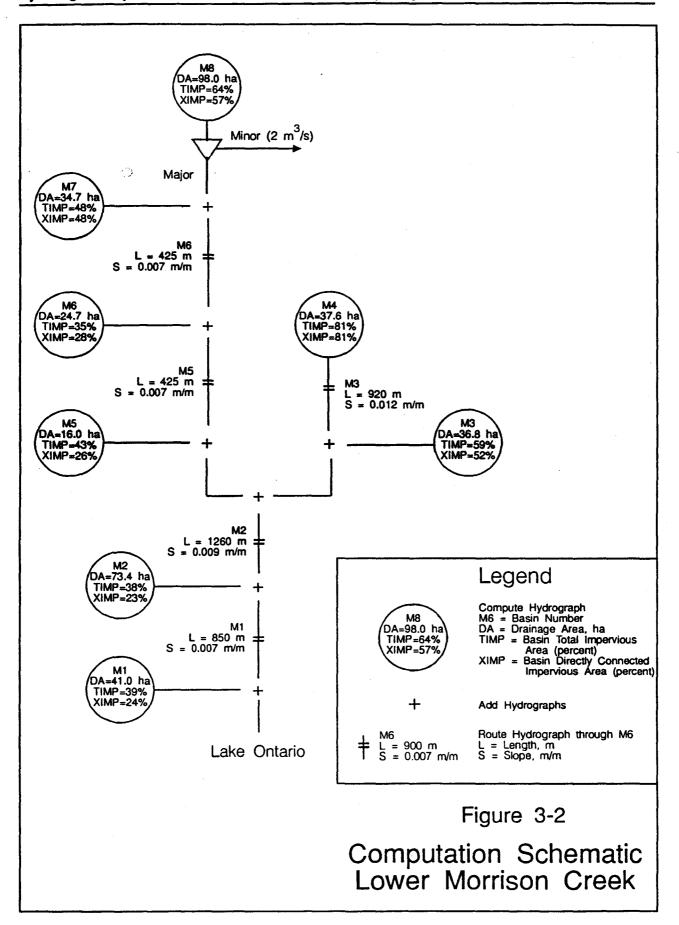
Input required by OTTHYMO includes the following:

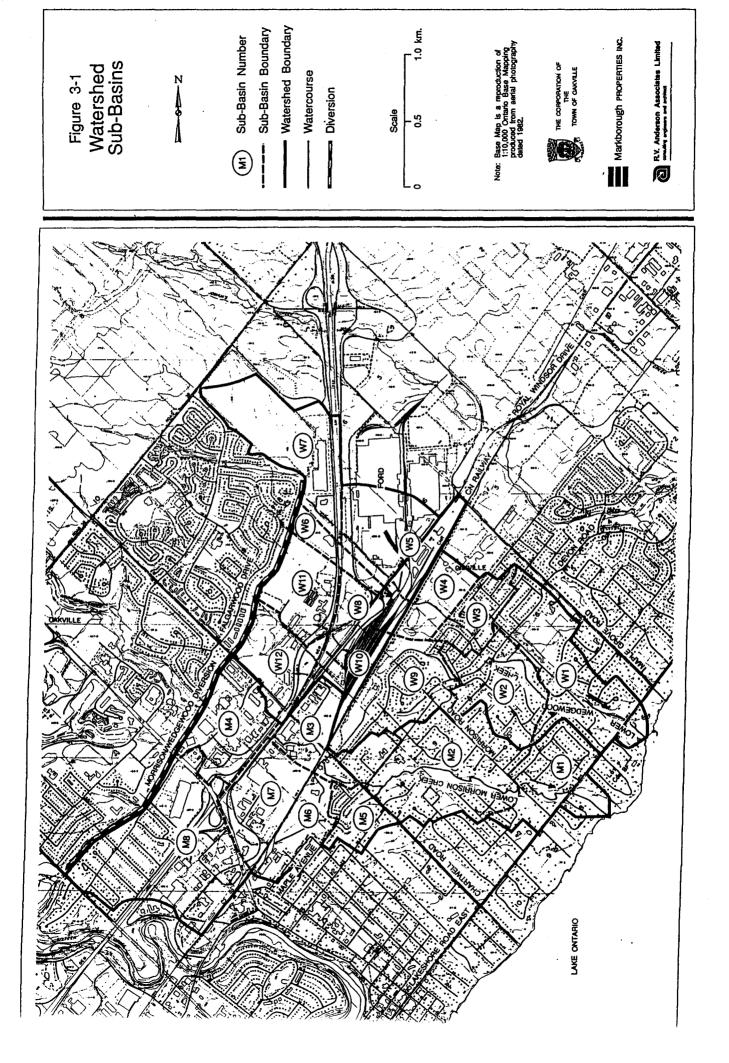
- design storm hyetograph;
- basin physical characteristics; and
- travel time and flow depth between points of interest along the watercourse.

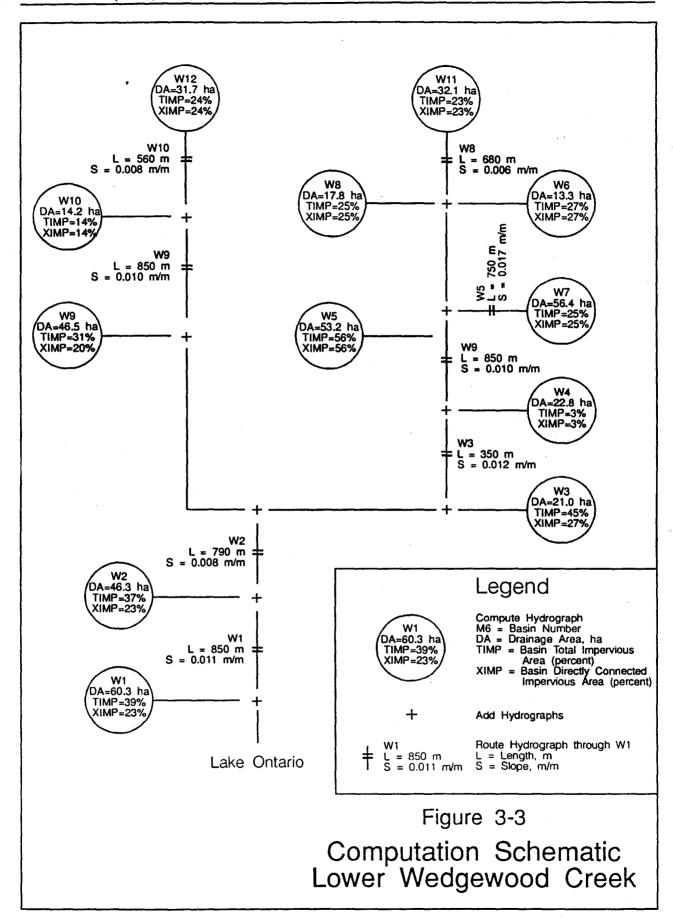
The physical characteristic input data required for this study are specifically:

- drainage area;
- directly connected impervious: total basin area ratio;
- total impervious : total basin area ratio;
- depression storage and linear storage coefficients for pervious and impervious areas; and
- runoff curve number.

The Lower Morrison/Wedgewood Creek basins were sub-divided for specific points of interest and hydrologic characteristics. The resulting sub-basins are depicted in Figure 3-1. Schematic diagrams of the OTTHYMO procedure are given in Figures 3-2 and 3-3 for the Lower Morrison Creek and Lower Wedgewood Creek, respectively.







# 3.4 Design Storms

# Regional Storm - Hurricane Hazel

The Regional Storm for the Lower Morrison/Wedgewood Creeks as specified by the Ministry of Natural Resources is Hurricane Hazel which passed through Southern Ontario. The 12 hour design storm, shown in Table 3.1, is applied to basins where the upstream circular drainage area is greater than 25 km² (10 mi²). The hourly rainfall values are multiplied by the percentages shown in Table 3.2 for circular drainage areas larger than 25 km².

The circular drainage areas for the Lower Morrison and the Lower Wedgewood Creeks are less than 25 km² and therefore no reduction factors were applied to the 12 hour Regional Storm values.

# 2 to 100 Year Design Storms

Design storms for return periods ranging from 2 to 100 years were developed using the Keifer & Chu method which is presently used by the Town of Oakville. The Keifer & Chu design storm has a variable duration and time step that are selected based on the physical characteristics of the watershed. A time step of 15 minutes and a storm duration of 24 hours were used in the simulations. The procedures used by the OTTHYMO model require a calculation time step equal to the time of concentration of the sub-basins. The sub-basins were selected assuming a time of concentration of approximately 15 minutes. A 24 hour storm was selected to include the largest time of concentration for each of the Study basins. Selecting a shorter duration storm could simulate runoff events with lower peak flow rates.

A long storm duration such as 24 hours will generate a higher peak flow rate for pervious areas than a shorter duration storm. However, for urban areas where peak flow rates are largely influenced by rainfall intensity, peak flow rates will only slightly change for a long duration storm. For the Keifer and Chu design storm, peak rainfall intensities do not vary with storm durations and therefore peak flow rates will not significantly change.

Table 3.1 HURRICANE HAZEL STORM

In the first 36 hours the total rainfall recorded was 73 mm. The following 12 hours represents the Ontario Ministry of Natural Resources Regional Storm.

	Depth (mm)	Percent of Total
37th hour 38th hour 39th hour 40th hour 41st hour 42nd hour 43rd hour 44th hour 45th hour 47th hour 48th hour	6 4 6 13 17 13 23 13 13 53 38 13	3 2 3 6 8 6 11 6 25 18 6
Total	212 mm	100

# Table 3.3 INTENSITY- DURATION-FREQUENCY VALUES

# AES TORONTO (BLOOR STREET) GAUGE 43 YEARS OF RECORD 1940 - 1986

# Rainfall Intensity (mm/hr)

Duration	2	5	10	25	50	100
(Minutes)	<u>Year</u>	<u>Year</u>	<u>Year</u>	<u>Year</u>	<u>Year</u>	<u>Year</u>
5	117	164	194	233	262	291
10	80	108	126	149	166	183
15	65	90	107	129	145	160
30	41	58	69	83	93	103
60	25	35	41	48	54	60
120	15	20	23	27	30	33
360	6.1	8.1	9.4	11	12	13
720	3.6	4.6	5.3	6.2	6.8	7.5
1440	2.0	2.5	2.9	3.4	3.7	4.1

# Table 3.4 RAINFALL INTENSITY EQUATION COEFFICIENTS\*

# AES TORONTO (BLOOR STREET) GAUGE 43 YEARS OF RECORD - 1940 TO 1986

Return	i	Coefficie	nt	Correlation	
Period (Years)	Α	b	С	Coefficient	· · · · · · · · · · · · · · · · · · ·
2	835	4.9	0.809	0.999942	
5	1155	5.1	0.841	0.999854	4).
10	1400	5.7	0.847	0.999762	
25	1680	5.6	0.851	0.999730	
50	1960	5.8	0.861	0.999683	
100	2150	5.7	0.861	0.999628	

<sup>\*</sup> Corrected for partial duration series.

$$i = \frac{A}{(t_d + b)^c} = rainfall intensity,$$

A, b and c constants.  $t_d$  = duration, minutes.

Table 3.6 BASIN PARAMETERS - LOWER MORRISON CREEK

			Existing Conditions						
		Drainage	Pervi	•	% Imp	ervious	Length		
Basin	OTTHYMO	Area	Curv	e Number			Parameter		
<u>Number</u>	Command	<u>(ha)</u>	П	Ш	<u>Total</u>	<u>Direct</u>	(metres)		
M-1	URBHYD	41.0	68	84	39	24	520		
M-2	URBHYD	73.4	67	83	38	23	700		
M-3	URBHYD	36.8	72	86	59	52	500		
M-4	URBHYD	37.6	81	92	81	81	500		
M-5	URBHYD	16.0	63	80	43	26	330		
M-6	URBHYD	24.7	73	87	35	28	410		
M-7	URBHYD	34.7	78	90	48	48	1200		
M-8	URBHYD	96.7	82	92	64	58	1800		

			Future Conditions							
Basin	ОТТНҮМО	Drainage Area	Pervi Curv	ous e Number	% Imp	Length Parameter				
Number	Command	<u>(ha)</u>	<u>II</u>	111	<u>Total</u>	<u>Direct</u>	(metres)			
M-1	URBHYD	41.0	68	84	39	24	520			
M-2	URBHYD	73.4	67	83	38	23	700			
M-3	URBHYD	36.8	71	86	66	60	500			
. М-4	URBHYD	37.6	81	92	81	81	500			
М-5	URBHYD	16.0	63	80	43	26	330			
M-6	URBHYD	24.7	70	85	67	60	410			
M-7	URBHYD	34.7	79	91	70	70	1200			
M-8	URBHYD	96.7	83	93	67	60	1800			

Il average antecedent precipitation conditions

III wet antecedent precipitation conditions

1

Table 3.7 BASIN PARAMETERS - LOWER WEDGEWOOD CREEK

			Existing Conditions						
Basin	OTTHYMO	Drainage Area	Pervious Curve Number		% Impervious		Length Parameter		
Number	Command	<u>(ha)</u>	<u>11</u>	111	<u>Total</u>	<u>Direct</u>	(metres)		
W-1	URBHYD	60.3	64	81	39	23	630		
W-2	URBHYD	46.3	65	82	37	23	560		
W-3	URBHYD	21.0	65	82	45	27	370		
W-4	URBHYD	22.8	58	76	3	3	390		
W-5	URBHYD	53.2	68	84	56	56	580		
W-6	URBHYD	13.3	71	86	27	27	300		
W-7	URBHYD	56.4	82	92	25	25	370		
W-8	URBHYD	17.8	73	87	25	25	380		
W-9	URBHYD	46.5	69	85	31	20	560		
W-10	URBHYD	14.2	72	86	14	14	310		
W-11	URBHYD	32.1	77	89	23	23	460		
W-12	URBHYD	31.7	77	89	24	24	460		

			Future Conditions						
Basin OTTHYMO		Drainage Area	Pervious Curve Number		% Impervious		Length Parameter		
<u>Number</u>	Command	<u>(ha)</u>	11	<u>III</u>	<u>Total</u>	<u>Direct</u>	(metres)		
W-1	URBHYD	60.3	64	81	39	23	630		
W-2	URBHYD	46.3	65	82	37	23	560		
W-3	URBHYD	21.0	65	82	45	27	370		
W-4	URBHYD	22.8	66	82	81	81	390		
W-5	URBHYD	53.2	72	86	78	78	580		
W-6	URBHYD	13.3	67	83	63	63	300		
W-7	URBHYD	56.4	82	92	30	30	370		
W-8	URBHYD	17.8	73	87	25	25	380		
W-9	URBHYD	46.5	67	83	52	41	560		
W-10	URBHYD	14.2	72	86	14	14	310		
W-11	URBHYD	32.1	80	91	76	76	460		
W-12	URBHYD	31.7	79	91	64	64	460		

Il average antecedent precipitation conditions

III wet antecedent precipitation conditions

Soils within the Lower Morrison/Wedgewood basins are described in the "Soils of Halton County, Report No. 43 of the Ontario Soil Survey". The soil maps cover only portions of the two (2) watersheds. The soils within the remaining areas were interpolated.

The Ontario Ministry of Transportation's Drainage Manual (Volumes I, II, and III) were used to determine the following hydrologic soil types found within the basins:

Hydrologic <u>Soil Group</u>	Percentage of Total Basin		
D	5		
AB	12		
С	34		
D	2		
AB	40		
С	3		
D	4		
	Soil Group  D AB C D AB		

The various soil types within the Lower Morrison/Wedgewood watersheds are shown in Figure 3-4.

All vegetation within the Lower Morrison/Wedgewood Creeks basins was classified under one of the following:

- meadows
- woods
- lawns

Curve numbers for the different classes of vegetation and soils are shown in Table 3.8. The values were abstracted from the National Engineering Handbook published by the U.S. Soil Conservation Service.

Figure 3-4

Hydrologic Soil
Groups

Soil Group AB

Soil Group B

Soil Group B

Soil Group B

Watershed Boundary

Watercourse

Watercourse

Diversion

O 0.5 1.0 km.

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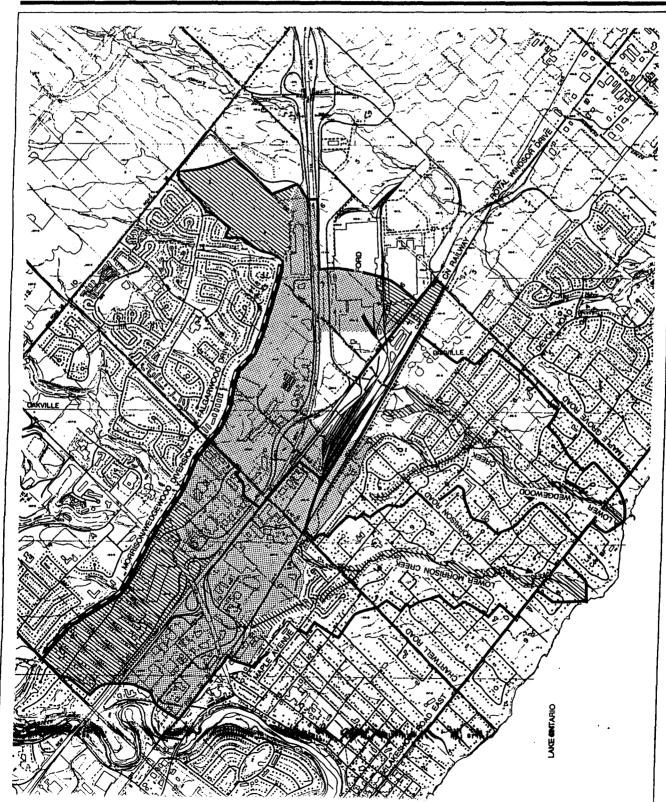


Table 3.8 CURVE NUMBERS'

	Hydrologic Soil Group					
Vegetation Cover	<u>A</u>	<u>B</u>	<u>C</u>	D		
meadows	46	66	77	82		
woods	36	60	73	79		
lawns	56	71	81	85		

The curve numbers for each of the sub-basins are shown in Table 3.6 for Lower Morrison Creek and Table 3.7 for Lower Wedgewood Creek. The curve number calculations are shown in Appendix A. The curve numbers shown in Table 3.8 represent average soil moisture conditions. Table 3.9 shows the relationship between dry (1), average (2) and wet (3) antecedent conditions. A large amount of rainfall preceded the maximum twelve (12) hour amount used for the Regional (Hurricane Hazel) Storm. Curve numbers shown in Table 3.8 must be increased from average to wet soil conditions for the Hurricane Hazel storm.

Depression storage values for impervious and pervious areas were set equal to 3 and 5 mm respectively. The values were determined after a review of the OTTHYMO User's Manual and a review of the Mimico Creek Study prepared for the Metropolitan Toronto and Region Conservation Authority.

The linear storage coefficient which determines the shape of the hydrograph may be input by the analyst/modeller or determined internally by specifying the overland flow length, Mannings roughness coefficients and the basin slope. Data is not available to estimate directly the linear storage coefficients. The storage coefficients for Lower Morrison/Wedgewood Creeks were determined internally by OTTHYMO.

Manning roughness coefficients for impervious and pervious areas were set equal to 0.015 and 0.250 respectively. The values were abstracted from a review of the OTTHYMO's and SWMM IV User's Manuals.

<sup>1.</sup> Page 9.2 National Engineering Handbook, Section 4, Hydrology, U.S. Soil Conservation Service, March 1985.

Table 3.9 VARIATION IN CURVE NUMBER BASED ON ANTECEDENT PRECIPITATION

Cond	dition			Cond	dition			Cond	dition	
1_	11	Ш		1	<u> </u>	<u> III</u>		1	11	Ш
_				_	_				_	<del></del> ,
100	100	100		48	68	84		19	36	56
97	99	100		47	67	83		18	35	55
94	98	99		46	66	82		18	34	54
91	97	99		45	65	82		17	33	53
89	96	99		44	64	81		16	32	52
87	95	98	÷	43	63	80		16	31	51
85	94	98		42	62	79		15	30	50
83	93	98		41	61	78		12	25	43
81	92	97		40	60	78		9	20	37
80	91	97		39	59	77		6	15	30
78	90	96		38	58	76		4	10	22
76	89	96		37	57	75		2	5	13
75	88	95		36	56	75		0	0	0
73	87	95		35	55	74				
72	86	94		34	54	73				
70	85	94		33	53	72	•			
68	84	93		32	52	71				
67	83	93		31	51	70				
66	82	92		31	50	70		•		
64	81	92		30	49	69				
63	80	91		29	48	68				
62	79	91		28	47	67				
60	78	90		27	46	66				
59	77	89		26	45	65				
58	76	89		25	44	64				
57	75	88		25	43	63				
55	74	88		24	42	62				
54	73	87		23	41	61				
53	72	86		22	40	60				
52	71	86		21	39	59				
51	70	85		21	38	58				
51	69	85		20	37	57				

I dry antecedent precipitation conditions

Il average antecedent precipitation conditions

III wet antecedent precipitation conditions

The overland flow length for each sub-basin was determined by taking the square root of the drainage area (hectares) divided by 1.5 and multiplying by 100. The values for each of the sub-basins are shown in Tables 3.6 and 3.7. The impervious and pervious lengths were assumed equal for all storage coefficient calculations.

The OTTHYMO input parameters are shown in Appendix B.

# 3.6 Routing

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The transposition of a hydrograph from one point of interest to another is referred to as routing. OTTHYMO requires a table of flow depths and travel times for specific flow rates to route a hydrograph from one point of interest to another.

The analyst/modeller may enter the values directly or have the values determined internally by the program. OTTHYMO will calculate the flow rates, depths and travel times if the following values are input:

- channel and flood plain slopes;
- cross section described by distance and elevation measured from the left bank;
- Manning's roughness coefficients; and
- routing length.

## 3.7 Model Calibration

Computer simulation models usually require the calibration of parameters which cannot be accurately measured to simulate the rainfall/runoff process. Calibration is recommended to adjust those input parameters until a good agreement is obtained between measured and simulated hydrographs.

Calibration of the Lower Morrison/Wedgewood Creek models cannot be undertaken as no rainfall or runoff gauges exist within the watersheds. When calibration cannot be carried out on the study basin it is common to undertake a calibration/verification of input parameters on adjacent basins. Sixteen Mile Creek and the Credit River have both rainfall and runoff gauges located within the watersheds. The watersheds have been the subject of recent flood plain mapping studies which involved the calibration/verification of the hydrologic models. However, the studies did not calibrate or verify specifically the URBHYD routine of the OTTHYMO model. The Mimico Creek Study carried out for the Metropolitan Toronto and Region Conservation Authority calibrated and verified the URBHYD routine for that watershed. That Study was reviewed to abstract calibrated parameters which would be representative of conditions within the Lower Morrison/Wedgewood Creeks.

# Mimico Creek Study

The Study calibrated the NASH HYD and the URBHYD routines on the Mimico and Etobicoke Creeks. An initial abstraction of 3 mm for the Etobicoke Creek was determined from an analysis of recorded rainfall and runoff.

The Study found that curve numbers and overland flow lengths did not have to be varied from standard procedures to accurately simulate recorded hydrographs.

No variations in the overland flow lengths and the curve numbers values will be made to the Lower Morrison/Wedgewood Creek models.

An analysis was carried out to compare peak flow rates determined by the URBHYD routine with values estimated by regional frequency analysis. The following three (3) regional frequency methods were chosen for comparison with URBHYD:

- (i) Environment Canada Index Flood Method
- (ii) Environment Canada Regression Analysis
- (iii) Ministry of Natural Resources Regression Analysis

The three (3) regional frequency analysis methods are based on recorded runoff from rural or undeveloped basins. Peak flow rates calculated using URBHYD assuming existing or highly developed conditions would be much higher than the regional methods. The URBHYD input parameters of the Lower Morrison/Wedgewood basins were changed to reflect natural/rural land uses. The impervious portions of all basins were set equal to 0.0 and curve numbers for each of the basins were recalculated assuming a land use composed of two thirds (2/3) meadow and one third (1/3) woods. The Mannings roughness coefficient for overland flow was increased from 0.25 to 0.40.

Peak flow rates determined from the regional frequency analysis for several points of interest within the Lower Morrison/Wedgewood Creeks are shown in Appendix C. The following is a comparison of the 100 year peak flow rates calculated at Lake Ontario:

				Environmen	ment Canada			
		MNR	Index f	lood		Upper	Lower	
Watershed	(m3/s)	Regression (m <sup>3</sup> /s)	Region 7 (m <sup>3</sup> /s)	Region 8 (m <sup>3</sup> /s)	Regression (m <sup>3</sup> /s)	Bound (m <sup>3</sup> /s)	Bound (m <sup>3</sup> /s)	
Lower Morrison	10.6	9.2	5.8	6.9	2.7	20	2	
Lower Wedgewood	15.1	10.7	6.4	7.8	3.1	25	3	

Note:

All peak flow rates represent natural/rural land use conditions. Upper and lower bounds are defined by Environments Canada for Region 8.

The peak flow rates generated by URBHYD are relatively high in comparison to the three (3) regional flood frequency methods. It should be remembered that URBHYD was developed for urban basins with significant impervious areas and efficient drainage systems. Although the peak flow rates are relatively high the values fall within the upper and lower bounds for Region 8 as defined by Environment Canada.

The values show that the URBHYD routine of OTTHYMO generates high values for natural/rural areas but within acceptable levels. It can be concluded that the URBHYD routine can be used to define flood hydrographs for flood plain management purposes.

## 3.8 Sensitivity Analysis

A sensitivity analysis was undertaken to determine the variation of runoff hydrographs as a result of variations in input parameters. The input parameters varied during the analysis include the following:

- overland flow lengths;
- curve number;
- ratio of total impervious area to total drainage area;
- ratio of impervious areas to total drainage area.

The analysis was conducted for future land use conditions using the 100 year design storm. The 100 year storm will yield the largest variation in runoff when compared to Hurricane Hazel and the other return period storms.

Overland flow lengths in OTTHYMO are calculated by taking the square root of the drainage area divided by 1.5. The OTTHYMO User's Manual assumes a basin length to width ratio of 1.5. The sensitivity analysis varied the length to width ratio from 1.0 to 2.0. The results shown in Table 3.10 indicate a 2% variation in peak flow rates for the Lower Morrison/Wedgewood Creek's basins.

Curve numbers for the pervious areas were varied by 10 above and below the values determined for the design values. The Lower Morrison/Wedgewood Creek's peak flow rates varied by approximately 8%.

Impervious ratios were increased and decreased by 20% from design values. Peak flow rates increased/decreased proportionally by approximately 15%. The values varied depending upon location within the basin. The largest increases were observed in the upper portions of the basin with the smallest in the lower reaches.

Roof leaders draining onto grassed areas yielded significant differences in total impervious and directly connected areas. A sensitivity analysis was made to determine increases in peak flow rates as a result of converting indirectly connected impervious areas to directly

connected. Table 3.10 shows that peak flow rates increased by approximately 6% by assuming all impervious areas were directly connected.

#### 3.9 Peak Flow Rates

Peak flow rates for existing and future land use scenarios are shown in Table 3.11. Generally, Lower Morrison Creek peak flow rates for future conditions are approximately 10% higher than values for existing land use conditions. Along Lower Wedgewood Creek peak flow rates for future land use conditions are approximately 40% higher than values for existing land use conditions.

Peak flow rates at Lake Ontario for the 100 year Storm were slightly less than the Regional (Hurricane Hazel) values. Upstream the 100 year peak flow rates were significantly larger than the Regional flows.

The Regulatory Flood is the greater of the Regional or the 100 year flood. The Regulatory Flood Plain will be determined using the Regional storm peak flow rates for the lower reaches of the watercourses, while the upper reaches will be defined using the 100 year values.

The Lower Morrison/Wedgewood Creek peak flow rates are conservative as the values have been calculated assuming no storage behind road/railway embankments. Storage behind road/railway embankments attenuates peak flow rates which leads to lower downstream peak flow rates and water surface elevations. Standard flood plain management practice assumes no storage behind road/railway crossing embankments as a culvert/bridge can be replaced at any time. The storage behind the embankment would be lost and peak flow rates downstream would be increased.

Lower Morrison/Wedgewood Creek Flood, Erosion and MDP

Final

TABLE 3.10 SENSITIVITY ANALYSIS - OTTHYMO

				FUTURE CON	DITIONS	-			
Location	Drainage Area (ha)	100 year Peak Flow (m <sup>3</sup> /s)	Overland L/W = 1 (m <sup>3</sup> /s)	Flow Length L/W=2 (m <sup>3</sup> /s)	Curve I - 10 (m <sup>3</sup> /s)	tumber + 10 <u>(m<sup>3</sup>/s)</u>	* 0.8	% Imperv	XIMP - TIMP
Location	III.	<u>[(1] /3)</u>	(m-78)	(m - / s)	(m-/si	<u>(m=74)</u>	<u>(m³/s)</u>	<u>(m<sup>3</sup>/s)</u>	<u>(m<sup>3</sup>/s)</u>
LOWER WEDGEWOO	OD CREEK								
Lake Ontario	420	43.8	42.9	44.5	40.4	48.8	38.5	50.3	45.6
Alscot Crescent	360	43.6	42.6	44.5	40.7	48.7	37.6	50.3	45.6
East Branch									
Amber Crescent	220	39.2	36.2	39.8	37.7	41.6	33.3	45.0	39.2
Constance Drive	200	39.2	38.2	39.8	37.7	41.6	33.3	45.0	39.2
CN Railway .	170	37.2	36.1	37.9	35.7	39.5	31.7	42.6	37.2
QEW	60	10.8	10.3	11.2	9.5	12.8	9.8	11.9	10.8
East Branch - Wester	n Tribulary								
CN Railway	30	11,1	10.9	11.3	10.8	11.5	9.6	12.7	11.1
West Branch									
Drummond Road	90	13,1	12.7	13.4	12.2	14.4	11.3	14.9	14.4
CN Railway	45	9.7	9.5	9.9	9.3	10.3	8.4	11.0	9.7
QEW	30	9.7	9.5	9.9	9.3	10.3	8.4	11.0	9.7
LOWER MORRISON	CREEK								
Lake Ontario	360	35.3	33.9	36.1	32.4	39.0	30.0	40.0	37.4
Morrison Road	320	34.5	33.3	35.1	32.4	37.4	29.7	39.2	36.3
Linbrook road	75	16.8	16.3	17.1	16.3	17.5	14.2	17.3	36.3 17.3
QEW	40	13.3	13.0	13.5	13.1	13.7	11.4	15.2	13.3
West Branch									
Chartwell Drive	170	25.6	24.1	25.5	25.0	27.1	21.5	30.2	27.2
Maple Avenue	160	25.6	24.1	25.8	25.0	27.1	21.5	30.2	27.2
CN Railway	130	25.6	24.1	27.1	25.0	27.1	21.5	30.2	27.2

TABLE 3.11 PEAK FLOW RATES

	Drainage	Regional		100 Y	ear	50 Ye	ar	25 Yes	<del>n</del>	10 Ye	軒	<u>5 Ye</u>	<del>a</del> r	2 Ye	ar
Location	Area (ha)	Existing (m <sup>3</sup> /s)	Future (m <sup>3</sup> /s)	Existing (m <sup>3</sup> /s)	Future (m <sup>3</sup> /s)	Existing (m <sup>3</sup> /s)	Future (m <sup>3</sup> /s)	Existing (m <sup>3</sup> /s)	Future (m <sup>3</sup> /s)	Existing (m <sup>3</sup> /s)	Future (m <sup>3</sup> /s)	Existing (m <sup>3</sup> /s)	Future (m <sup>3</sup> /s)	Existing (m <sup>3</sup> /s)	Future (m <sup>3</sup> /s)
LOWER WEDGEWOOD	CREEK														
Lake Ontario	420.0	44.9	47.7	31.6	43.8	26.8	38.5	22.7	33.2	17,6	26.2	14.0	21.6	10.9	17.1
Alscot Crescent	360.0	39.0	42.0	30.1	43.6	25.8	38.4	21.9	33.2	17.0	26.2	13.6	21.6	10.6	17.1
East Branch															
Amber Crescent	220.0	24.8	27.2	26.7	39.2	23.4	34.7	20.2	30.3	16.1	24.7	13.3	20.7	10.3	16.2
Constance Drive	200.0	22.6	25.0	26.7	39.2	23.4	34.7	20.2	30.3	16.1	24.7	13.3	20.7	10.3	16.2
CN Railway	170.0	20.8	22.2	26.7	37.2	23.4	33.0	20.2	28.8	16.1	23.5	13.3	19.7	10.3	15.4
QEW	60.0	6.8	6.9	9.9	10.8	8.6	9.4	7.4	8.1	5.7	6.4	4.7	5.2	3.5	4.0
East Branch - Western	Tributary														
QEW	30.o	4.0	4.5	5.4	11.1	4.7	9.9	4.0	8.7	3.1	7.2	2.5	6.1	1.9	4.8
West Branch															
Drummond Road	90.0	10.4	11.3	8.7	13.1	7.5	11.5	6.4	10.0	4.9	8.1	3.9	6.7	3.0	5.2
CN Railway	45.0	5.5	5.9	5.7	9.7	4.9	8.6	4.2	7.6	3.3	6.2	2.6	5.2	1.9	4.1
ØEM	30.0	3.9	4.3	5.4	9.7	4.7	8.6	4.0	7.6	3.1	6.2	2.5	5.2	1.9	4.1
LOWER MORRISON C	REEK														
Lake Ontario	360.0	37.0	37.9	32.0	35.3	27.4	30.4	23.5	26.2	18.2	20.8	14.6	16.5	11.2	12.7
Morrison Road	320.0	32.7	33.6	31.5	34.5	27.4	30.4	23.5	26.2	18.2	20.6	14.6	16.5	11.2	12.7
East Branch															
Linbrook Road	75.0	9.9	10.0	15.9	16.8	14.1	14.9	12.4	13.1	10.1	10.7	8.5	9.1	6.7	7.1
QEW	40.0	5.3	5.3	13.3	13.3	11.9	11.9	10.5	10.5	8.6	8.6	7.3	7.3	5.7	5.7
West Branch															
Chartwell Drive	170.0	17.0	17.9	23.0	25.6	20.0	22.5	17.0	19.3	13.2	15.1	10.6	12.2	7.6	8.9
Maple Avenue	160.0	15.3	16.2	23.0	25.6	20.0	22.5	17.0	19.3	13.2	15.1	10.6	12.2	7.6	8.9
CN Railway	130.0	12.9	13.5	23.0	25.6	20.0	22.5	17.0	19.3	13.2	15.1	10.6	12.2	7.6	8.9

## 9.8 Corrective - Structural Alternatives to Modify the Flood

Structural alternatives to modify the flood include storage ponds, dykes, channel improvements (crossings and alignment) and diversions. Several alternatives were formulated for the Lower Morrison/Wedgewood Creeks after a review of the flood damage locations and the hydrologic/hydraulic results.

The detailed cost breakdowns for each of the alternatives discussed in this section are shown in Appendix H.

## 9.8.1 Flood Storage - Lower Morrison Creek

The only vacant land that could be used for a detention facility is located in Figure 9-3, upstream of Maple Avenue along the West Tributary. Only vacant land was considered due to the large social disruption of acquiring occupied land.

The hydraulic analysis results indicated that the majority of potential flooding within the Study area was the result of inadequate culvert capacities. Any detention facility would have to reduce peak flow rates to the capacity of the smallest downstream culvert.

The dry detention pond was designed to have a maximum outflow rate of approximately 10 m³/s or the capacity of the Maple Avenue culvert. The existing Maple Avenue culvert would be retained as an outlet with appropriate inlet works being constructed.

The detention facility would be designed to accommodate runoff from both the West and East Branches. Runoff from the East Branch would be diverted by a trapezoidal Terrafix block (or equivalent) lined channel from the CN Railway culvert to the upstream face of the Maple Avenue culvert.

A diversion is necessary to reduce flooding along the East Branch and downstream of the confluence. Without the diversion the detention facility would only reduce flooding along the West Branch. Peak runoff rates from the East Branch watershed would be greater than the capacities of the downstream culverts. Characteristics of the pond and the diversion channel are described in Table 9.1 and 9.2.

Table 9.1 LOWER MORRISON CREEK DETENTION FACILITY CHARACTERISTICS

Property Required 8 ha
Maximum Water Level 95.0 m
Maximum Water Depth 1.9 m
Maximum Storage 4.8 ha-m

Outlet - Maple Avenue Culvert

Peak Outflow Rate
Peak Inflow Rate

3.1 x 1.2 m rectangular concrete

12.9 m³/s (Regional future) 35.0 m³/s (100 year future)

Maximum Ponding

Duration

4.0 hours

**Excavation Required** 

11.0 ha-m

Terrafix Block (or equivalent) Low Flow Channel

#### Table 9.2 LOWER MORRISON CREEK DIVERSION CHANNEL CHARACTERISTICS

Length 500 m

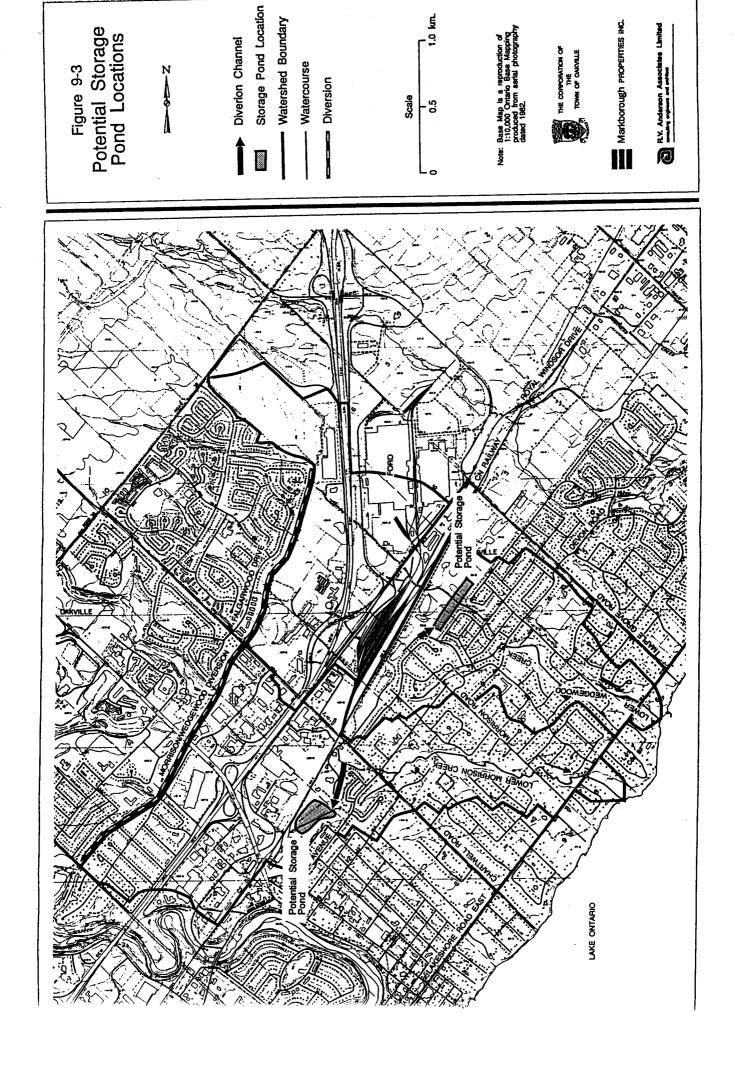
Side Slopes 3:1 (horizontal to vertical)

Bottom Width 1 m Maximum Depth 2 m

Channel Slope 0.004 m/m

Material Terrafix Block (or equivalent)

The detention facility would have sufficient capacity to eliminate damages for the 100 year flood downstream along both the East and West Branches. However, the pond would not significantly affect flood damages for the Regional event. Other measures such as floodproofing and culvert enlargement would be required to completely eliminate flood damages.



The proposed diversion and detention facilities would have a total cost of \$12.9 million. Construction costs are estimated at \$3.2 million; land costs at \$9 million. Annual operation and maintenance are estimated at \$20,000. Average annual flood damages would be reduced by \$95,000 to \$120,000.

The maximum pond elevation is limited by the ground elevation (95.5 m) of adjacent properties. The properties drain through a rear yard swale to the Maple Avenue culvert.

## 9.8.2 Flood Storage - Lower Wedgewood Creek

Two (2) locations along the East Branch of Lower Wedgewood Creek were identified for detention facilities.

One was located between Cornwall Road and the CN Railway and the other was located east of Cornwall Road adjacent to the residential subdivision.

The proposed detention facility located south of Cornwall Road was favoured because it could accommodate a diversion from the West Branch. Without the diversion the detention facility would only reduce peak flow rates and damages along the East Branch.

An embankment and outlet structure would have to be constructed in order to detain runoff. Details of the diversion and the detention facility can be found in Table 9.3 and 9.4. Peak outflow rates would have to be reduced to the downstream minimum culvert capacity of approximately 9.0 m³/s. The outlet works would consist of a concrete box culvert. The embankment would have a length of approximately 700 m.

A diversion channel from the West Branch would be constructed along the upstream face of the detention embankment. The trapezoidal Terrafix (or equivalent) lined channel would be approximately 4 m deep with 3:1 side slopes and a bottom width of 1.0 m.

The hydrologic analysis of the proposed detention facility found that the pond did have sufficient volume to eliminate flood damages for the Regional event. Other measures such as floodproofing and culvert enlargement would have to be employed to eliminate damages for the Regional Flood.

The proposed diversion and detention facility would have a total cost of \$12.2 million. Included are land costs at approximately \$9.0 million and construction costs at approximately \$3.2 million. Annual operation and maintenance is estimated at \$20,000. Average annual flood damages would be reduced from \$360,000 to \$37,000 (future land use).

## Table 9.3 LOWER WEDGEWOOD CREEK DETENTION FACILITY CHARACTERISTICS

Property Required	8 ha
Maximum Water Level	97.0 m
Maximum Water Depth	2.5 m
Maximum Storage	5.1 ha-m

Outlet -

Peak Outflow Rate 18.3 m³/s (Regional future)
Peak Inflow Rate 52 m³/s (100 year future)

Maximum Ponding Duration 4.0 hours

Excavation Required 7.0 ha-m

Terrafix Block (or equivalent) Low Flow Channel

# Table 9.4 LOWER WEDGEWOOD CREEK DIVERSION CHANNEL CHARACTERISTICS

Length	360 m
Side Slopes	3:1
Bottom Width	1 m
Maximum Depth	4 m
O	'

Channel Slope 0.004 m/m

Material Terrafix Block (or equivalent)

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Designation of Trafalgar Road as a permanent flood route may impact other essential services during flooding events. Emergency services may not be able to utilize Trafalgar Road due to the depth of flood waters in the subway.

Approximately \$50,000 has been allotted to designate Trafalgar Road as a permanent flood route. The cost includes time for Town of Oakville staff to conduct the necessary analyses and investigations. Average annual damages along Lower Morrison Creek would be reduced from \$215,000 to \$140,000 and one (1) building would be removed from the Regulatory Flood Plain. The building is located adjacent to the Maple Avenue crossing. Flood levels upstream of Maple Avenue would be reduced by approximately 0.1 m.

## 9.8.7 Diversion - Lower Morrison Creek, Cornwall Road

This alternative would reduce potential flood damages along both the West and East Tributaries of Lower Morrison Creek. Cornwall Road will be extended from Chartwell to Trafalgar Road. The alignment has been selected, but construction has not started. A culvert could be constructed to divert runoff from the upper reaches of Lower Morrison Creek to the Sixteen Mile Creek. The culvert would be constructed within the Cornwall Road right-of-way and would follow Trafalgar Road to Sixteen Mile Creek.

Runoff rates higher than the existing 2 year peak flow rates would be diverted to Sixteen Mile Creek. The construction cost is based on a concrete box culvert which varies in size from 2.0 m X 2.0 m to 4.0 m X 2.0 m. The total length of the diversion culvert would be approximately 1.3 km. The culvert would require a significant outlet structure into Sixteen Mile Creek. The capacity of the 4.0 m X 2.0 m concrete box culvert is approximately 26 m³/s. The 100 year peak flow rate is approximately 26 m³/s. Peak flow rates greater than 8 m³/s would be diverted to Sixteen Mile Creek. The 4.0 X 2.0 m box culvert would convey runoff from both the East and West Tributaries.

# CONCLUSIONS AND RECOMMENDATIONS

**Chapter 12** 

## 12.0 CONCLUSIONS AND RECOMMENDATIONS

The Regulatory Flood Plain for the Lower Morrison/Wedgewood Creeks was delineated on topographic mapping with a scale of 1:2,000.

The Regulatory Flood would potentially inundate approximately 26 buildings along Lower Morrison Creek and 42 buildings along Lower Wedgewood Creek. The Regulatory Flood would potentially create approximately \$2,030,000 in flood damages along both watercourses. Potential average annual flood damages for the Lower Morrison Creek are approximately \$215,000 and \$360,000 along Lower Wedgewood Creek.

An erosion inventory of the Lower Morrison/Wedgewood Creeks was undertaken during October 1989. A total of 15 erosion sites were identified.

One (1) of the sites requires immediate attention as two (2) buildings are located within one (1) metre of the top of bank. Two (2) additional sites require regular monitoring. The remainder of the sites were classified as medium or low priority.

A number of alternative flood control measures were identified and evaluated. The evaluation considered both social and environmental factors.

The implementation of the master drainage plan will cost approximately \$3,410,000 and is expected to be completed within the next 10 to 20 years.

A master drainage plan was developed. It is composed of preventive stormwater management policies and structural flood and erosion control works.

The flood control works consisted of culvert enlargement, floodproofing and channelization. The erosion control measures included, retaining walls, culvert protection and seed and mulch.

A stormwater management policy was developed to ensure future development would not increase flood and erosion damages.

IT IS RECOMMENDED THAT THE AUTHORITY AND THE TOWN ADOPT THE FLOOD PLAIN MAPPING TO REGULATE FUTURE DEVELOPMENT IN THE FLOOD PLAIN.

IT IS RECOMMENDED THAT THE AUTHORITY AND THE TOWN IMPLEMENT THE MASTER DRAINAGE PLAN TO ALLEVIATE EXISTING FLOODING AND EROSION AND TO PREVENT FUTURE DEVELOPMENT FROM INCREASING FLOODING AND EROSION.

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